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February 14, 2022

Rochester Planning Board Attn. Nel Sylvian 31 Wakefield Street Rochester, NH 03867

RE: Response Letter 3 Wadleigh Road, Rochester, NH Tax Map 137, Lot 35-1 JBE Project No. 21137

Dear Mr. Sylvian,

We are in receipt of comments from Renee Bourdeau, P.E. At Geosyntec dated January 11, 2022. Review comments are listed below with our responses in **bold**.

GEOSYTEC DRAINAGE ANALYSIS COMMENTS:

- Anticipated project state and completion dates, and duration of grading and construction activities are not provided.
 RESPONSE: This section 218-8 B of the Stormwater Management & Erosion Control allows for sites that require SWPPP's to have the SMECP requirements added into that document. We would like to request that we do this for this development. This information will be provided as part of EPA SWPPP documents as they will outline all of this information. Dates of construction will be determined once all permits have been obtained.
- 2. Documentation on what LID site planning and design strategies were used on-site or why using LID strategies are not feasible, as required under § 218-8.B(1)(d) is not provided. RESPONSE: LID design features are included in the Drainage Report and include the use of Focal Point Treatment Systems to treat all parking lot runoff and also a portion of runoff from Wadleigh Road. The remainder of the road will utilize a bioretention basin designed to AoT specifications for water quality treatment. Design sheets for the Focal Point systems are included in the Drainage Report.
- 3. Description of the proposed changes in impervious cover is not provided. RESPONSE: Changes in impervious cover is described in the Drainage Report.

4. Description of the procedures to limit and/or optimize use of deicing materials and minimize off-site increases in chloride levels in adjacent surface and groundwater is not provided.

RESPONSE: This site is not located in a Chloride Impaired area and typically NHDES AOT does not require salt minimizations plans for these sites. All of our stormwater treatment is downstream of the road network and the stormwater gets treated per AOT regulations prior to release.

- 5. Description of the procedures to control waste such as discarded building materials, construction debris, sanitary waste, concrete washout, chemicals, litter are not provided. RESPONSE: The above will be addressed in the SMECP and SWPPP Plan and will be provided by the contractor prior to construction.
- 6. Copies are pertinent state permits (AoT and wetlands), if applicable, are not provided. RESPONSE: State permits required for the project are listed on Sheet C3 of the plan set. All permits are currently pending and will be forwarded when received.

GEOSYTEC SITE DEVELOPMENT PLAN COMMENTS:

- 1. Drainage patterns and direction of flow of stormwater runoff using arrows within the project area and 200-feet outside of the project boundary were not provided for the existing or proposed conditions on the site plans or watershed plans **RESPONSE: Flow arrows have been added to the Watershed Plans.**
- A limit of earth disturbance is not shown on the site plans.
 RESPONSE: A limit of work line is now shown on the Erosion Control Plans.
- 3. A cut and fill plan was not provided. RESPONSE: The above will be provided with the SMECP Plan when we submit that application.
- 4. Location of equipment storage and staging areas are not shown. Procedures should be added to the Drainage Analysis Report to reflect the added controls. RESPONSE: The above will be addressed in the SWPPP Plan will be provided by the contractor prior to construction.
- 5. Location of vehicle fueling areas or equipment fueling areas are not shown. Procedures should be added to the Drainage Analysis Report to reflect the added controls. **RESPONSE: The above will be addressed in the SWPPP Plan will be provided by the contractor prior to construction.**
- Locations of disposal facilities for solid waste, construction debris, sanitary waste, concrete washout, and plan for stump disposal (if applicable) are not shown.
 RESPONSE: The above will be addressed in the SWPPP Plan will be provided by the contractor prior to construction.



7. A Grading and Drainage Plan and Erosion Control Plan for the southern portion of the project should be provided. **BESPONSE:** A Grading and Drainage Plan and Erosion Control Plan for the

RESPONSE: A Grading and Drainage Plan and Erosion Control Plan for the southern portion of the site is now included in the Plan Set.

GEOSYTEC TEMPORARY CONSTRUCTION STORMWATER DESIGN COMMENTS:

 Site plans show locations for proposed snow management areas. However, a snow storage area is show between the two parking areas which is also intended to be used to capture stormwater, as this area is uncurbed. The Applicant should find an alternative location for snow storage, as snow should not be stored in stormwater management facilities.
 RESPONSE: The snow storage area between the two parking lots has been

RESPONSE: The snow storage area between the two parking lots has been removed.

- Stabilization notes on the site plans and within the Drainage Analysis Report should be updated to reflect the requirements under § 218-9.A(8)(a), which state that temporary stabilization measures should be in place within 5 calendar days for exposed soil areas that are within 100-feet of a surface water body or a wetland.
 RESPONSE: The above note has been added to the Drainage Report and on Sheet E1.
- Sediment traps are identified in the Drainage Analysis Report; however, are not proposed on the site plan. Locations for temporary sediment traps should be shown on the site plan.
 RESPONSE: The above will be addressed in the SWPPP Plan will be provided by the contractor prior to construction.
- An inspection and maintenance schedule is not provided for the construction entrance, inlet protection, stockpiles, slope protection, and outlet protection.
 RESPONSE: Permanent Erosion Control Items are included the Inspection and Maintenance (I&M) document. Temporary Erosion Control used during construction will be provided in the SWPPP Plan by the contractor.

GEOSYTEC POST-CONSTRUCTION STORMWATER COMMENTS:

1. Calculations are not provided to demonstrate that the existing drainage system and catch basin grate located at the entrance of the site adjacent to Route 125 can accommodate additional flows and volumes from the proposed development. The drainage analysis shows that the peak discharge will increase to this area from all storm events presented. Further, water quality treatment is not provided for the impervious cover draining to this catch basin.

RESPONSE: A portion of the offsite Anchorage Inn drainage currently flowing to the existing drainage system along Route 125 has been redirected to a cross culvert under Wadleigh Road. In additions, a swale has been graded along the entry to Wadleigh Road to capture any offsite flow going to paved areas. These changes now allow for a decrease in flow to the catch basing on Route 125. The amount of



pavement flowing to this catch basin will remain the same therefore no additional treatment is planned for this runoff.

2. Provide a planting plan for the Focal Point biofiltration systems. Native plants should be considered and proposed in density sufficient to prevent surface erosion and to achieve water quality treatment requirements. Also, an alternative to hardwood bark mulch should be considered as this tends to float, not reduce erosion at the inlet, and clog overflow structures.

RESPONSE: A planting plan for the Focal points is included on the Detail Sheet.

GEOSYTEC STORMWATER MANAGEMENT DESIGN STANDARDS FOR NEW DEVELOPMENT COMMENTS:

1. Calculations are not provided to demonstrate that the total post-construction impervious area is treated to remove at least 80% total suspended solids and 50% removal of total phosphorus and total nitrogen, as required under § 218-10.C(1)(a). The Applicant should provide calculations that are consistent with the methods referenced in § 218-10.A(3)(a,b).

RESPONSE: FocalPoint is approved by NH AOT site development projects and provides the following standalone pollutant removal efficiencies: 91% TSS, 66% phosphorous and 48% nitrogen. A cut sheet for the Focal Point efficiencies is included with this submittal and listed in the Drainage Report.

Bioretention Ponds are listed in AoT Stormwater Regulations as having pollutant removal efficiencies of 90% TSS, 65% PH and 65% Nitrogen. Combined with Deep sump catch basins and a Sediment Pond in the Treatment Train, the combined pollutant removal is almost 100% TSS. 70% PH and 70% Nitrogen and therefore exceed City requirements. The AoT Pollutant Removal Efficiency Table has been added to the Drainage Report for reference.

2. Calculations are not provided to demonstrate that the stormwater treatment practices have been designed for the water quality volume or water quality flow, in accordance with Env- Wq 1504.10 and Env-Wq 1504.11, respectively, as required under § 218-10.C(1)(c).

RESPONSE: Focal Point Sizing is now included in the Drainage Report which demonstrates that the Focal Points are sized for the correct water quality volume. A BMP for the Bioretention Pond is also included in the Drainage Report to demonstrate that it is designed to treat the water quality volume per AoT standards.

3. Calculations are not provided to demonstrate protection of groundwater resources by reducing the post-development stormwater runoff volume by infiltrating Groundwater Recharge Volume as required under § 218-10.C(2)(a,b).

RESPONSE: A portion of the stormwater runoff will infiltrate within the Stormtech Chambers and within the drip edge adjacent to the building. There is a small (3.4%) increase in runoff volume in the 25-year storm event.



4. Calculations are not provided to demonstrate that the post-development stormwater runoff volumes do not exceed the pre-development stormwater runoff volumes for the 2-year, 10-year and 25-year, 24-hour design storm events, as required under § 218-10.C(3)(a).

RESPONSE: There is no increase in the peak rate of runoff for the 2-, 10- or 25year storm event, however there remains a small increase (3.4%) in runoff volume in post development conditions because of the rocky soil type and limitations in infiltration area. We are requesting a waiver for this City requirement and will be requesting a similar waiver from AoT when submitted.

GEOSYTEC STORMWATER DRAINAGE SYSTEM COMMENTS:

- Calculations are not provided to demonstrate that the closed drainage system was sized for the 25-year, 24-hour storm event, as required under § 218-10.F(2)(a).
 RESPONSE: The closed drainage system piping has been added to the Hydrocad model to demonstrate that it is sufficient size for all storm events.
- Calculations are not provided to demonstrate that the proposed culverts (both open bottom and circular) were sized in accordance with the New Hampshire Stream Crossing Guidelines in accordance with § 218-10.F(2)(b).
 RESPONSE: Both culverts crossing Wadleigh Road are replacing existing culverts already in place. Neither of the culverts cross a stream. The cross culverts have been modeled using Hydrocad and have ample capacity to convey the required stormwater.
- Calculations are not provided to demonstrate that the closed drainage network has a minimum velocity of 2 feet per second, as required under § 218-10.F(2)(d).
 RESPONSE: The velocities for the two culverts in the closed drainage system are included in the Drainage report.
- Rip-rap depths along slopes have not been specified in accordance with § 218-10.F(2)(e). RESPONSE: Rip rap calculations are now included in the Drainage Report. Riprap sizes have been added the Grading Plans.
- 5. Calculations are not provided to demonstration that velocities entering the proposed swale are less than 10 feet per second and that the maximum velocity within the swale is 1 foot per second during the 25-year, 24-hour storm event, as required under § 218-10.F(2)(c).
 RESPONSE: The velocities within the swale are included in the Drainage Report.
- 6. If the City will be accepting the road and associated utilities, maintenance access easements need to be established for the drainage network and should be provided on the plans, as required under § 218-10.F(3).
 RESPONSE: We will be discussing any required easements with the City DPW and will provide what is necessary.



7. In the pre-development condition, a swale exists along Wadleigh Road adjacent to the Anchorage Inn site to convey flows from the property to an existing catch basin. Based on the proposed grading, this existing swale is removed. The Applicant should provide details for how existing flows from the Anchorage Inn parcel will be conveyed adjacent to Wadleigh Road.

RESPONSE: A swale has been graded along Wadleigh Road in front of the Anchorage Inn to intercept runoff from the Anchorage Inn site and the slope in front of the Anchorage Inn will be regraded. The Anchorage Inn site runoff will flow to the same catch basin that it currently does.

<u>GEOSYTEC POST CONSTRUCTION INSPECTION AND MAINTENANCE</u> <u>AGREEMENT COMMENTS:</u>

- 1. The inspection and Maintenance Plan should include the following:
 - a. The name of the responsible party for inspections and maintenance RESPONSE: These units are proposed as rental units and all maintenance will be the responsibility of the owners. Typically, AOT requires that projects of this size have annual maintenance inspection performed by a qualified third-party inspector
 - all of the proposed stormwater practices including but not limited to subsurface chambers, focal point media filters, pret-x units, riprap inlet and outlet protection, catch basin, and the closed drainage network.
 RESPONSE: The I&M document discusses these best management practices
 - c. a proposed schedule of inspection frequency, RESPONSE: We are proposing annual inspections. A checklist is provided in the I&M manual.
 - *A plan identifying each BMP and associated details an inspection checklist and photo documentation requirements,* **RESPONSE: A BMP plan has been added to the I&M document**
 - e. Sample log to document each inspection and maintenance activity RESPONSE: This has been added to the I&M document.
 - f. Sample deicing log to track amount and type of deicing materials I applied to the site
 RESPONSE: This has been added to the I&M document.
 - g. description of maintenance response actions, including actions to be taking if invasive species begin to grow in stormwater practices, and
 RESPONSE: We have added the information provided in the Stormwater Management and Erosion Control Chapter 218 into the I&M document



h. documentation of how reports will be completed, submittal and retention procedures, and contingency plans if future maintenance is required.
RESPONSE: This information is provided in the I&M document and will be handled on a case by case depending on the situation and we will make reports available upon request to the DPW.

GEOSYTEC OTHER COMMENTS:

1. Stone slope protection hatching is show on Drawing No. C6 (Sheet 9) to be partially within a proposed swale adjacent to the parking area. The Applicant should clarify whether this swale should be a stone lined swale or a vegetated swale. Further, the Landscaping Plan (Drawing No. L1) shows this entire area as "lawn area" and does not show the rip-rap slope protection. The Applicant should ensure that the proposed trees do not encroach on the proposed swale. The plans should be updated to reflect the appropriate conditions.

RESPONSE: The swale adjacent to the parking area has been called out as a stonelined swale. The Landscape Plan has been revised to include the stone slope protection and the trees in this area have been removed. The "lawn area" label has been removed.

- 2. Stone slope protection hatching shown on Drawing No. C6 (Sheet 9) adjacent to the existing wetland and proposed open box culvert is not shown on the Landscaping Plan (Drawing No. L1). A tree is also proposed at the top of this slope. The Applicant should ensure that there is sufficient room to accommodate the tree at the top of the slope. RESPONSE: Areas of riprap and stone slope protection are now shown on the Landscape Plan. The tree at the top of the slope has been removed.
- 3. The Grading and Drainage Plan (Drawing No. C5) identifies Focal Point 1, 2 and 3. The Utility Plan (Drawing No. U2) also identifies a Focal Point 3 in an alternate location of the one specified in the Grading and Drainage Plan. The Applicant should reconcile the numbering and include a detail schedule on the Detail Sheet (Drawing No. D4) with the appropriate elevations as noted in the detail.

RESPONSE: The numbering on the Focal Points has been corrected. A detail schedule of the Focal Point sizing and elevations is included on the Detail Sheet.

- 4. The Grading and Drainage Plan (Drawing No. C5) identifies Pret-X filters 1, 2, 3, 4 and 5. The Utility Plan (Drawing No. U2) also identifies a Pret-X filter 3 in an alternate location of the one specified in the Grading and Drainage Plan. The Applicant should reconcile the numbering and provide a detail schedule on a detail sheet. RESPONSE: The numbering of the Pre-Tx filters has been reconciled.
- 5. Detail for the Pret-X filters is not provided RESPONSE: A detail for the Pre-Tx filter has been added to the Detail Sheets.



- 6. Bedding material specified for the Precast Rigid Frame Box Culvert should be consistent with native stream bed materials. The Applicant should provide material specifications consistent with recommendations from the New Hampshire Stream Crossing Standards. RESPONSE: The Box Culvert is not located in an existing stream but is instead replacing and existing culvert already in place. The bedding under the culvert is specified on the Detail Sheet.
- 7. For the proposed bioretention facility (Pond 3P), the detail shows the bottom of the sediment forebay at elevation 212; however, the invert out into the sediment forebay is 210.92.

RESPONSE: The bottom of the forebay has been regraded to be at elevation 208.95

8. Details, specifications, and calculations are not provided for the proposed porous paver patio drip edge. Test pit data in the vicinity of the drip edge shows SHWT between 222.11 and 215.66, whereas the HydroCAD report shows bottom of the drip edge at 216.99. The Applicant should conduct additional test pits to confirm SHWT and infiltration calculations to confirm exfiltration rates.

RESPONSE: The bottom of the drip edge has been raised to elevation 217.50. Test pit #5 shows SHWT at 215.68 while Test Pit 4 shows high ledge within the building footprint. The ledge in the building area will be overblasted to well below the bottom of the building footing and removed and the area filled in with free drainage structural fill, which will allow some infiltration in the area of the drip edge.

- 9. Permanent riprap apron outlet protection sizing calculations are not provided. RESPONSE: Riprap calculations are now provided in the Drainage Report.
- 10. Outlet protection is not shown at the outlet of Focal Point 3 on Utility Plan U2. Calculations should be provided to demonstrate that proposed velocities will not cause erosion to downstream soil/vegetation.

RESPONSE: Riprap and sizing has been added to this Focal Point outlet. Riprap calculations are included in the Drainage Report.

- 11. The following comments are specific to the HydroCAD Report and Watershed Plans:
 - a. The Existing Watershed Plan identifies an Analysis Point #2 which is not provided in the HydroCAD model. This Analysis Point should be added and peak discharge and runoff volumes summarized to this point in the Drainage Analysis Report.
 RESPONSE: Analysis Point #2 has been added to the Hydrocad models.
 - b. The post-construction plan has subcatchment 10S being routed to Analysis Point #1. The existing conditions model has this area discharging to Analysis Point #2 (Columbus Avenue). This subcatchment should be routed to Analysis Point #2 and peak discharge and runoff volumes summarized to this point in the Drainage Analysis Report.

RESPONSE: The Subcatchments have been revised to flow to the corrected Analysis Points.



 c. The time of concentration paths are not provided on the Proposed Watershed Plan
 RESPONSE: The Tc Paths have been added to the Proposed Watershed

RESPONSE: The Tc Paths have been added to the Proposed Watershed Plans.

- d. Summary for Pond 2P: StormTech 2 has a 4" round culvert as the primary outlet. The Grading and Drainage Plan shows a 6" pipe out.
 RESPONSE: The pipes sizes have been corrected.
- e. Summary for Pond 3P: Pond 3P shows 100% void space (reflective of ponded area) between elevations 212.50 and 213.79; however, the detail-on-Detail Sheet D3 shows that between elevations 212.25 and 213.80 is the topsoil, mulch, and sand mixture.
 RESPONSE: The void space calculations have been revised.
- f. Outlet device table for Pond 3P: Pond 3P shows an 18" pipe with an invert of 208.5 whereas the detail-on-Detail Sheet D3 shows an 8" pipe out with an invert of 210.50. HydroCAD table also shows a 2" vertical orifice which is not shown on the detail.
 RESPONSE: The detail has been corrected to show to correct pipe size and invert to match the Hydrocad model. The 2" vertical orifice modeled within Hydrocad is shown on the detail as the 2" perforated Underdrain to drain

the bottom 18" stone of the bioretention pond.

g. The Focal Point media filters are not modeled. It is unclear if the proposed filters can convey the proposed storm events and where bypass flows go if the filters become clogged or overwhelmed.
RESPONSE: Sizing for the Focal Points is now included in the Drainage Report.

Included with this response letter are the following:

- 1. Three (3) Full Size Plan Sets.
- 2. Sixteen (16) Half-Size Plan Sets.
- 3. Three (3) Revised Drainage Analysis.
- 4. Waiver Request Letter.

Thank you very much for your time.

Very truly yours, JONES & BEACH ENGINEERS, INC.

Brad Jones Vice President

cc: Fenton Groen, Groen Construction (via email)





February 11, 2022

Rochester Planning Board Attn. Nel Sylvian 31 Wakefield Street Rochester, NH 03867

RE: Waiver Request Wadleigh Road, Rochester, NH Tax Map 137, Lot 35-1 JBE Project No. 21137

Dear Mr. Sylvian,

Jones & Beach Engineers, Inc. is the Engineer of Record for the Proposed Wadleigh Road Apartment Project currently under review by the City of Rochester Planning Board.

We respectfully request a waiver from section 218-10 C(2) Groundwater Recharge Requirements. Using multiple stormwater management technologies, we have been successful is decreasing the peak stormwater discharge from this project for all studied storm events. We have attempted to infiltrate as much stormwater as possible to also reduce stormwater volume, however, due to high water tables and the quantity of ledge on this site, we are unable to reduce the volume of stormwater to the level that exists in pre-existing conditions. We anticipate a calculated increase in total stormwater volume of 3.4% with this development over the entire parcel.

All stormwater from the project flows to Axe Handle Brook, which abuts the property. This brook has enough capacity to accept the small increase in stormwater volume discharged from the site and will not cause adverse impacts to downstream properties, infrastructure, aquatic habitat, or water quality degradation in downstream water bodies. We will be detaining much of the stormwater on site so as not to increase the peak amount of stormwater.

Thank you very much for your time.

Very truly yours, JONES & BEACH ENGINEERS, INC.

Brad Jones Vice President

cc: Fenton Groen, Groen Construction (via email)

DRAINAGE ANALYSIS

SEDIMENT AND EROSION CONTROL PLAN

Wadleigh Road Apartments Tax Map 137 Lot 35-1 Route 125 Rochester, NH 03839

Prepared for:

Groen Construction 120 Washington Street Suite 302 Rochester, NH 03839



Prepared by: Jones & Beach Engineers, Inc. 85 Portsmouth Avenue P.O. Box 219 Stratham, NH 03885 (603) 772-4746 November 3, 2021 Revised December 14, 2021 Revised February 10, 2022 JBE Project No. 21137

EXECUTIVE SUMMARY

Groen Construction proposes to construct a 52-Unit Apartment Building on a ± 8.4 -acre parcel of land located at the end of Wadleigh Road in Rochester, NH. A drainage analysis of this parcel was conducted for the purpose of estimating the peak rate of stormwater runoff and to subsequently design adequate drainage structures. Two models were compiled, one for the area in its existing (preconstruction) condition, and a second for its proposed (post-construction) condition. The analysis was conducted using data for the 2 Year – 24 Hour (3.08"), 10 Year – 24 Hour (4.63"), 25 Year– 24 Hour (5.84") storm events using the USDA SCS TR-20 method within the HydroCAD Stormwater Modeling System environment. A summary of the existing and proposed conditions peak rates of runoff is as follows:

COMPONENT	PEAK RA	PEAK RATE OF RUNOFF (CUBIC FEET/SECOND)							
	2 Y	ear	10 Year		25 Year				
	<u>Existing</u>	Proposed	<u>Existing</u>	Proposed	Existing	Proposed			
Analysis Point #1	10.49	9.41	23.94	20.61	35.83	30.95			
Analysis Point #2	2.39	2.10	4.33	3.95	5.87	5.43			

The project site is located in Zone Highway/Commercial. The subject parcel consists primarily woodlands with an existing cell tower and gravel access road. The site is primarily undeveloped with the exception of the cell tower structure. The entrance to the site is by way of the existing paved Wadleigh Road which is the entrance to the abutting Anchorage Inn. The existing topography is such that the existing conditions site analysis requires four (4) subcatchments. The site drains in a northerly direction to a wetland adjacent to Axe Handle Brook (Analysis Point #1). The existing paved portion drains westerly to an existing drainage system located at the entrance of the site adjacent to Route 125, which outlets to Analysis Point #2.

The proposed site development consists of the aforementioned apartment complex with associated paved parking areas. The site is accessed by an approximate 650-foot extension of the existing Wadleigh Road. Wadleigh Road will also be widened from 20' to 26' to accommodate the increase in traffic and the addition of a bike lane. The remainder of the site is divided into fifteen subcatchments. The runoff from these subcatchments has increased from that of the existing conditions due to the addition of the impervious buildings and paving. This runoff will be directed via site grading and closed drainage to three stormwater management areas located throughout the site. As shown in the above table, the proposed peak rates of stormwater runoff will be reduced from that of existing conditions for all analysis points.

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1.0 RAINFALL CHARACTERISTICS

This drainage report includes an existing conditions analysis of the area involved in the proposed development, as well as a proposed condition, or post-construction analysis, of the same location. These analyses were accomplished using the USDA SCS TR-20 Method within the HydroCAD Stormwater Modeling System. The curve numbers were developed using the SCS TR-55 Runoff Curve numbers for Urban Areas. A Type III SCS 24-hour rainfall distribution was utilized in analyzing the data for the 2 Year – 24 Hour (3.08"), 10 Year – 24 Hour (4.63"), and 25 Year – 24 Hour (5.84") storm events.

As the table in the Executive Summary demonstrates, the proposed peak rates of runoff will be reduced from the existing conditions of the site, thereby minimizing any potential for a negative impact on abutting properties or infrastructure by allowing for better control of peak rates of stormwater runoff.

2.0 EXISTING CONDITIONS ANALYSIS

The subject parcel consists primarily of undeveloped woodland with the exception of a cell tower structure and gravel access road. The entrance to the site is by way of the existing paved Wadleigh Road which is the entrance to the abutting Anchorage Inn. The existing topography is such that the existing conditions site analysis requires four (4) subcatchment. The topography of the site varies from flat to steep throughout the site, with some slopes that are adjacent to the wetland exceeding 15%.

Classified through the use of the Natural Resources Conservation Service's web soil survey, the land of the site is composed of two soil types. The in-situ soils are categorized into Hydrologic Soil Group C, with an area of D soils located in the northwest portion of the site (see appendix for soil types and HSG designations). Most of the development is located on HSG C type soils that comprise most of the site.

The majority of the site drains in a northerly direction to a wetland area adjacent to Axe Handle Brook (Analysis Point #1). The remainder of the site drains southerly to an existing catch basin and drainage system located southerly of the site adjacent to Route 125 (Analysis Point #2).

3.0 PROPOSED CONDITIONS ANALYSIS

The addition of the proposed impervious paved areas and buildings causes an increase in the curve number (C_n) and a decrease in the time of concentration (T_c), the net result being a potential increase in peak rates of runoff from the site. The proposed site development consists of the aforementioned apartment building with associated pavement/parking areas. The site is accessed by the construction of an approximately 650- foot extension of Wadleigh Road. Wadleigh Road will also be widened to allow for an increase of traffic. Wadleigh Road will be regraded to allow for the southerly half to continue to flow to the existing drainage system (Subcatchment 12S). Subcatchment 11S consists of the northerly half of Wadleigh, which will be regraded to flow into a focal point stormwater treatment system and be released to Analysis Point 1.

The runoff from the extended Wadleigh Road, Subcatchments 7S1 and 7S2, will flow via closed drainage to Bioretention Pond 3P, which outlets to AP1. A portion of the Existing Anchorage Inn site

(Subcatchment 7S) will be redirected to flow to a cross culvert under Wadleigh Road to eliminate offsite flow over the travelway and to Analysis Point #1.

The remainder of the site is divided into 11 subcatchments. The runoff from Subcatchments 2S and 3S will flow to Focal Point Treatment systems and to a subsurface detention system located under the main parking area. The runoff from Subcatchment 5S will flow to an additional Focal Point and subsurface detention system located under the parking area southerly of the building. Stormwater from both of these systems will be treated using Pre-Tx structures outletting to focal points. As shown in the above table, the proposed peak rates of stormwater runoff will be reduced from that of existing conditions for all analysis points.

As shown in the table within the Executive Summary, the proposed peak rates of stormwater runoff will be reduced from that of existing conditions for all analysis points.

In an effort to reduce sedimentation and erosion, the outlets of all culverts will be protected from erosion by the use of riprap protection aprons. Overall, the structures outlined in this proposal provide for adequate treatment of stormwater runoff for sediment and associated pollutants.

Pollutant Removal

FocalPoint is approved by NH AOT site development projects and provides the following standalone pollutant removal efficiencies: 91% TSS, 66% phosphorous and 48% nitrogen. A cut sheet for the Focal Point efficiencies is included with this submittal and listed in the Drainage Report. Bioretention Ponds are listed in AoT Stormwater Regulations as having pollutant removal efficiencies of 90% TSS, 65% PH and 65% Nitrogen. Combined with Deep sump catch basins and a Sediment Pond in the Treatment Train, the combined pollutant removal for the Bioretention Area is almost 100% TSS. 70% PH and 70% Nitrogen.

4.0 SEDIMENT & EROSION CONTROL BEST MANAGEMENT PRACTICES

The proposed site development is protected from erosion and the roadways and abutting properties are protected from sediment by the use of Best Management Practices as outlined in the NHDES <u>Stormwater Manual</u>. Any area disturbed by construction will be re-stabilized within 30 days and abutting properties and wetlands will suffer minimal adversity resultant of this development. All swales and drainage structures will be constructed and stabilized prior to having runoff directed to them.

4.1 Organic Filter Berm

The plan set demonstrates the location of organic filter berm for sediment control. Sheet E1 – Erosion and Sediment Control Details, has the specifications for installation and maintenance of the filter berm. In areas where the limits of construction need to be emphasized to operators, construction fence for added visibility will be installed. Orange construction fence will be VISI Perimeter Fence by Conwed Plastic Fencing, or equal. The four-foot fencing to be installed using six foot posts at least two feet in the ground at a spacing of six to eight feet.

4.2 Stabilized Construction Entrance

A temporary gravel construction entrance provides an area where mud can be dislodged from tires before the vehicle leaves the construction site to reduce the amount of mud and sediment transported onto paved municipal and state roads. The stone size for the pad should be between 1 to 2 inch coarse aggregate, and the pad itself constructed to a minimum length of 50 feet for the full width of the access road. The aggregate should be placed at least six inches thick. A plan view and profile are shown on Sheet E1.

4.3 Environmental Dust Control

Dust will be controlled on the site by the use of multiple Best Management Practices. Mulching and temporary seeding will be the first line of protection to be utilized where problems occur. If dust problems are not solved by these applications, the use of water can be applied. Dump trucks hauling material from the construction site will be covered with a tarpaulin.

4.4 Vegetated Stabilization

All areas that are disturbed during construction will be stabilized with vegetated material within 30 days of breaking ground. Construction will be managed in such a manner that erosion is prevented and that no abutting property will be subjected to any siltation, unless otherwise permitted. All areas to be planted with grass for long-term cover will follow the specification on Sheet E1 using seeding mixture C.

4.5 Stone Grade Stabilization Structures (Check Dams)

Stone check dams will be constructed in the ditch line where specified on the plan set and in accordance with Figures 15.2 and 15.3 of the NHDES <u>Stormwater Manual</u>. They will be constructed from 2-inch to 3-inch stone riprap to a height of 24-inches. The maximum slope of the stone will be 2 to 1. The check dams will be spaced based on a flow depth of 18-inches so that the top of one check dam is at an equal elevation to the toe of the next up-slope check dam. For example, for a slope of 8% the spacing will be 18.75 feet (1.5' / .08' / = 18.75').

4.6 Temporary Sediment Traps

Temporary Sediment Traps are small temporary ponding areas that are formed by excavation or by constructing an earthen embankment across a drainage way and providing a stabilized outlet. These structures intercept sediment-laden runoff from small, disturbed areas and detain it long enough for the majority of the sediment to settle out into the sump of the trap.

4.7 Riprap Outlet Protection

Riprap Outlet Protection will be provided at the outlet of all culverts that discharge runoff into the environment (as opposed to a catch basin). The riprap outlet protection has been designed with the equations provided in the NHDES <u>Stormwater Manual</u> depending on inlet or outlet control. Details of the protection design can be found on Sheet E1 – Erosion & Sediment Control Details.

4.8 Riprap Inlet Protection Aprons

Riprap Inlet Protection Aprons are four-foot by four-foot sections of riprap placed on the ground in front of the inlet of a culvert. These aprons, built to the same specifications as the outlet protection

aprons mentioned above, help to prevent the growth of vegetation directly adjacent to an inlet, therefore reducing the potential for a debilitating clog.

4.9 Drain Manholes

A drain manhole is a pre-cast concrete structure intended for the transport of stormwater, typically utilized in streets and parking areas. These structures are to be cleaned regularly.

4.10 Catch Basins with Grease Hoods and Sumps

A Catch Basin is a pre-cast concrete structure intended for the transport of stormwater, typically utilized in streets and parking areas. All Catch Basins are to be equipped with grease hoods designed to trap oils and floatable sediment and three-foot sedimentation sumps in order to provide an area for sediment to settle out of runoff prior to its discharge from the structure. These structures are to be cleaned regularly.

4.11 Erosion Control Blanket (Jute Mat)

In newly graded areas where there exists the potential for extensive erosion prior to the establishment of an adequate vegetative cover, an erosion control blanket or jute mat may be required. A tightly woven fabric of fibers (preferably biodegradable) or a synthetic mesh, the blanket provides stability by trapping soil particles, shields loam and seed from rain and runoff, retains moisture for seed germination, deposits additional bio-mass after the blanket rots, and provides temporary (or permanent) reinforcement to turf on slopes, in channels, and along shorelines.

4.12 Rock Stabilized Steep Slope

In newly graded areas where there exists the potential for extensive erosion because of steep slope conditions, a Rock Stabilized Slope may be required. A tightly woven fabric of fibers or a synthetic mesh should be placed under the rock and a layer of sand to be placed over the fabric to protect from puncture. The blanket provides stability by trapping soil particles, and provides temporary (or permanent) reinforcement to turf on slopes, in channels, and along shorelines.

4.13 LOW IMPACT DEVELOPMENT (LID) PRACTICES

LID is a site planning and design strategy intended to maintain or replicate predevelopment hydrology through the use of site planning, source control, and small-scale practices integrated throughout the site to prevent, infiltrate, and manage stormwater runoff as close to its source as possible. Examples of LID strategies are pervious pavement, rain gardens, green roofs, bioretention basins and swales, filtration trenches, and other functionally similar BMPs located near the stormwater runoff source.

4.14 Raingarden - Bioretention cells

Construction Component – Excavate a hole at least 3 ft deep and consist of, from the bottom up:

• A geotextile fabric between natural soils and constructed media

- A base of coarse clean stone in which a 4 to 6 inch perforated underdrain is usually installed
- A layer of lightly compacted soil media at least 18 inches thick. See detail sheet for Soil filter media blend specifications.
- Vegetation mix that are both drought and flood tolerant. See Detail sheet for recommended plantings.
- Covers of 2-3 inches of aged, fibrous bark mulch.

4.15 FocalPoint Bioretention System

1. FocalPoint Biofiltration System

FocalPoint is an ultra-efficient, modular biofiltration system that treats and drains large volumes of stormwater runoff in a small footprint to meet post-construction stormwater treatment requirements. The system removes pollutants from stormwater runoff through the physical, chemical and biological mechanisms of its soil, plant and microbe complex infiltration flow rates for the system's standard media.

I. Summary

The following general specifications describe the components and installation requirements for a volume based High Performance Modular Biofiltration System (HPMBS) that utilizes physical, chemical and biological mechanisms of a soil, plant and microbe complex to remove pollutants typically found in urban storm water runoff. The modular treatment system in which the biologically active biofiltration media is used shall be a complete, integrated system designed to be placed in Square Foot or Linear Foot increments per the approved drawings to treat contaminated runoff from impervious surfaces.

The High Performance Modular Biofiltration System (HPMBS) is comprised of the following components:

A. Plant Component

- 1. Manufacturer shall provide a regionalized list of acceptable plants.
- 2. Plants, as specified in the approved drawings/manufacturer's plant list, shall be installed at the time the HPMBS is commissioned for use.
- 3. Plants and planting are typically included in landscape contract.

B. Biofilter Component

- 1. This component employs a high performance cross-section in which each element is highly dependent on the others to meet the performance specification for the complete system. It is important that this entire cross-section be provided as a complete system and installed as such.
- 2. As indicated in the approved drawings, the elements of the Biofilter include:
 - A. A <u>mulch protective layer</u> (if specified).

- B. An advanced <u>high infiltration rate biofiltration planting media bed</u> which utilizes physical, chemical and biological mechanisms of the soil, plant, and microbe complex, to remove pollutants found in storm waterrunoff.
- *C.* A <u>separation layer which utilizes the concept of 'bridging'</u> to separate the biofiltration media from the underdrain without the use of geotextile fabrics.
- D. A <u>wide aperture mesh layer</u> utilized to prevent bridging stone from entering the underdrain/storage element.
- E. A <u>modular, high infiltration rate 'flat pipe'</u> style underdrain/storage system which is designed to directly infiltrate or exfiltrate water through its surface. The modular underdrain must provide a minimum of 95% void space.

C. Energy Dissipation Component

1. An Energy Dissipation Component is typically specified to slow and spread out water as it enters the system. This component is dependent upon the design in the approved drawings, but typically consists of a rock gabion, rock filter dam or dense vegetation element, such as native grasses, either surrounding the Biofiltration Component or located immediately upstream of it.

D. Pretreatment Component

1. Pretreatment, when specified, is typically accomplished by locating the Biofiltration Component downstream of a swale, curb cut/rock apron, sediment forebay, deep or shallow sump water quality manhole, etc. These BMPs should target trash and debris and medium to coarse sediment.

E. Observation and Maintenance Component

1. An Observation and Maintenance Port shall be installed per the approved drawings to provide for easy inspection of the underdrain/storage element, and cleanout access if needed.

F. Extreme Event Overflow (by others)

1. An Extreme Event Overflow should be located external to, but near the Biofiltration element to provide bypass when needed. This may be an overland flow bypass structure, beehive overflow grate structure, or equivalent that serves the purpose. If beehive overflow structures is utilized it should include a removable filter insert to provide a minimum of 50% TSS removal and control of gross pollutants, trash and floatables.

II. Quality Assurance and Performance Specifications

The quality and composition of all system components and all other appurtenances and their assembly process shall be subject to inspection upon delivery of the system to the work

site.

Installation is to be performed only by skilled work people with satisfactory record of performance on earthworks, pipe, chamber, or pond/landfill construction projects of comparable size and quality.

A. Plants

- 1. Plants must be compatible with the HPMBS media and the associated highly variable hydrologic regime. Plants are typically facultative with fibrous roots systems such a native grasses and shrubs.
- 2. Manufacturer shall provide a regionalized list of acceptable plants.
- 3. All plant material shall comply with the type and size required by the approved drawings and shall be alive and free of obvious signs of disease.

B. Mulch

 Mulch, typically double shredded hardwood (non-floatable), shall comply with the type and size required by the approved drawings, and shall be screened to minimize fines. Rock mulch is an alternative to wood based mulch and typically consists of clean, rounded river rock (3-4" diam in size).

C. Biofiltration Media

- 1. Biologically active biofiltration media shall be visually inspected to ensure appropriate volume, texture and consistency with the approved drawings, and must bear a batch number marking from the manufacturer which certifies performance testing of the batch to meet or exceed the required infiltration rate (100 in/hr). A third-party laboratory test must be provided to certify the 100 in/hr rate.
- 2. At no additional cost and within the first year following installation, authorized valueadded reseller shall provide one site visit/maintenance training at the request of owner or owners representative. The owner or owners' rep will be supplied with the first round of replacement mulch by the reseller at no cost, so long as it occurs in the first year following installation.
- 3. Pollutant Removal performance, composition and characteristics of the Biofiltration Media must meet or exceed the following minimum standards as demonstrated by testing acceptable to the projectengineer:

Pollutant	Removal Efficiency		
TSS	91%		
Phosphorus	66%		
Nitrogen	48%		
Composition and	l Characteristics		
Sand - Fine	< 5%		
Sand – Medium	10% - 15%		

Sand – Coarse	15% - 25%				
Sand – Very Coarse	40% - 45%				
Gravel	10% - 20%				
Infiltration Rate	>100 inches per hour				
Peat Moss*	5% - 15%				
* Peat Moss Specification					
Listed by Organic Materials Review Institute					
100% natural peat (no composted, sludge, yard or leaf waste)					
Total Carbon >85%					
Carbon to Nitrogen Ratio 15:1 to 23:1					
Lignin Content 49% to 52%					
Humic Acid >18%					
pH 6.0 to 7.0					
Moisture Content 30% to 50%					
95% to 100% passing 2.0mm sieve					
> 80% passing 1.0mm sieve					

D. Underdrain/Storage System

- 1. Underdrain/storage components shall be manufactured in an ISO certified facility and be manufactured from at least 90% recycled materials.
- 2. Underdrain/storage components shall meet or exceed the following characteristics:

Property	Value		
Surface Void Area	≥ 85%		
Unit Weight	3.25 lbs/cf		
Service Temperature	-14° to 167°		
Unconfined Crush Strength	32.48 psi		
180 Day C	reep Test		
Load Applied – Initial and Sustained	11.16 psi		
Creep Sustained – After 180 Days	0.20 inches		
Creep Sustained – After 180 Days	1.13 %		
Projected Creep – 40 years	1.72%		

E. Separation Mesh

1. Separation Mesh shall be composed of high-tenacity monofilament polypropylene yarns that are woven together to produce an open mesh geotextile which shall be inert to biological degradation and resistant to naturally encountered chemicals, alkalis and acids. The mesh shall meet or exceed the following characteristics:

Properties	Test Method	Unit	Min Ave I	Roll Value
			MD	CD
Tensile Strength	ASTM D4595	kN/m (lbs/ft)	21 (1440)	25.3 (1733)

Creep Reduced Strength	ASTM D5262	kN/m (lbs/ft)	6.9 (471) 8.3 (566	
Long Term Allowable Design Load	GRI GG-4	kN/m (lbs/ft)	5.9 (407) 7.2 (490)	
UV Resistance (at 500 hours)	-	% strength retained	90	
Aperture Size (machine direction)	-	mm (in)	2 (0.08)	
Aperture Size (cross machine direction)	-	mm (in)	2 (0.08)	
Mass/Unit Area	ASTM D5261	g/m ² (oz/yd ²)	197 (5.8)	

F. Bridging Stone

- 1. Bridging Stone shall be 3/8" pea gravel, or other diameter sized to prevent migration of filter media, as specified by manufacturer.
- 2. Stone must be washed and free from sediment, soil and contaminants.

4.16 Construction Sequence

- 2. Prior to the start of *any* activity, it is the responsibility of the site's Developer (or Owner) to file a Notice of Intent (NOI) form and a copy of one (shared) Stormwater Pollution Prevention Plan (SWPPP) with the U.S. Environmental Protection Agency (EPA) in order to gain coverage under the NPDES General Permit for Stormwater Discharges from Construction Activities. A pre-construction meeting shall be held prior to the start of construction to discuss the SWPPP and all associated responsibilities. Participants shall include the developer (or owner), the General Contractor, the Site Contractor, and the Engineer.
- 3. Wetland boundaries shall be clearly marked by the project's land surveyor prior to the start of construction.
- 4. Cut and remove trees in construction area as required or directed.
- 5. Install silt fencing, and construction entrances prior to the start of earthwork. These shall be maintained until the final pavement surfacing and landscaping areas are established.
- 6. Clear, cut, grub, and dispose of debris in approved facilities. This includes any required demolition of existing structures, utilities, etc.
- 7. Construct and/or install temporary sediment basin(s) as required. These facilities shall be installed and stabilized prior to directing runoff to them.

APPENDIX I

EXISTING CONDITIONS DRAINAGE ANALYSIS

Summary 2 YEAR Summary 10 YEAR Complete 25 YEAR



Pre	epared by {	[enter y	our com	pany nar	me here	}	
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Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
1	2-YR STORM	Type III 24-hr		Default	24.00	1	3.08	2

Rainfall Events Listing (selected events)

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Area Listing (all nodes)

Area	CN	Description
(acres)		(subcatchment-numbers)
0.235	74	>75% Grass cover, Good, HSG C (3S)
0.286	96	Gravel surface, HSG C (1S, 2S, 3S)
0.188	98	Paved parking, HSG C (3S)
5.978	70	Woods, Good, HSG C (1S, 2S)
0.838	77	Woods, Good, HSG D (2S)
7.525	73	TOTAL AREA

Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
0.000	HSG B	
6.687	HSG C	1S, 2S, 3S
0.838	HSG D	2S
0.000	Other	
7.525		TOTAL AREA

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			Fip	e Listing	(an nou	63)			
Line#	Node	In-Invert	Out-Invert	Length	Slope	n	Width	Diam/Height	Inside-Fill
	Number	(feet)	(feet)	(feet)	(ft/ft)		(inches)	(inches)	(inches)
1	2S	0.00	0.00	22.0	0.0330	0.011	0.0	18.0	0.0

Pipe Listing (all nodes)

21137-PRE DEVELOPMENTType III 24-hr2-YR STORM Rainfall=3.08"Prepared by {enter your company name here}Printed 10/29/2021HydroCAD® 10.10-5a s/n 10589 © 2020 HydroCAD Software Solutions LLCPage 6

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S	Runoff Area=173,493 sf 0.00% Impervious Runoff Depth>0.80" Flow Length=350' Tc=9.6 min CN=71 Runoff=2.95 cfs 0.267 af
Subcatchment2S: Subcatchment2S	Runoff Area=134,265 sf 0.00% Impervious Runoff Depth>0.90" Flow Length=575' Tc=13.7 min CN=73 Runoff=2.35 cfs 0.232 af
Subcatchment3S: Subcatchment3S	Runoff Area=20,050 sf 40.93% Impervious Runoff Depth>1.73" Tc=6.0 min CN=86 Runoff=0.92 cfs 0.066 af
Reach AP1: Analysis Point #1	Inflow=5.17 cfs 0.499 af Outflow=5.17 cfs 0.499 af
Reach AP2: Analysis Point #2	Inflow=0.92 cfs 0.066 af Outflow=0.92 cfs 0.066 af

Total Runoff Area = 7.525 acRunoff Volume = 0.566 afAverage Runoff Depth = 0.90"97.50% Pervious = 7.337 ac2.50% Impervious = 0.188 ac

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Event#	Event	Storm Type	Curve	Mode	Duration	B/B	Depth	AMC
	Name				(hours)		(inches)	
1	10-YR STORM	Type III 24-hr		Default	24.00	1	4.63	2

Rainfall Events Listing (selected events)

21137-PRE DEVELOPMENTType III 24-hr10-YR STORM Rainfall=4.63"Prepared by {enter your company name here}Printed 10/29/2021HydroCAD® 10.10-5a s/n 10589 © 2020 HydroCAD Software Solutions LLCPage 8

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S	Runoff Area=173,493 sf 0.00% Impervious Runoff Depth>1.84" Flow Length=350' Tc=9.6 min CN=71 Runoff=7.34 cfs 0.610 af
Subcatchment 2S: Subcatchment 2S	Runoff Area=134,265 sf 0.00% Impervious Runoff Depth>1.99" Flow Length=575' Tc=13.7 min CN=73 Runoff=5.52 cfs 0.511 af
Subcatchment3S: Subcatchment3S	Runoff Area=20,050 sf 40.93% Impervious Runoff Depth>3.12" Tc=6.0 min CN=86 Runoff=1.63 cfs 0.120 af
Reach AP1: Analysis Point #1	Inflow=12.60 cfs 1.121 af Outflow=12.60 cfs 1.121 af
Reach AP2: Analysis Point #2	Inflow=1.63 cfs 0.120 af Outflow=1.63 cfs 0.120 af

Summary for Subcatchment 1S: Subcatchment 1S

Runoff = 7.34 cfs @ 12.15 hrs, Volume= 0.610 af, Depth> 1.84"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YR STORM Rainfall=4.63"

A	rea (sf)	CN I	Description		
1	69,441	70 \	Noods, Go	od, HSG C	
	4,052	96 (Gravel surfa	ace, HSG C	
1	73,493	71 \	Neighted A	verage	
1	73,493		100.00% Pe	ervious Are	а
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
6.1	50	0.1200	0.14		Sheet Flow, Sheet Flow
					Woods: Light underbrush n= 0.400 P2= 3.11"
3.5	300	0.0800	1.41		Shallow Concentrated Flow, Shallow Flow
					Woodland Kv= 5.0 fps
9.6	350	Total			

Summary for Subcatchment 2S: Subcatchment 2S

Runoff	=	5.52 cfs @	12.20 hrs,	Volume=	0.511 af,	Depth>	1.99"
		0	,		,	•	

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YR STORM Rainfall=4.63"

Α	rea (sf)	CN D	escription		
	90,962 36,501 3,547 3,255	70 W 77 W 96 G 96 G	Voods, Goo Voods, Goo Gravel surfa Gravel surfa	od, HSG C od, HSG D ace, HSG C ace, HSG C	
1	34,265 34,265	73 V 1	Veighted A 00.00% Pe	verage ervious Are	a
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.5	50	0.0400	0.09		Sheet Flow, Sheet Flow
0.5	50	0.0400	1.56		Woods: Light underbrush n= 0.400 P2= 3.11" Sheet Flow, Sheet Flow Gravel Smooth surfaces n= 0.011 P2= 3.11"
3.1	250	0.0720	1.34		Shallow Concentrated Flow, Shallow Flow
0.6	175	0.0460	5.11	170.24	Woodland Kv= 5.0 fps Parabolic Channel, Flow through Wetland W=100.00' D=0.50' Area=33.3 sf Perim=100.0'
0.0	22	0.0330	12.76	22.55	n= 0.030 Stream, clean & straight Pipe Channel, Culvert 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'
0.0	28	0.3800	30.38	121.51	Parabolic Channel, Channel Flow

W=6.00' D=1.00' Area=4.0 sf Perim=6.4'

		n= 0.022 Earth, clean & straight
13.7 575	Total	

Summary for Subcatchment 3S: Subcatchment 3S

Runoff = 1.63 cfs @ 12.09 hrs, Volume= 0.120 af, Depth> 3.12"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YR STORM Rainfall=4.63"

Area (sf) CN	Description		
10,2	53 74	>75% Gras	s cover, Go	ood, HSG C
1,5	91 96	Gravel surfa	ace, HSG C	C
8,2	06 98	Paved park	ing, HSG C	C
20,0	50 86	Weighted A	verage	
11,8	44	59.07% Pei	vious Area	a
8,2	06	40.93% Imp	pervious Are	rea
Tc ler	ath Slo	ne Velocitv	Capacity	Description
(min) (fe	eet) (ft	/ft) (ft/sec)	(cfs)	
6.0				Direct Entry,

Summary for Reach AP1: Analysis Point #1

[40] Hint: Not Described (Outflow=Inflow)

Inflow /	Area	=	7.065 ac,	0.00% Impervious, In	flow Depth > 1.9	90" for 10-YR STORM event
Inflow	:	=	12.60 cfs @	12.16 hrs, Volume=	1.121 af	
Outflov	N :	=	12.60 cfs @	12.16 hrs, Volume=	1.121 af,	Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach AP2: Analysis Point #2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	a =	0.460 ac, 40.	.93% Impervious	, Inflow Depth >	> 3.12"	for 10-YR ST	ORM event
Inflow	=	1.63 cfs @ 1	2.09 hrs, Volum	e= 0.12	0 af		
Outflow	=	1.63 cfs @ 1	2.09 hrs, Volum	e= 0.12	0 af, Atte	en= 0%, Lag= (0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

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Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
1	50-YR STORM	Type III 24-hr		Default	24.00	1	6.96	2

Rainfall Events Listing (selected events)

21137-PRE DEVELOPMENTType III 24-hr50-YR STORM Rainfall=6.96"Prepared by {enter your company name here}Printed10/29/2021HydroCAD® 10.10-5a s/n 10589 © 2020 HydroCAD Software Solutions LLCPage 12

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S	Runoff Area=173,493 sf 0.00% Impervious Runoff Depth>3.68" Flow Length=350' Tc=9.6 min CN=71 Runoff=15.02 cfs 1.223 af
Subcatchment2S: Subcatchment2S	Runoff Area=134,265 sf 0.00% Impervious Runoff Depth>3.89" Flow Length=575' Tc=13.7 min CN=73 Runoff=10.96 cfs 0.999 af
Subcatchment3S: Subcatchment3S	Runoff Area=20,050 sf 40.93% Impervious Runoff Depth>5.32" Tc=6.0 min CN=86 Runoff=2.72 cfs 0.204 af
Reach AP1: Analysis Point #1	Inflow=25.49 cfs 2.222 af Outflow=25.49 cfs 2.222 af
Reach AP2: Analysis Point #2	Inflow=2.72 cfs 0.204 af Outflow=2.72 cfs 0.204 af

APPENDIX II

PROPOSED CONDITIONS DRAINAGE ANALYSIS

Summary 2 YEAR Summary 10 YEAR Complete 25 YEAR


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Area Listing (all nodes)

Area	CN	Description
(acres)		(subcatchment-numbers)
1.891	74	>75% Grass cover, Good, HSG C (1S, 2S, 3S, 4S, 5S, 6S, 7S, 11S)
0.054	80	>75% Grass cover, Good, HSG D (6S)
0.114	96	Gravel surface, HSG C (6S)
1.555	98	Paved parking, HSG C (1S, 2S, 3S, 5S, 7S1, 7S2, 11S, 12S)
0.032	98	Paved parking, HSG D (7S2)
0.401	98	Roofs, HSG C (8S, 9S, 10S)
2.726	70	Woods, Good, HSG C (1S, 4S, 6S, 7S)
0.752	77	Woods, Good, HSG D (6S)
7.525	80	TOTAL AREA

Soil Listing (all nodes)

Area	a Soil	Subcatchment
(acres) Group	Numbers
0.00) HSG A	
0.00) HSG B	
6.68	7 HSG C	1S, 2S, 3S, 4S, 5S, 6S, 7S, 7S1, 7S2, 8S, 9S, 10S, 11S, 12S
0.83	B HSG D	6S, 7S2
0.00	O Other	
7.52	5	TOTAL AREA

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Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Width (inches)	Diam/Height (inches)	Inside-Fill (inches)
1	6S	0.00	0.00	50.0	0.1400	0.040	2.0	1.0	0.0
2	1P	223.60	223.42	35.0	0.0051	0.013	0.0	8.0	0.0
3	2P	220.80	220.50	48.0	0.0063	0.013	0.0	6.0	0.0
4	3P	210.50	210.30	26.0	0.0077	0.013	0.0	8.0	0.0
5	CB1	211.92	211.82	20.0	0.0050	0.013	0.0	15.0	0.0
6	CB2	211.72	211.62	20.0	0.0050	0.013	0.0	15.0	0.0
7	CB3	225.00	224.40	120.0	0.0050	0.013	0.0	12.0	0.0
8	FP1	225.66	225.56	10.0	0.0100	0.013	0.0	15.0	0.0
9	FP2	225.66	225.56	10.0	0.0100	0.013	0.0	15.0	0.0
10	FP3	222.49	222.39	10.0	0.0100	0.013	0.0	12.0	0.0
11	FP4	189.80	189.70	15.0	0.0067	0.013	0.0	6.0	0.0

Pipe Listing (all nodes)

21137 - POST DEV -W-FPType III 24-hr2-YR STORM Rainfall=3.08"Prepared by {enter your company name here}Printed 10/29/2021HydroCAD® 10.10-5a s/n 10589 © 2020 HydroCAD Software Solutions LLCPage 5

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S	Runoff Area=102,651 sf 0.77% Impervious Runoff Depth>0.85" Flow Length=350' Tc=9.6 min CN=72 Runoff=1.88 cfs 0.168 af
Subcatchment2S: Subcatchment2S	Runoff Area=17,857 sf 85.11% Impervious Runoff Depth>2.43" Tc=6.0 min CN=94 Runoff=1.10 cfs 0.083 af
Subcatchment3S: Subcatchment3S	Runoff Area=14,768 sf 90.79% Impervious Runoff Depth>2.63" Tc=6.0 min CN=96 Runoff=0.95 cfs 0.074 af
Subcatchment4S: Subcatchment4S	Runoff Area=12,745 sf 0.00% Impervious Runoff Depth>0.90" Flow Length=350' Tc=9.6 min CN=73 Runoff=0.25 cfs 0.022 af
Subcatchment 5S: Subcatchment 5S	Runoff Area=14,630 sf 78.26% Impervious Runoff Depth>2.33" Tc=6.0 min CN=93 Runoff=0.87 cfs 0.065 af
Subcatchment6S: Subcatchment6S	Runoff Area=104,590 sf 0.00% Impervious Runoff Depth>0.96" Flow Length=597' Tc=14.7 min CN=74 Runoff=1.91 cfs 0.191 af
Subcatchment7S: Subcatchment7S	Runoff Area=5,959 sf 0.00% Impervious Runoff Depth>0.96" Tc=6.0 min CN=74 Runoff=0.14 cfs 0.011 af
Subcatchment7S1: SubcatchmentCB1	Runoff Area=5,639 sf 100.00% Impervious Runoff Depth>2.85" Tc=6.0 min CN=98 Runoff=0.38 cfs 0.031 af
Subcatchment7S2: SubcatchmentCB2	Runoff Area=7,419 sf 100.00% Impervious Runoff Depth>2.85" Tc=6.0 min CN=98 Runoff=0.50 cfs 0.040 af
Subcatchment8S: Subcatchment8S	Runoff Area=5,280 sf 100.00% Impervious Runoff Depth>2.85" Tc=6.0 min CN=98 Runoff=0.35 cfs 0.029 af
Subcatchment9S: Subcatchment9S	Runoff Area=3,313 sf 100.00% Impervious Runoff Depth>2.85" Tc=6.0 min CN=98 Runoff=0.22 cfs 0.018 af
Subcatchment 10S: Subcatchment 10S	Runoff Area=8,865 sf 100.00% Impervious Runoff Depth>2.85" Tc=6.0 min CN=98 Runoff=0.59 cfs 0.048 af
Subcatchment11S: Subcatchment11S	Runoff Area=18,787 sf 52.98% Impervious Runoff Depth>1.81" Tc=6.0 min CN=87 Runoff=0.90 cfs 0.065 af
Subcatchment 12S: Subcatchment 11S	Runoff Area=5,279 sf 100.00% Impervious Runoff Depth>2.85" Tc=6.0 min CN=98 Runoff=0.35 cfs 0.029 af
Reach 1R: Flow Through Wetland n=0.030 L=2	Avg. Flow Depth=0.03' Max Vel=0.79 fps Inflow=0.32 cfs 0.063 af 10.0' S=0.0548 '/' Capacity=185.74 cfs Outflow=0.32 cfs 0.063 af
Reach AP1: Analysis Point #1	Inflow=4.84 cfs 0.699 af

Outflow=4.84 cfs 0.699 af

Reach AP2: Analysis Point #2

Type III 24-hr 2-YR STORM Rainfall=3.08" Printed 10/29/2021

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Inflow=0.90 cfs 0.065 af Outflow=0.90 cfs 0.065 af

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Pond 1P: STORMTECH1	Peak Elev=224.20' Storage=0.045 af Inflow=2.61 cfs 0.157 af Discarded=0.00 cfs 0.000 af Primary=0.62 cfs 0.149 af Outflow=0.62 cfs 0.149 af
Dand 2D: STORMTECH 2	Peak Elev-221 25' Storage-0.013 of Inflow-1.18 of 0.065 of
FOND 2F. STORWIECH2	Discarded=0.00 cfs 0.000 af Primary=0.32 cfs 0.063 af Outflow=0.32 cfs 0.063 af
Pond 3P: Pond 3P	Peak Elev=212.73' Storage=1,786 cf Inflow=1.02 cfs 0.082 af
	Outflow=0.08 cfs 0.075 af
Pond 4P: Drip Edge	Peak Elev=230.24' Storage=406 cf Inflow=0.35 cfs 0.029 af
	Discarded=0.04 cfs 0.029 af Primary=0.00 cfs 0.000 af Outflow=0.04 cfs 0.029 af
Pond 5P: Drip Edge	Peak Elev=229.79' Storage=225 cf Inflow=0.22 cfs 0.018 af
	Discarded=0.03 cfs 0.018 af Primary=0.00 cfs 0.000 af Outflow=0.03 cfs 0.018 af
Pond 6P: Drip Edge	Peak Elev=222.00' Storage=1,872 cf Inflow=0.59 cfs 0.048 af
	Outflow=0.02 cfs 0.005 af
Pond CB1: CB1	Peak Elev=212.73' Inflow=0.38 cfs 0.031 af
	15.0" Round Culvert n=0.013 L=20.0' S=0.0050 '/' Outflow=0.38 cfs 0.031 af
Pond CB2: CB2	Peak Elev=212.73' Inflow=0.87 cfs 0.071 af
	15.0" Round Culvert n=0.013 L=20.0' S=0.0050 '/' Outflow=0.87 cfs 0.071 af
Pond CB3: CB3	Peak Elev=225.29' Inflow=0.25 cfs 0.022 af
	12.0" Round Culvert n=0.013 L=120.0' S=0.0050 '/' Outflow=0.25 cfs 0.022 af
Pond FP1: FocalPoint 1	Peak Elev=230.05' Storage=347 cf Inflow=1.10 cfs 0.083 af
	Outflow=1.77 cfs 0.083 af
Pond FP2: FocalPoint 2	Peak Elev=229.95' Storage=346 cf Inflow=0.95 cfs 0.074 af
	Outflow=0.91 cfs 0.074 af
Pond FP3: FocalPoint 3	Peak Elev=226.92' Storage=346 cf Inflow=0.87 cfs 0.065 af
	Outflow=1.18 cfs 0.065 af
Pond FP4: FocalPoint 4	Peak Elev=193.02' Storage=224 cf Inflow=0.35 cfs 0.029 af
	Outflow=0.19 cfs 0.025 af
Total Runo	ff Area = 7.525 ac Runoff Volume = 0.874 af Average Runoff Depth = 1.39" 73.58% Pervious = 5.537 ac 26.42% Impervious = 1.988 ac

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S	Runoff Area=102,651 sf 0.77% Impervious Runoff Depth>0.29" Flow Length=350' Tc=9.6 min CN=72 Runoff=0.45 cfs 0.057 af
Subcatchment2S: Subcatchment2S	Runoff Area=17,857 sf 85.11% Impervious Runoff Depth>1.40" Tc=6.0 min CN=94 Runoff=0.65 cfs 0.048 af
Subcatchment3S: Subcatchment3S	Runoff Area=14,768 sf 90.79% Impervious Runoff Depth>1.57" Tc=6.0 min CN=96 Runoff=0.59 cfs 0.044 af
Subcatchment4S: Subcatchment4S	Runoff Area=12,745 sf 0.00% Impervious Runoff Depth>0.32" Flow Length=350' Tc=9.6 min CN=73 Runoff=0.07 cfs 0.008 af
Subcatchment5S: Subcatchment5S	Runoff Area=14,630 sf 78.26% Impervious Runoff Depth>1.31" Tc=6.0 min CN=93 Runoff=0.50 cfs 0.037 af
Subcatchment6S: Subcatchment6S	Runoff Area=104,590 sf 0.00% Impervious Runoff Depth>0.35" Flow Length=597' Tc=14.7 min CN=74 Runoff=0.55 cfs 0.070 af
Subcatchment7S: Subcatchment7S	Runoff Area=5,959 sf 0.00% Impervious Runoff Depth>0.35" Tc=6.0 min CN=74 Runoff=0.04 cfs 0.004 af
Subcatchment7S1: SubcatchmentCB1	Runoff Area=5,639 sf 100.00% Impervious Runoff Depth>1.77" Tc=6.0 min CN=98 Runoff=0.24 cfs 0.019 af
Subcatchment7S2: SubcatchmentCB2	Runoff Area=7,419 sf 100.00% Impervious Runoff Depth>1.77" Tc=6.0 min CN=98 Runoff=0.32 cfs 0.025 af
Subcatchment8S: Subcatchment8S	Runoff Area=5,280 sf 100.00% Impervious Runoff Depth>1.77" Tc=6.0 min CN=98 Runoff=0.23 cfs 0.018 af
Subcatchment9S: Subcatchment9S	Runoff Area=3,313 sf 100.00% Impervious Runoff Depth>1.77" Tc=6.0 min CN=98 Runoff=0.14 cfs 0.011 af
Subcatchment10S: Subcatchment10S	Runoff Area=8,865 sf 100.00% Impervious Runoff Depth>1.77" Tc=6.0 min CN=98 Runoff=0.38 cfs 0.030 af
Subcatchment11S: Subcatchment11S	Runoff Area=18,787 sf 52.98% Impervious Runoff Depth>0.90" Tc=6.0 min CN=87 Runoff=0.45 cfs 0.033 af
Subcatchment 12S: Subcatchment 11S	Runoff Area=5,279 sf 100.00% Impervious Runoff Depth>1.77" Tc=6.0 min CN=98 Runoff=0.23 cfs 0.018 af
Reach 1R: Flow Through Wetland n=0.030 L=2	Avg. Flow Depth=0.02' Max Vel=0.66 fps Inflow=0.18 cfs 0.035 af 10.0' S=0.0548 '/' Capacity=185.74 cfs Outflow=0.18 cfs 0.035 af
Reach AP1: Analysis Point #1	Inflow=1.59 cfs_0.314 af

Outflow=1.59 cfs 0.314 af

Reach AP2: Analysis Point #2

Type III 24-hr FP1 Rainfall=2.00" Printed 10/29/2021 LC Page 8

Inflow=0.45 cfs 0.033 af

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-	Outflow=0.45 cfs 0.033 af
Pond 1P: STORMTECH1	Peak Elev=224.01' Storage=0.031 af Inflow=0.44 cfs 0.092 af Discarded=0.00 cfs 0.000 af Primary=0.34 cfs 0.085 af Outflow=0.34 cfs 0.085 af
Pond 2P: STORMTECH 2	Peak Elev=221.11' Storage=0.009 af Inflow=0.20 cfs 0.037 af Discarded=0.00 cfs 0.000 af Primary=0.18 cfs 0.035 af Outflow=0.18 cfs 0.035 af
Pond 3P: Pond 3P	Peak Elev=212.35' Storage=1,001 cf Inflow=0.60 cfs 0.048 af Outflow=0.07 cfs 0.044 af
Pond 4P: Drip Edge	Peak Elev=229.60' Storage=211 cf Inflow=0.23 cfs 0.018 af Discarded=0.04 cfs 0.018 af Primary=0.00 cfs 0.000 af Outflow=0.04 cfs 0.018 af
Pond 5P: Drip Edge	Peak Elev=229.33' Storage=110 cf Inflow=0.14 cfs 0.011 af Discarded=0.03 cfs 0.011 af Primary=0.00 cfs 0.000 af Outflow=0.03 cfs 0.011 af
Pond 6P: Drip Edge	Peak Elev=221.07' Storage=1,310 cf Inflow=0.38 cfs 0.030 af Outflow=0.00 cfs 0.000 af
Pond CB1: CB1	Peak Elev=212.35' Inflow=0.24 cfs 0.019 af 15.0" Round Culvert n=0.013 L=20.0' S=0.0050 '/' Outflow=0.24 cfs 0.019 af
Pond CB2: CB2	Peak Elev=212.35' Inflow=0.56 cfs 0.044 af 15.0" Round Culvert n=0.013 L=20.0' S=0.0050 '/' Outflow=0.56 cfs 0.044 af
Pond CB3: CB3	Peak Elev=225.15' Inflow=0.07 cfs 0.008 af 12.0" Round Culvert n=0.013 L=120.0' S=0.0050 '/' Outflow=0.07 cfs 0.008 af
Pond FP1: FocalPoint 1	Peak Elev=229.83' Storage=344 cf Inflow=0.65 cfs 0.048 af Outflow=0.23 cfs 0.048 af
Pond FP2: FocalPoint 2	Peak Elev=229.67' Storage=286 cf Inflow=0.59 cfs 0.044 af Outflow=0.21 cfs 0.044 af
Pond FP3: FocalPoint 3	Peak Elev=226.38' Storage=203 cf Inflow=0.50 cfs 0.037 af Outflow=0.20 cfs 0.037 af
Pond FP4: FocalPoint 4	Peak Elev=192.83' Storage=157 cf Inflow=0.23 cfs 0.018 af Outflow=0.19 cfs 0.015 af
Total Runo	off Area = 7.525 ac Runoff Volume = 0.421 af Average Runoff Depth = 0.67 "

Total Runoff Area = 7.525 ac Runoff Volume = 0.421 af Average Runoff Depth = 0.67" 73.58% Pervious = 5.537 ac 26.42% Impervious = 1.988 ac Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S	Runoff Area=102,651 sf 0.77% Impervious Runoff Depth>1.91" Flow Length=350' Tc=9.6 min CN=72 Runoff=4.54 cfs 0.376 af
Subcatchment2S: Subcatchment2S	Runoff Area=17,857 sf 85.11% Impervious Runoff Depth>3.94" Tc=6.0 min CN=94 Runoff=1.73 cfs 0.135 af
Subcatchment3S: Subcatchment3S	Runoff Area=14,768 sf 90.79% Impervious Runoff Depth>4.16" Tc=6.0 min CN=96 Runoff=1.47 cfs 0.118 af
Subcatchment4S: Subcatchment4S	Runoff Area=12,745 sf 0.00% Impervious Runoff Depth>1.99" Flow Length=350' Tc=9.6 min CN=73 Runoff=0.59 cfs 0.049 af
Subcatchment5S: Subcatchment5S	Runoff Area=14,630 sf 78.26% Impervious Runoff Depth>3.83" Tc=6.0 min CN=93 Runoff=1.39 cfs 0.107 af
Subcatchment6S: Subcatchment6S	Runoff Area=104,590 sf 0.00% Impervious Runoff Depth>2.07" Flow Length=597' Tc=14.7 min CN=74 Runoff=4.38 cfs 0.413 af
Subcatchment7S: Subcatchment7S	Runoff Area=5,959 sf 0.00% Impervious Runoff Depth>2.07" Tc=6.0 min CN=74 Runoff=0.32 cfs 0.024 af
Subcatchment7S1: SubcatchmentCB1	Runoff Area=5,639 sf 100.00% Impervious Runoff Depth>4.39" Tc=6.0 min CN=98 Runoff=0.57 cfs 0.047 af
Subcatchment7S2: SubcatchmentCB2	Runoff Area=7,419 sf 100.00% Impervious Runoff Depth>4.39" Tc=6.0 min CN=98 Runoff=0.75 cfs 0.062 af
Subcatchment8S: Subcatchment8S	Runoff Area=5,280 sf 100.00% Impervious Runoff Depth>4.39" Tc=6.0 min CN=98 Runoff=0.54 cfs 0.044 af
Subcatchment9S: Subcatchment9S	Runoff Area=3,313 sf 100.00% Impervious Runoff Depth>4.39" Tc=6.0 min CN=98 Runoff=0.34 cfs 0.028 af
Subcatchment10S: Subcatchment10S	Runoff Area=8,865 sf 100.00% Impervious Runoff Depth>4.39" Tc=6.0 min CN=98 Runoff=0.90 cfs 0.074 af
Subcatchment11S: Subcatchment11S	Runoff Area=18,787 sf 52.98% Impervious Runoff Depth>3.22" Tc=6.0 min CN=87 Runoff=1.57 cfs 0.116 af
Subcatchment 12S: Subcatchment 11S	Runoff Area=5,279 sf 100.00% Impervious Runoff Depth>4.39" Tc=6.0 min CN=98 Runoff=0.54 cfs 0.044 af
Reach 1R: Flow Through Wetland n=0.030 L=2	Avg. Flow Depth=0.03' Max Vel=0.92 fps Inflow=0.52 cfs 0.105 af 10.0' S=0.0548 '/' Capacity=185.74 cfs Outflow=0.52 cfs 0.105 af
Reach AP1: Analysis Point #1	Inflow=10.88 cfs 1.372 af

Outflow=10.88 cfs 1.372 af

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Reach AP2: Analysis Poir	t #2 Inflow=1.57 cfs 0.116 a Outflow=1.57 cfs 0.116 a	af af
Pond 1P: STORMTECH1	Peak Elev=224.59' Storage=0.072 af Inflow=3.31 cfs 0.252 a Discarded=0.00 cfs 0.000 af Primary=1.02 cfs 0.242 af Outflow=1.02 cfs 0.242 a	af af
Pond 2P: STORMTECH 2	Peak Elev=221.63' Storage=0.023 af Inflow=1.81 cfs 0.107 a Discarded=0.00 cfs 0.000 af Primary=0.52 cfs 0.105 af Outflow=0.52 cfs 0.105 a	af af
Pond 3P: Pond 3P	Peak Elev=213.08' Storage=2,566 cf Inflow=1.65 cfs 0.133 a Outflow=0.51 cfs 0.114 a	af af
Pond 4P: Drip Edge	Peak Elev=231.29' Storage=724 cf Inflow=0.54 cfs 0.044 a Discarded=0.05 cfs 0.044 af Primary=0.00 cfs 0.000 af Outflow=0.05 cfs 0.044 a	af af
Pond 5P: Drip Edge	Peak Elev=230.50' Storage=407 cf Inflow=0.34 cfs 0.028 a Discarded=0.04 cfs 0.028 af Primary=0.00 cfs 0.000 af Outflow=0.04 cfs 0.028 a	af af
Pond 6P: Drip Edge	Peak Elev=222.01' Storage=1,875 cf Inflow=0.90 cfs 0.074 a Outflow=0.42 cfs 0.032 a	af af
Pond CB1: CB1	Peak Elev=213.08' Inflow=0.57 cfs 0.047 a 15.0" Round Culvert n=0.013 L=20.0' S=0.0050 '/' Outflow=0.57 cfs 0.047 a	af af
Pond CB2: CB2	Peak Elev=213.08' Inflow=1.32 cfs 0.110 a 15.0" Round Culvert n=0.013 L=20.0' S=0.0050 '/' Outflow=1.32 cfs 0.110 a	af af
Pond CB3: CB3	Peak Elev=225.45' Inflow=0.59 cfs 0.049 a 12.0" Round Culvert n=0.013 L=120.0' S=0.0050 '/' Outflow=0.59 cfs 0.049 a	af af
Pond FP1: FocalPoint 1	Peak Elev=230.07' Storage=348 cf Inflow=1.73 cfs 0.135 a Outflow=1.88 cfs 0.135 a	af af
Pond FP2: FocalPoint 2	Peak Elev=230.02' Storage=347 cf Inflow=1.47 cfs 0.118 a Outflow=1.44 cfs 0.118 a	af af
Pond FP3: FocalPoint 3	Peak Elev=226.99' Storage=348 cf Inflow=1.39 cfs 0.107 a Outflow=1.81 cfs 0.107 a	af af
Pond FP4: FocalPoint 4	Peak Elev=193.84' Storage=344 cf Inflow=0.54 cfs 0.044 a	af

Total Runoff Area = 7.525 acRunoff Volume = 1.637 afAverage Runoff Depth = 2.61"73.58% Pervious = 5.537 ac26.42% Impervious = 1.988 ac

Outflow=0.33 cfs 0.041 af

Summary for Subcatchment 1S: Subcatchment 1S

Runoff = 4.54 cfs @ 12.14 hrs, Volume= 0.376 af, Depth> 1.91"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YR STORM Rainfall=4.63"

A	rea (sf)	CN I	Description				
	48,626	70	Woods, Good, HSG C				
	8,966	70	Noods, Go	od, HSG C			
	6,940	70	Noods, Go	od, HSG C			
	794	98	Paved park	ing, HSG C			
	36,539	74 🔅	>75% Gras	s cover, Go	ood, HSG C		
	786	74 :	>75% Gras	s cover, Go	ood, HSG C		
1	02,651	72	Neighted A	verage			
1	01,857	ę	99.23% Pei	vious Area			
	794	().77% Impe	ervious Area	а		
Тс	Length	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
6.1	50	0.1200	0.14		Sheet Flow, Sheet Flow		
					Woods: Light underbrush n= 0.400 P2= 3.11"		
3.5	300	0.0800	1.41		Shallow Concentrated Flow, Shallow Flow		
					Woodland Kv= 5.0 fps		
9.6	350	Total					

Summary for Subcatchment 2S: Subcatchment 2S

Runoff = 1.73 cfs @ 12.09 hrs, Volume= 0.135 af, Depth> 3.94"

A	rea (sf)	CN	Description		
	14,373	98	Paved park	ing, HSG C	C
	825	98	Paved park	ing, HSG C	С
	1,360	74	>75% Gras	s cover, Go	Good, HSG C
	1,299	74	>75% Gras	s cover, Go	Good, HSG C
	17,857	94	Weighted A	verage	
	2,659		14.89% Per	vious Area	а
	15,198		85.11% Imp	pervious Ar	rea
Тс	Length	Slop	e Velocity	Capacity	Description
(min)	(feet)	(ft/f	t) (ft/sec)	(cfs)	
6.0					Direct Entry,

Summary for Subcatchment 3S: Subcatchment 3S

Runoff = 1.47 cfs @ 12.09 hrs, Volume= 0.118 af, Depth> 4.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YR STORM Rainfall=4.63"

Ar	rea (sf)	CN	Description			
	13,408	98	Paved park	ing, HSG C	2	
	1,360	74	>75% Gras	s cover, Go	ood, HSG C	
Ta	14,768 1,360 13,408	96 Slan	Weighted Average 9.21% Pervious Area 90.79% Impervious Area			
IC (min)	Length (feet)	Siope (ft/ft	e Velocity	Capacity (cfs)	Description	
6.0	(1001)	(1010	, (1000)	(010)	Direct Entry.	
0.0					_ · · · · · _ · · · · , ,	

Summary for Subcatchment 4S: Subcatchment 4S

Runoff	=	0.59 cfs @	12.14 hrs,	Volume=	0.049 af,	Depth>	1.99"
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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YR STORM Rainfall=4.63"

A	rea (sf)	CN [Description						
	3,468	70 \	Noods, Good, HSG C						
	9,277	74 >	>75% Gras	s cover, Go	bod, HSG C				
	12,745	73 \	Neighted A	verage					
	12,745		100.00% Pe	ervious Are	а				
Tc	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
6.1	50	0.1200	0.14		Sheet Flow, Sheet Flow				
					Woods: Light underbrush n= 0.400 P2= 3.11"				
3.5	300	0.0800	1.41		Shallow Concentrated Flow, Shallow Flow				
					Woodland Kv= 5.0 fps				
9.6	350	Total							

Summary for Subcatchment 5S: Subcatchment 5S

Runoff = 1.39 cfs @ 12.09 hrs, Volume= 0.107 af, Depth> 3.83"

Type III 24-hr 10-YR STORM Rainfall=4.63" Printed 10/29/2021

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Are	a (sf)	CN	Description						
1(0,386	98	Paved park	ing, HSG C	;				
	1,064	98	Paved park	ing, HSG C)				
	2,992	74	>75% Gras	s cover, Go	ood, HSG C				
	188	74	>75% Gras	s cover, Go	ood, HSG C				
14	4,630	93	Weighted A	verage					
:	3,180		21.74% Per	vious Area					
1 ⁻	1,450		78.26% Imp	ervious Ar	ea				
Tc L	_ength	Slop	e Velocity	Capacity	Description				
(min)	(feet)	(ft/ft	:) (ft/sec)	(cfs)					
6.0					Direct Entry,				

Summary for Subcatchment 6S: Subcatchment 6S

Runoff = 4.38 cfs @ 12.21 hrs, Volume= 0.413 af, Depth> 2.07"

A	rea (sf)	CN E	Description						
	31,117	70 V	Woods, Good, HSG C						
	18,906	70 V	Voods, Go	od, HSG C					
	4,969	96 G	Gravel surfa	ace, HSG C					
	12,429	74 >	75% Gras	s cover, Go	ood, HSG C				
	2,075	74 >	75% Gras	s cover, Go	ood, HSG C				
	2,358	80 >	75% Gras	s cover, Go	ood, HSG D				
	32,736	77 V	Voods, Go	od, HSG D					
1	04,590	74 V	Veighted A	verage					
1	04,590	1	00.00% Pe	ervious Are	а				
Тс	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
9.5	50	0.0400	0.09		Sheet Flow, Sheet Flow				
					Woods: Light underbrush n= 0.400 P2= 3.11"				
0.5	50	0.0400	1.56		Sheet Flow, Sheet over Gravel				
					Smooth surfaces n= 0.011 P2= 3.11"				
3.1	250	0.0720	1.34		Shallow Concentrated Flow, Shallow Flow				
					Woodland Kv= 5.0 fps				
0.6	175	0.0460	5.11	170.24	Parabolic Channel, Flow through Wetland				
					W=100.00' D=0.50' Area=33.3 sf Perim=100.0'				
07	50	0 4 4 0 0	4.07	0.00	n= 0.030 Stream, clean & straight				
0.7	50	0.1400	1.27	0.02	Pipe Channel, Culvert				
					2.0° X 1.0° Box Area= 0.0 st Perim= 0.5° r= 0.03°				
0.0	22	0 4 0 0 0	1 00	0.05	n= 0.040 Earth, cobble bottom, clean sides				
0.3	22	0.1200	1.23	0.05	Marabolic Channel,				
					W = 0.00 D=0.10 Alea = 0.3 SI Felilite = 0.0				
	507	Tatal							
14.7	597	i otai							

Summary for Subcatchment 7S: Subcatchment 7S

Runoff = 0.32 cfs @ 12.10 hrs, Volume= 0.024 af, Depth> 2.07"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YR STORM Rainfall=4.63"

A	rea (sf)	CN	Description		
	740	70	Woods, Go	od, HSG C	
	5,219	74	>75% Gras	s cover, Go	ood, HSG C
	5,959	74	Weighted A	verage	
	5,959		100.00% Pe	ervious Are	ea
Tc	Length	Slop	e Velocity	Capacity	Description
(min)	(feet)	(ft/f	t) (ft/sec)	(cfs)	
6.0					Direct Entry,
					•

Summary for Subcatchment 7S1: Subcatchment CB1

Runoff = 0.57 cfs @ 12.09 hrs, Volume= 0.047 af, Depth> 4.39"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YR STORM Rainfall=4.63"

A	rea (sf)	CN I	Description				
	5,639	98 I	Paved park	ing, HSG C	0		
	5,639		100.00% Impervious Area				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
6.0					Direct Entry,		

Summary for Subcatchment 7S2: Subcatchment CB2

Runoff = 0.75 cfs @ 12.09 hrs, Volume= 0.062 af, Depth> 4.39"

A	rea (sf)	CN	Description		
	6,012	98	Paved park	ing, HSG C	
	1,407	98	Paved park	ing, HSG D	
	7,419	98	Weighted A	verage	
	7,419		100.00% Im	npervious A	Area
Tc	Length	Slope	e Velocity	Capacity	Description
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)	
6.0					Direct Entry,

Summary for Subcatchment 8S: Subcatchment 8S

Runoff = 0.54 cfs @ 12.09 hrs, Volume= 0.044 af, Depth> 4.39"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YR STORM Rainfall=4.63"

A	rea (sf)	CN	Description					
	5,280	98	Roofs, HSC	G C				
	5,280		100.00% Impervious Area					
Tc	Length	Slop	e Velocity	Capacity	Description			
(min)	(feet)	(ft/f	t) (ft/sec)	(cfs)				
6.0					Direct Entry,			
		0.			takmant 00. Cukaatakmant 00			

Summary for Subcatchment 9S: Subcatchment 9S

Runoff = 0.34 cfs @ 12.09 hrs, Volume= 0.028 af, Depth> 4.39"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YR STORM Rainfall=4.63"

A	rea (sf)	CN	Description		
	3,313	98	Roofs, HSC	G C	
	3,313		100.00% In	npervious A	Area
Tc (min)	Length (feet)	Slope (ft/ft	e Velocity) (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Summary for Subcatchment 10S: Subcatchment 10S

Runoff = 0.90 cfs @ 12.09 hrs, Volume= 0.074 af, Depth> 4.39"

A	rea (sf)	CN I	Description		
	8,865	98 I	Roofs, HSG	G C	
	8,865		100.00% In	npervious A	Area
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Summary for Subcatchment 11S: Subcatchment 11S

Runoff = 1.57 cfs @ 12.09 hrs, Volume= 0.116 af, Depth> 3.22"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YR STORM Rainfall=4.63"

A	rea (sf)	CN	Description					
	9,953	98	Paved park	ing, HSG C	C			
	3,298	74	>75% Gras	s cover, Go	lood, HSG C			
	5,536	74	>75% Gras	75% Grass cover, Good, HSG C				
	18,787	87	Weighted A	verage				
	8,834		47.02% Per	7.02% Pervious Area				
	9,953		52.98% Imp	2.98% Impervious Area				
Tc	Length	Slop	e Velocity	Capacity	Description			
(min)	(teet)	(π/τ	t) (11/sec)	(CIS)				
6.0					Direct Entry,			

Summary for Subcatchment 12S: Subcatchment 11S

Runoff = 0.54 cfs @ 12.09 hrs, Volume= 0.044 af, Depth> 4.39"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YR STORM Rainfall=4.63"

Α	rea (sf)	CN [Description		
	5,279	98 F	Paved park	ing, HSG C	2
	5,279		00.00% In	npervious A	Area
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Summary for Reach 1R: Flow Through Wetland

Inflow Area = Inflow = Outflow =	0.412 ac, 8 0.52 cfs @ 0.52 cfs @	2.28% Impervious 12.32 hrs, Volum 12.39 hrs, Volum	, Inflow Depth > e= 0.105 e= 0.105	3.05" 5 af 5 af, Atte	for 10-Y en= 0%, I	R STORM event ₋ag= 4.3 min
Routing by Dyn-Sto Max. Velocity= 0.9 Avg. Velocity = 0.4	or-Ind method 2 fps, Min. Tr 2 fps, Avg. T	, Time Span= 0.00 avel Time= 3.8 mi ravel Time= 8.2 m)-24.00 hrs, dt= (n in	0.05 hrs		
Peak Storage= 119 Average Depth at I Bank-Full Depth= (9 cf @ 12.39 h Peak Storage).50' Flow Are	ırs = 0.03' , Surface V ea= 33.3 sf, Capa	/idth= 25.72' city= 185.74 cfs			

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100.00' x 0.50' deep Parabolic Channel, n= 0.030 Stream, clean & straight Length= 210.0' Slope= 0.0548 '/' Inlet Invert= 220.50', Outlet Invert= 209.00'



Summary for Reach AP1: Analysis Point #1

Inflow A	rea =	7.094 ac, 24.80% Impervious	, Inflow Depth > 2.3	2" for 10-YR STORM event
Inflow	=	10.88 cfs @ 12.17 hrs, Volum	ne= 1.372 af	
Outflow	=	10.88 cfs @ 12.17 hrs, Volum	ne= 1.372 af,	Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach AP2: Analysis Point #2

Inflow A	rea =	0.431 ac, 52.98% Impervious, Inflow	Depth > 3.22" for 10-YR STORM eve	ent
Inflow	=	1.57 cfs @ 12.09 hrs, Volume=	0.116 af	
Outflow	=	1.57 cfs @ 12.09 hrs, Volume=	0.116 af, Atten= 0%, Lag= 0.0 min	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Pond 1P: STORMTECH 1

Inflow Area	a =	0.749 ac, 8	7.68% Imp	ervious,	Inflow	Depth >	4.04"	for 1	0-YF	R STO	RM event
Inflow	=	3.31 cfs @	12.09 hrs,	Volume	=	0.252	af				
Outflow	=	1.02 cfs @	12.39 hrs,	Volume	=	0.242	af, Atte	en= 69	9%, L	_ag= 1	7.9 min
Discarded	=	0.00 cfs @	0.00 hrs,	Volume	=	0.000	af			-	
Primary	=	1.02 cfs @	12.39 hrs,	Volume	=	0.242	af				

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 224.59' @ 12.39 hrs Surf.Area= 0.066 ac Storage= 0.072 af

Plug-Flow detention time= 80.3 min calculated for 0.242 af (96% of inflow) Center-of-Mass det. time= 57.9 min (833.9 - 776.0)

Volume	Invert	Avail.Stora	ge Storage Description
#1	223.60'	0.135	af ADS_StormTech SC-740 +Cap x 128 Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap 128 Chambers in 8 Rows
Device	Routing	Invert	Outlet Devices
#1	Primary	223.60'	8.0" Round Culvert

L= 35.0'	CPP, projecting, no	headwall,	Ke= 0.900	
Inlet / Ou	tlet Invert= 223.60' /	223.42' S	S= 0.0051 '/'	Cc= 0.900

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n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.35 sf #2 Discarded

223.60' 2.000 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 220.83'

Discarded OutFlow Max=0.00 cfs @ 0.00 hrs HW=223.60' (Free Discharge) -2=Exfiltration (Controls 0.00 cfs)

Summary for Pond 2P: STORMTECH 2

Inflow Area	=	0.412 ac, 8	2.28% Imp	ervious,	Inflow	Depth >	3.1	2" foi	⁻ 10-Y	R STO	RM event
Inflow	=	1.81 cfs @	12.06 hrs,	Volume	=	0.107	af				
Outflow	=	0.52 cfs @	12.32 hrs,	Volume	=	0.105	af,	Atten=	71%,	Lag= 1	5.9 min
Discarded	=	0.00 cfs @	0.00 hrs,	Volume	=	0.000	af				
Primary	=	0.52 cfs @	12.32 hrs,	Volume	=	0.105	af				

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 221.63' @ 12.32 hrs Surf.Area= 0.026 ac Storage= 0.023 af

Plug-Flow detention time= 48.3 min calculated for 0.105 af (98% of inflow) Center-of-Mass det. time= 34.5 min (821.1 - 786.6)

Volume	Invert	Avail.Storag	ge Storage Description
#1	220.80'	0.051	af ADS_StormTech SC-740 +Cap x 48 Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap 48 Chambers in 8 Rows
Device	Routing	Invert	Outlet Devices
#1	Discarded	220.80'	2.000 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 215.39'
#2	Primary	220.80'	6.0" Round Culvert L= 48.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 220.80' / 220.50' S= 0.0063 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.20 sf

Discarded OutFlow Max=0.00 cfs @ 0.00 hrs HW=220.80' (Free Discharge) 1=Exfiltration (Controls 0.00 cfs)

Primary OutFlow Max=0.52 cfs @ 12.32 hrs HW=221.63' TW=220.53' (Dynamic Tailwater) ←2=Culvert (Barrel Controls 0.52 cfs @ 2.66 fps)

Summary for Pond 3P: Pond 3P

Inflow Area	=	0.437 ac, 6	8.66% Impervious	s, Inflow De	pth > 3.66"	for 10-YR ST	ORM event
Inflow	=	1.65 cfs @	12.09 hrs, Volun	ne=	0.133 af		
Outflow	=	0.51 cfs @	12.41 hrs, Volun	ne=	0.114 af, At	ten= 69%, Lag=	: 19.5 min
Primary	=	0.51 cfs @	12.41 hrs, Volun	ne=	0.114 af		

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

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Starting Elev= 129.08' Storage= 0 cf Peak Elev= 213.08' @ 12.41 hrs Surf.Area= 2,363 sf Storage= 2,566 cf

Plug-Flow detention time= 249.3 min calculated for 0.114 af (86% of inflow) Center-of-Mass det. time= 185.6 min (950.9 - 765.3)

Volume	Inv	ert Avail.	Storage	Storage	Description		
#1	210.4	49'	6,106 cf	Custom	Stage Data (Irreg	ular)Listed below (F	Recalc)
Elevatio	on	Surf.Area	Perim.	Voids	Inc.Store	Cum.Store	Wet.Area
(fee	et)	(sq-ft)	(feet)	(%)	(cubic-feet)	(cubic-feet)	(sq-ft)
210.4	49	930	153.0	0.0	0	0	930
210.5	50	930	153.0	40.0	4	4	932
212.0	00	1,720	190.0	40.0	783	787	1,974
212.0)1	1,720	190.0	5.0	1	788	1,976
212.2	25	1,863	195.0	5.0	21	809	2,136
212.2	26	2,010	200.0	100.0	19	828	2,293
212.5	51	2,010	200.0	100.0	503	1,331	2,343
213.0	00	2,316	210.0	100.0	1,059	2,390	2,684
213.8	30	2,835	234.0	100.0	2,057	4,447	3,551
214.0	00	3,900	254.0	100.0	671	5,117	4,329
214.2	25	4,010	256.0	100.0	989	6,106	4,432
Device	Routing	Inv	ert Outle	et Devices	6		
#1	Primary	210.	50' 8.0''	Round (Culvert		
	-		L= 2	6.0' CPF	P, projecting, no hea	adwall, Ke= 0.900	
			Inlet	/ Outlet In	nvert= 210.50' / 210	0.30' S= 0.0077 '/'	Cc= 0.900
			n= 0	.013 Cor	rugated PE, smootl	h interior, Flow Are	a= 0.35 sf
#2	Device 1	210.8	83' 1.5"	Vert. Ori	fice/Grate C= 0.6	00 Limited to weir	flow at low heads
#3	Device 1	213.0	00' 24.0	" Horiz. C	Drifice/Grate C= 0	0.600	
			Limit	ed to wei	r flow at low heads		

Primary OutFlow Max=0.51 cfs @ 12.41 hrs HW=213.07' TW=0.00' (Dynamic Tailwater)

_1=Culvert (Passes 0.51 cfs of 1.99 cfs potential flow)

2=Orifice/Grate (Orifice Controls 0.09 cfs @ 7.11 fps)

-3=Orifice/Grate (Weir Controls 0.42 cfs @ 0.89 fps)

Summary for Pond 4P: Drip Edge

Inflow Area	a =	0.121 ac,10	0.00% Imp	ervious,	Inflow	Depth >	4.39"	for 10-Y	R STOR	A event
Inflow	=	0.54 cfs @	12.09 hrs,	Volume	=	0.044	af			
Outflow	=	0.05 cfs @	13.01 hrs,	Volume	=	0.044	af, Atte	en= 92%,	Lag= 55.	6 min
Discarded	=	0.05 cfs @	13.01 hrs,	Volume	=	0.044	af		-	
Primary	=	0.00 cfs @	0.00 hrs,	Volume	=	0.000	af			

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 231.29' @ 13.01 hrs Surf.Area= 756 sf Storage= 724 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 123.2 min (872.1 - 748.9)

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Volume	Inver	t Avail.Sto	rage Storage	Description	
#1	228.90	' 1,24	10 cf Custom 3,100 cf	Stage Data (P Overall x 40.09	rismatic) Listed below (Recalc) % Voids
Elevatio	on S	urf.Area	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
228.9	90	756	0	0	
229.0	00	756	76	76	
230.0	00	756	756	832	
232.0	00	756	1,512	2,344	
233.0	00	756	756	3,100	
Device	Routing	Invert	Outlet Device	S	
#1	Discarded	228.90'	2.000 in/hr Ex	xfiltration over	Surface area
			Conductivity to	o Groundwater I	Elevation = 220.83'
#2	Primary	232.00'	156.0' long x	1.0' breadth B	road-Crested Rectangular Weir
			Head (feet) 0	.20 0.40 0.60	0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00		
			Coef. (English	n) 2.69 2.72 2.	75 2.85 2.98 3.08 3.20 3.28 3.31
			3.30 3.31 3.3	32	

Discarded OutFlow Max=0.05 cfs @ 13.01 hrs HW=231.29' (Free Discharge) **1=Exfiltration** (Controls 0.05 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=228.90' TW=0.00' (Dynamic Tailwater) **2=Broad-Crested Rectangular Weir** (Controls 0.00 cfs)

Summary for Pond 5P: Drip Edge

Inflow Area	a =	0.076 ac,10	0.00% Imp	ervious,	Inflow	Depth >	4.39"	for 10-Y	'R STORM	event
Inflow	=	0.34 cfs @	12.09 hrs,	Volume	=	0.028	af			
Outflow	=	0.04 cfs @	12.81 hrs,	Volume	=	0.028	af, Atte	en= 90%,	Lag= 43.2	min
Discarded	=	0.04 cfs @	12.81 hrs,	Volume	=	0.028	af		-	
Primary	=	0.00 cfs @	0.00 hrs,	Volume	=	0.000	af			

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 230.50' @ 12.81 hrs Surf.Area= 634 sf Storage= 407 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 80.3 min (829.2 - 748.9)

Volume	Invert A	vail.Storage	Storage	e Description	
#1	228.90'	1,040 cf	Custon 2,599 c	n Stage Data (Pr f Overall x 40.0%	i smatic) Listed below (Recalc) 6 Voids
Elevation (feet)	Surf.Are (sq-	ea Inc ft) (cubi	c.Store c-feet)	Cum.Store (cubic-feet)	
228.90	63	34	0	0	
229.00	63	34	63	63	
230.00	63	34	634	697	
232.00	63	34	1,268	1,965	
233.00	63	34	634	2.599	

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Device	Routing	Invert	Outlet Devices
#1	Discarded	228.90'	2.000 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 220.83'
#2	Primary	232.00'	132.0' long x 1.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00
			Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31
			3.30 3.31 3.32
#2	Primary	232.00'	132.0' long x 1.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2. 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.3' 3.30 3.31 3.32

Discarded OutFlow Max=0.04 cfs @ 12.81 hrs HW=230.50' (Free Discharge) **1=Exfiltration** (Controls 0.04 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=228.90' TW=220.80' (Dynamic Tailwater) ←2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 6P: Drip Edge

Inflow Are	ea =	0.204 ac,100.00% Impervious, Inflov	v Depth > 4.39"	for 10-YR STORM event
Inflow	=	0.90 cfs @ 12.09 hrs, Volume=	0.074 af	
Outflow	=	0.42 cfs @ 12.29 hrs, Volume=	0.032 af, Atter	n= 53%, Lag= 12.2 min
Primary	=	0.42 cfs @ 12.29 hrs, Volume=	0.032 af	-

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 222.01' @ 12.30 hrs Surf.Area= 1,509 sf Storage= 1,875 cf

Plug-Flow detention time= 302.3 min calculated for 0.032 af (42% of inflow) Center-of-Mass det. time= 155.5 min (904.4 - 748.9)

Volume	Inv	ert Avail.St	orage Storag	ge Description
#1	218.9	90' 2,4	475 cf Custo 6,187	om Stage Data (Prismatic)Listed below (Recalc) ′ cf Overall x 40.0% Voids
Elevatio (fee	n t)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
218.9 219.0 220.0 222.0 223.0	0 0 0 0 0	1,509 1,509 1,509 1,509 1,509 1,509	0 151 1,509 3,018 1,509	0 151 1,660 4,678 6,187
Device	Routing	Invert	Outlet Devic	ices
#1	Primary	222.00'	312.0' long Head (feet) 2.50 3.00 Coef. (Engli 3.30 3.31 3	y x 1.0' breadth Broad-Crested Rectangular Weir) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 lish) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.32

Primary OutFlow Max=0.41 cfs @ 12.29 hrs HW=222.01' TW=0.00' (Dynamic Tailwater) **1=Broad-Crested Rectangular Weir** (Weir Controls 0.41 cfs @ 0.21 fps) **21137 - POST DEV -W-FP** Prepared by {enter your company name here} HydroCAD® 10.10-5a s/n 10589 © 2020 HydroCAD Software Solutions LLC

Summary for Pond CB1: CB1

 Inflow Area =
 0.129 ac,100.00% Impervious, Inflow Depth > 4.39" for 10-YR STORM event

 Inflow =
 0.57 cfs @ 12.09 hrs, Volume=
 0.047 af

 Outflow =
 0.57 cfs @ 12.09 hrs, Volume=
 0.047 af, Atten= 0%, Lag= 0.0 min

 Primary =
 0.57 cfs @ 12.09 hrs, Volume=
 0.047 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 213.08' @ 12.50 hrs Flood Elev= 215.17'

Device	Routing	Invert	Outlet Devices
#1	Primary	211.92'	15.0" Round Culvert
	5		L= 20.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 211.92' / 211.82' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf

Primary OutFlow Max=0.00 cfs @ 12.09 hrs HW=212.65' TW=212.70' (Dynamic Tailwater)

Summary for Pond CB2: CB2

Inflow Area	a =	0.300 ac,10	0.00% Imp	ervious,	Inflow Depth	n > 4.3	39" for	10-YR	STORM event
Inflow	=	1.32 cfs @	12.09 hrs,	Volume	= 0.1	110 af			
Outflow	=	1.32 cfs @	12.09 hrs,	Volume	= 0.1	110 af,	Atten= 0)%, Lag	g= 0.0 min
Primary	=	1.32 cfs @	12.09 hrs,	Volume	= 0.1	110 af			-

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 213.08' @ 12.45 hrs Flood Elev= 215.17'

Device	Routing	Invert	Outlet Devices
#1	Primary	211.72'	15.0" Round Culvert L= 20.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 211.72' / 211.62' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf

Primary OutFlow Max=0.00 cfs @ 12.09 hrs HW=212.70' TW=212.72' (Dynamic Tailwater) **1=Culvert** (Controls 0.00 cfs)

Summary for Pond CB3: CB3

Inflow Area	a =	0.293 ac,	0.00% Impervious,	Inflow Depth >	1.99" fo	r 10-YR STORM event
Inflow	=	0.59 cfs @	12.14 hrs, Volume	= 0.049	af	
Outflow	=	0.59 cfs @	12.14 hrs, Volume	= 0.049	af, Atten=	0%, Lag= 0.0 min
Primary	=	0.59 cfs @	12.14 hrs, Volume	= 0.049	af	-

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 225.45' @ 12.14 hrs Flood Elev= 229.00'

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Type III 24-hr 10-YR STORM Rainfall=4.63" Printed 10/29/2021 HydroCAD® 10.10-5a s/n 10589 © 2020 HydroCAD Software Solutions LLC Page 23

Device	Routing	Invert	Outlet Devices
#1	Primary	225.00'	12.0" Round Culvert L= 120.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 225.00' / 224.40' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.58 cfs @ 12.14 hrs HW=225.44' TW=0.00' (Dynamic Tailwater) **1=Culvert** (Barrel Controls 0.58 cfs @ 2.54 fps)

Summary for Pond FP1: FocalPoint 1

Inflow Area	=	0.410 ac, 8	5.11% Impe	ervious,	Inflow Deptl	ı> 3.	94" for	10-YR	STORM event
Inflow	=	1.73 cfs @	12.09 hrs,	Volume	= 0.	135 af			
Outflow	=	1.88 cfs @	12.10 hrs,	Volume	= 0.	135 af,	Atten= ()%, Lag	g= 0.5 min
Primary	=	1.88 cfs @	12.10 hrs,	Volume	= 0.	135 af			

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 230.07' @ 12.09 hrs Surf.Area= 80 sf Storage= 348 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 6.1 min (781.3 - 775.2)

Volume	Invert	Avail.Stora	age S	torage De	scription		
#1	228.81'	30	6 cf 1	0.00'W x 8	8.00'L x 2.25'	H FocalPoint	
			18	30 cf Over	rall_x 20.0% \	/oids	
#2	228.80'	327	7 cf S	<u>urface Bo</u>	owl Area (Pris	smatic)Listed below	<u>/ (Recalc) -Imperviou</u> s
		363	3 cf T	otal Availa	able Storage		
Elevatio	on Si	urf.Area	Inc.St	ore	Cum.Store		
(fee	et)	(sq-ft) ((cubic-fe	et)	(cubic-feet)		
228.8	30	250		0	0		
228.8	31	250		2	2		
229.8	31	400		325	327		
Device	Routing	Invert	Outlet I	Devices			
#1	Device 2	229.81'	15.0" H	loriz. Orif	ice/Grate C	= 0.600	
			Limited	to weir flo	ow at low hea	ds	
#2	Primary	225.66'	15.0" I	Round Cu	ulvert		
			L= 10.0)' CPP, p	rojecting, no l	headwall, Ke= 0.90	0
			Inlet / C	Jutlet Inve	ert= 225.66' / 2	225.56' S = 0.0100	'/' Cc= 0.900
	D	000.041	n= 0.01	3 Corrug	ated PE, smo	oth interior, Flow A	rea= 1.23 st
#3	Primary	228.81	100.00	J IN/Nr Ex	Tiltration ove	er Surface area	
			Conauc	cuvity to G	roundwater E	evalion = 220.83	Phase-In= 0.01

Primary OutFlow Max=1.83 cfs @ 12.10 hrs HW=230.06' TW=224.29' (Dynamic Tailwater)

2=Culvert (Passes 1.62 cfs of 9.06 cfs potential flow) **1=Orifice/Grate** (Weir Controls 1.62 cfs @ 1.64 fps)

-3=Exfiltration (Controls 0.21 cfs)

Summary for Pond FP2: FocalPoint 2

Inflow Area	=	0.339 ac, 9	0.79% Impe	ervious,	Inflow Depth	> 4.	16" for	10-YR	STORM event
Inflow	=	1.47 cfs @	12.09 hrs,	Volume	= 0.11	8 af			
Outflow	=	1.44 cfs @	12.08 hrs,	Volume	= 0.11	l8 af,	Atten= 2	2%, Lag	g= 0.0 min
Primary	=	1.44 cfs @	12.08 hrs,	Volume	= 0.11	8 af			-

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 230.02' @ 12.08 hrs Surf.Area= 80 sf Storage= 347 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 6.1 min (769.9 - 763.8)

Volume	Invert	Avail.Stor	rage	Storage De	escription			
#1	228.81'	3	36 cf	10.00'W x	8.00'L x 2.2	5'H Focall	Point	
				180 cf Ove	rall x 20.0%	Voids		
#2	228.80'	32	27 cf	Surface B	owl Area (Pr	rismatic)L	isted belov	v (Recalc) -Impervious
		36	63 cf	Total Availa	able Storage			
Elevatio	on Su	urf.Area	Inc	.Store	Cum.Store			
	ət)	(sq-it)	(Cubic	<u>-ieet)</u>				
228.8	30	250		0	0			
228.8	31	250		2	2			
229.8	31	400		325	327			
Device	Routing	Invert	Outle	et Devices				
#1	Device 2	229.81'	15.0	" Horiz. Ori	fice/Grate	C= 0.600		
			Limit	ed to weir fl	ow at low he	ads		
#2	Primary	225.66'	15.0	" Round C	ulvert			
			L= 1	0.0' CPP, p	projecting, no	o headwall	, Ke= 0.90	00
			Inlet	/ Outlet Inve	ert= 225.66' /	225.56'	S= 0.0100	'/' Cc= 0.900
			n= 0	.013 Corrug	gated PE, sm	nooth inter	ior, Flow A	Area= 1.23 sf
#3	Primary	228.81'	100.	000 in/hr E	filtration ov	ver Surfac	e area	
	-		Cond	ductivity to C	Groundwater	Elevation	= 220.83'	Phase-In= 0.01'
				-				
Primary	OutFlow M	lax=1.41 cfs @	ງ 12.0	8 hrs HW=	230.02' TW=	=224.24'	(Dynamic	Tailwater)

2=Culvert (Passes 1.20 cfs of 9.01 cfs potential flow) **1=Orifice/Grate** (Weir Controls 1.20 cfs @ 1.48 fps)

3=Exfiltration (Controls 0.21 cfs)

Summary for Pond FP3: FocalPoint 3

Inflow Area	=	0.336 ac, 7	8.26% Imp	ervious,	Inflow De	epth >	3.83"	for 1	0-YR	STORM e	vent
Inflow	=	1.39 cfs @	12.09 hrs,	Volume	=	0.107	af				
Outflow	=	1.81 cfs @	12.06 hrs,	Volume	=	0.107	af, Atte	n= 0%	5, Lag	g= 0.0 min	l
Primary	=	1.81 cfs @	12.06 hrs,	Volume	=	0.107	af		-		

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 226.99' @ 12.06 hrs Surf.Area= 80 sf Storage= 348 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow)

Invert Avail.Storage Storage Description 10.00'W x 8.00'L x 2.25'H FocalPoint 225.74' 36 cf 180 cf Overall x 20.0% Voids 225.73' 328 cf Surface Bowl Area (Prismatic)Listed below (Recalc) - Impervious 364 cf Total Available Storage

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Center-of-Mass det. time= 6.5 min (786.6 - 780.2)

Volume

#1

#2

Sı	ation Surf.Area	I	nc.Store		Cum.Store
	feet) (sq-ft)	(cu	bic-feet)	(cubic-feet)
	5.73 250		0		0
	5.74 250		3		3
	6.74 400		325		328

Device	Routing	Invert	Outlet Devices					
#1	Device 2	226.74'	15.0" Horiz. Orifice/Grate C= 0.600					
			Limited to weir flow at low heads					
#2	Primary	222.49'	12.0" Round Culvert					
	-		L= 10.0' CPP, projecting, no headwall, Ke= 0.900					
			Inlet / Outlet Invert= 222.49' / 222.39' S= 0.0100 '/' Cc= 0.900					
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf					
#3	Primary	225.74'	100.000 in/hr Exfiltration over Surface area					
	-		Conductivity to Groundwater Elevation = 215.39' Phase-In= 0.01'					

Primary OutFlow Max=1.68 cfs @ 12.06 hrs HW=226.98' TW=221.25' (Dynamic Tailwater)

2=Culvert (Passes 1.47 cfs of 5.96 cfs potential flow)

1=Orifice/Grate (Weir Controls 1.47 cfs @ 1.59 fps)

-3=Exfiltration (Controls 0.21 cfs)

Summary for Pond FP4: FocalPoint 4

Inflow Area	a =	0.121 ac,10	0.00% Imper	rvious,	Inflow Dep	pth >	4.39"	for 10-Y	R STORM event
Inflow	=	0.54 cfs @	12.09 hrs, \	Volume	= (0.044 a	af		
Outflow	=	0.33 cfs @	12.20 hrs, \	Volume:	= (0.041 a	af, Atte	n= 38%,	Lag= 7.0 min
Primary	=	0.33 cfs @	12.20 hrs, \	√olume [;]	= (0.041 a	af		-

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 193.84' @ 12.20 hrs Surf.Area= 80 sf Storage= 344 cf

Plug-Flow detention time= 77.5 min calculated for 0.041 af (93% of inflow) Center-of-Mass det. time= 37.9 min (786.8 - 748.9)

Volume	Invert	Avail.Storage	Storage Description
#1	192.80'	36 cf	10.00'W x 8.00'L x 2.25'H FocalPoint
			180 cf Overall x 20.0% Voids
#2	192.29'	328 cf	193.7 (Prismatic) Listed below (Recalc) - Impervious
		364 cf	Total Available Storage

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Elevatio (fee	on et)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)						
192.2	29	250	0	0						
192.3	30	250	3	3						
193.:	30	400	325	328						
Device	Routing	Invert	Outlet Devices							
#1	Device 2	193.80'	15.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads							
#2	Primary	189.80'	6.0" Round Culvert L= 15.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 189.80' / 189.70' S= 0.0067 '/' Cc= 0.900 n= 0.013 Corrugated PE smooth interior. Flow Area= 0.20 sf							
#3	Primary	192.80'	100.000 in/hr E Conductivity to	Groundwater E	er Surface area Elevation = 188.00'	Phase-In= 0.01'				

Primary OutFlow Max=0.32 cfs @ 12.20 hrs HW=193.84' TW=0.00' (Dynamic Tailwater) 2=Culvert (Passes 0.10 cfs of 1.45 cfs potential flow) 1=Orifice/Grate (Weir Controls 0.10 cfs @ 0.65 fps) 3=Exfiltration (Controls 0.23 cfs)

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S	Runoff Area=102,651 sf 0.77% Impervious Runoff Depth>0.29" Flow Length=350' Tc=9.6 min CN=72 Runoff=0.45 cfs 0.057 af
Subcatchment2S: Subcatchment2S	Runoff Area=17,857 sf 85.11% Impervious Runoff Depth>1.40" Tc=6.0 min CN=94 Runoff=0.65 cfs 0.048 af
Subcatchment3S: Subcatchment3S	Runoff Area=14,768 sf 90.79% Impervious Runoff Depth>1.57" Tc=6.0 min CN=96 Runoff=0.59 cfs 0.044 af
Subcatchment4S: Subcatchment4S	Runoff Area=12,745 sf 0.00% Impervious Runoff Depth>0.32" Flow Length=350' Tc=9.6 min CN=73 Runoff=0.07 cfs 0.008 af
Subcatchment5S: Subcatchment5S	Runoff Area=14,630 sf 78.26% Impervious Runoff Depth>1.31" Tc=6.0 min CN=93 Runoff=0.50 cfs 0.037 af
Subcatchment6S: Subcatchment6S	Runoff Area=104,590 sf 0.00% Impervious Runoff Depth>0.35" Flow Length=597' Tc=14.7 min CN=74 Runoff=0.55 cfs 0.070 af
Subcatchment7S: Subcatchment7S	Runoff Area=5,959 sf 0.00% Impervious Runoff Depth>0.35" Tc=6.0 min CN=74 Runoff=0.04 cfs 0.004 af
Subcatchment7S1: SubcatchmentCB1	Runoff Area=5,639 sf 100.00% Impervious Runoff Depth>1.77" Tc=6.0 min CN=98 Runoff=0.24 cfs 0.019 af
Subcatchment7S2: SubcatchmentCB2	Runoff Area=7,419 sf 100.00% Impervious Runoff Depth>1.77" Tc=6.0 min CN=98 Runoff=0.32 cfs 0.025 af
Subcatchment8S: Subcatchment8S	Runoff Area=5,280 sf 100.00% Impervious Runoff Depth>1.77" Tc=6.0 min CN=98 Runoff=0.23 cfs 0.018 af
Subcatchment9S: Subcatchment9S	Runoff Area=3,313 sf 100.00% Impervious Runoff Depth>1.77" Tc=6.0 min CN=98 Runoff=0.14 cfs 0.011 af
Subcatchment10S: Subcatchment10S	Runoff Area=8,865 sf 100.00% Impervious Runoff Depth>1.77" Tc=6.0 min CN=98 Runoff=0.38 cfs 0.030 af
Subcatchment11S: Subcatchment11S	Runoff Area=18,787 sf 52.98% Impervious Runoff Depth>0.90" Tc=6.0 min CN=87 Runoff=0.45 cfs 0.033 af
Subcatchment 12S: Subcatchment 11S	Runoff Area=5,279 sf 100.00% Impervious Runoff Depth>1.77" Tc=6.0 min CN=98 Runoff=0.23 cfs 0.018 af
Reach 1R: Flow Through Wetland n=0.030 L=2	Avg. Flow Depth=0.02' Max Vel=0.66 fps Inflow=0.18 cfs 0.035 af 10.0' S=0.0548 '/' Capacity=185.74 cfs Outflow=0.18 cfs 0.035 af
Reach AP1: Analysis Point #1	Inflow=1.59 cfs 0.314 af

Outflow=1.59 cfs 0.314 af

Reach AP2: Analysis Point #2

Type III 24-hr FP1 Rainfall=2.00" Printed 10/29/2021 e Solutions LLC Page 28

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Inflow=0.45 cfs 0.033 af Outflow=0.45 cfs 0.033 af

Pond 1P: STORMTECH 1	Peak Elev=224.01' Storage=0.031 af Inflow=0.44 cfs 0.092 af Discarded=0.00 cfs 0.000 af Primary=0.34 cfs 0.085 af Outflow=0.34 cfs 0.085 af
Pond 2P: STORMTECH 2	Peak Elev=221.11' Storage=0.009 af Inflow=0.20 cfs 0.037 af Discarded=0.00 cfs 0.000 af Primary=0.18 cfs 0.035 af Outflow=0.18 cfs 0.035 af
Pond 3P: Pond 3P	Peak Elev=212.35' Storage=1,001 cf Inflow=0.60 cfs 0.048 af Outflow=0.07 cfs 0.044 af
Pond 4P: Drip Edge	Peak Elev=229.60' Storage=211 cf Inflow=0.23 cfs 0.018 af Discarded=0.04 cfs 0.018 af Primary=0.00 cfs 0.000 af Outflow=0.04 cfs 0.018 af
Pond 5P: Drip Edge	Peak Elev=229.33' Storage=110 cf Inflow=0.14 cfs 0.011 af Discarded=0.03 cfs 0.011 af Primary=0.00 cfs 0.000 af Outflow=0.03 cfs 0.011 af
Pond 6P: Drip Edge	Peak Elev=221.07' Storage=1,310 cf Inflow=0.38 cfs 0.030 af Outflow=0.00 cfs 0.000 af
Pond CB1: CB1	Peak Elev=212.35' Inflow=0.24 cfs 0.019 af 15.0" Round Culvert n=0.013 L=20.0' S=0.0050 '/' Outflow=0.24 cfs 0.019 af
Pond CB2: CB2	Peak Elev=212.35' Inflow=0.56 cfs 0.044 af 15.0" Round Culvert n=0.013 L=20.0' S=0.0050 '/' Outflow=0.56 cfs 0.044 af
Pond CB3: CB3	Peak Elev=225.15' Inflow=0.07 cfs 0.008 af 12.0" Round Culvert n=0.013 L=120.0' S=0.0050 '/' Outflow=0.07 cfs 0.008 af
Pond FP1: FocalPoint 1	Peak Elev=229.83' Storage=344 cf Inflow=0.65 cfs 0.048 af Outflow=0.23 cfs 0.048 af
Pond FP2: FocalPoint 2	Peak Elev=229.67' Storage=286 cf Inflow=0.59 cfs 0.044 af Outflow=0.21 cfs 0.044 af
Pond FP3: FocalPoint 3	Peak Elev=226.38' Storage=203 cf Inflow=0.50 cfs 0.037 af Outflow=0.20 cfs 0.037 af
Pond FP4: FocalPoint 4	Peak Elev=192.83' Storage=157 cf Inflow=0.23 cfs 0.018 af Outflow=0.19 cfs 0.015 af
Total Puno	ff Area = 7 525 ac Runoff Volume = 0.421 af Average Runoff Depth = 0.67

Total Runoff Area = 7.525 acRunoff Volume = 0.421 afAverage Runoff Depth = 0.67"73.58% Pervious = 5.537 ac26.42% Impervious = 1.988 ac

Summary for Subcatchment 1S: Subcatchment 1S

Runoff = 0.45 cfs @ 12.19 hrs, Volume= 0.057 af, Depth> 0.29"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr FP1 Rainfall=2.00"

A	rea (sf)	CN I	Description						
	48,626	70	Noods, Go	Noods, Good, HSG C					
	8,966	70	Noods, Go	od, HSG C					
	6,940	70	Noods, Go	od, HSG C					
	794	98	Paved park	ing, HSG C					
	36,539	74 :	>75% Gras	s cover, Go	ood, HSG C				
	786	74 :	>75% Gras	s cover, Go	ood, HSG C				
1	02,651	72	Neighted A	verage					
1	01,857	ę	99.23% Pei	vious Area					
	794	().77% Impe	ervious Area	а				
Тс	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
6.1	50	0.1200	0.14		Sheet Flow, Sheet Flow				
					Woods: Light underbrush n= 0.400 P2= 3.11"				
3.5	300	0.0800	1.41		Shallow Concentrated Flow, Shallow Flow				
					Woodland Kv= 5.0 fps				
9.6	350	Total							

Summary for Subcatchment 2S: Subcatchment 2S

Runoff = 0.65 cfs @ 12.09 hrs, Volume= 0.048 af, Depth> 1.40"

A	rea (sf)	CN	Description						
	14,373	98	Paved park	ing, HSG C	C				
	825	98	Paved park	ing, HSG C	С				
	1,360	74	>75% Gras	s cover, Go	lood, HSG C				
	1,299	74	>75% Gras	s cover, Go	lood, HSG C				
	17,857	94	Weighted Average						
	2,659		14.89% Pervious Area						
	15,198		85.11% Impervious Area						
Tc	Length	Slop	e Velocity	Capacity	Description				
(min)	(feet)	(ft/f	t) (ft/sec)	(cfs)					
6.0					Direct Entry,				

Summary for Subcatchment 3S: Subcatchment 3S

Runoff = 0.59 cfs @ 12.09 hrs, Volume= 0.044 af, Depth> 1.57"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr FP1 Rainfall=2.00"

Are	a (sf)	CN	Description		
13	3,408	98	Paved parki	ing, HSG C	C
-	1,360	74	>75% Ġras	s cover, Go	ood, HSG C
14 13 Tc L (min)	4,768 1,360 3,408 -ength (feet)	96 Slope (ft/ft)	Weighted A 9.21% Perv 90.79% Imp Velocity (ft/sec)	verage ious Area pervious Are Capacity (cfs)	rea Description
6.0	· · · ·		· · · · ·		Direct Entry,

Summary for Subcatchment 4S: Subcatchment 4S

Runoff = 0.07 cfs @ 12.17 hrs, Volume= 0.008 af, Depth> 0.32"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr FP1 Rainfall=2.00"

A	rea (sf)	CN I	Description		
	3,468	70 \	Noods, Go	od, HSG C	
	9,277	74 >	>75% Gras	s cover, Go	ood, HSG C
	12,745	73 \	Neighted A	verage	
	12,745		100.00% Pe	ervious Are	a
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
6.1	50	0.1200	0.14		Sheet Flow, Sheet Flow
					Woods: Light underbrush n= 0.400 P2= 3.11"
3.5	300	0.0800	1.41		Shallow Concentrated Flow, Shallow Flow
					Woodland Kv= 5.0 fps
9.6	350	Total			

Summary for Subcatchment 5S: Subcatchment 5S

Runoff = 0.50 cfs @ 12.09 hrs, Volume= 0.037 af, Depth> 1.31"

 Type III 24-hr
 FP1 Rainfall=2.00"

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Are	ea (sf)	CN	Description					
10	0,386	98	Paved parki	ng, HSG C				
	1,064	98	Paved parki	ng, HSG C				
2	2,992	74	>75% Grass	s cover, Go	od, HSG C			
	188	74	>75% Grass	s cover, Go	od, HSG C			
14	4,630	93	Weighted Average					
:	3,180		21.74% Pervious Area					
1	1,450		78.26% Impervious Area					
Tc L	_ength	Slope	e Velocity	Capacity	Description			
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)				
6.0					Direct Entry,			

Summary for Subcatchment 6S: Subcatchment 6S

Runoff = 0.55 cfs @ 12.26 hrs, Volume= 0.070 af, Depth> 0.35"

A	rea (sf)	CN E	Description						
	31,117	70 V	70 Woods, Good, HSG C						
	18,906	70 V	Voods, Go	od, HSG C					
	4,969	96 0	Gravel surfa	ace, HSG (
	12,429	74 >	·75% Gras	s cover, Go	bod, HSG C				
	2,075	74 >	·75% Gras	s cover, Go	bod, HSG C				
	2,358	80 >	·75% Gras	s cover, Go	bod, HSG D				
	32,736	77 V	Voods, Go	od, HSG D					
1	04,590	74 V	Veighted A	verage					
1	04,590	1	00.00% P	ervious Are	а				
Tc	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
9.5	50	0.0400	0.09		Sheet Flow, Sheet Flow				
					Woods: Light underbrush n= 0.400 P2= 3.11"				
0.5	50	0.0400	1.56		Sheet Flow, Sheet over Gravel				
					Smooth surfaces n= 0.011 P2= 3.11"				
3.1	250	0.0720	1.34		Shallow Concentrated Flow, Shallow Flow				
					Woodland Kv= 5.0 fps				
0.6	175	0.0460	5.11	170.24	Parabolic Channel, Flow through Wetland				
					W=100.00' D=0.50' Area=33.3 sf Perim=100.0'				
					n= 0.030 Stream, clean & straight				
0.7	50	0.1400	1.27	0.02	Pipe Channel, Culvert				
					2.0" x 1.0" Box Area= 0.0 sf Perim= 0.5' r= 0.03'				
					n= 0.040 Earth, cobble bottom, clean sides				
0.3	22	0.1200	1.23	0.65	Parabolic Channel,				
					W=8.00' D=0.10' Area=0.5 sf Perim=8.0'				
					n= 0.069 Riprap, 6-inch				
14.7	597	Total							

Summary for Subcatchment 7S: Subcatchment 7S

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0.04 cfs @ 12.12 hrs, Volume= 0.004 af, Depth> 0.35" Runoff =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr FP1 Rainfall=2.00"

A	rea (sf)	CN	Description			
	740	70	Woods, Go	od, HSG C		
	5,219	74	>75% Gras	s cover, Go	ood, HSG C	
	5,959	74	Weighted A	verage		
	5,959		100.00% Pervious Area			
Tc	Length	Slop	e Velocity	Capacity	Description	
(min)	(feet)	(ft/ft	i) (ft/sec)	(cfs)		
6.0					Direct Entry,	

Summary for Subcatchment 7S1: Subcatchment CB1

Runoff 0.24 cfs @ 12.09 hrs, Volume= 0.019 af, Depth> 1.77" =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr FP1 Rainfall=2.00"

A	rea (sf)	CN I	Description				
	5,639	98 I	Paved parking, HSG C				
	5,639		100.00% Impervious Area				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
6.0					Direct Entry,		

Summary for Subcatchment 7S2: Subcatchment CB2

Runoff 0.32 cfs @ 12.09 hrs, Volume= 0.025 af, Depth> 1.77" =

A	rea (sf)	CN	Description			
	6,012	98	Paved park	ing, HSG C		
	1,407	98	Paved park	ing, HSG D		
	7,419	98	Weighted Average			
	7,419		100.00% Impervious Area			
Tc	Length	Slope	e Velocity	Capacity	Description	
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)		
6.0					Direct Entry,	

Summary for Subcatchment 8S: Subcatchment 8S

Runoff = 0.23 cfs @ 12.09 hrs, Volume= 0.018 af, Depth> 1.77"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr FP1 Rainfall=2.00"

A	rea (sf)	CN	Description				
	5,280	98	Roofs, HSC	ЭС			
	5,280		100.00% Impervious Area				
Тс	Length	Slop	e Velocity	Capacity	Description		
(min)	(feet)	(ft/f	t) (ft/sec)	(cfs)			
6.0					Direct Entry,		
		0		or Cuboot	tahmant 00: Subaatahmant 00		

Summary for Subcatchment 9S: Subcatchment 9S

Runoff = 0.14 cfs @ 12.09 hrs, Volume= 0.011 af, Depth> 1.77"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr FP1 Rainfall=2.00"

A	rea (sf)	CN	Description		
	3,313	98	Roofs, HSC	G C	
	3,313		100.00% In	npervious A	Area
Tc (min)	Length (feet)	Slope (ft/ft	e Velocity) (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Summary for Subcatchment 10S: Subcatchment 10S

Runoff = 0.38 cfs @ 12.09 hrs, Volume= 0.030 af, Depth> 1.77"

A	rea (sf)	CN E	Description		
	8,865	98 F	Roofs, HSC	G C	
	8,865	1	00.00% In	npervious A	Area
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Summary for Subcatchment 11S: Subcatchment 11S

Runoff = 0.45 cfs @ 12.10 hrs, Volume= 0.033 af, Depth> 0.90"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr FP1 Rainfall=2.00"

Α	rea (sf)	CN	Description				
	9,953	98	Paved park	ing, HSG C	С		
	3,298	74	>75% Gras	s cover, Go	Good, HSG C		
	5,536	74	>75% Gras	s cover, Go	Good, HSG C		
	18,787	87	Weighted A	Weighted Average			
	8,834		47.02% Per	vious Area	а		
	9,953		52.98% Imp	pervious Are	rea		
Tc (min)	Length (feet)	Slop (ft/ff	e Velocity t) (ft/sec)	Capacity (cfs)	/ Description)		
6.0					Direct Entry,		

Summary for Subcatchment 12S: Subcatchment 11S

Runoff = 0.23 cfs @ 12.09 hrs, Volume= 0.018 af, Depth> 1.77"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr FP1 Rainfall=2.00"

A	rea (sf)	CN	Description					
	5,279	98	Paved parking, HSG C					
	5,279		100.00% Impervious Area					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
6.0					Direct Entry,			

Summary for Reach 1R: Flow Through Wetland

Inflow Area = Inflow = Outflow =	0.412 ac, 8 0.18 cfs @ 0.18 cfs @	2.28% Impe 12.88 hrs, 12.89 hrs,	ervious, Inflow D Volume= Volume=	0epth > 1.0 0.035 af 0.035 af,	02" for FP1 event Atten= 1%, Lag= 0.6 min	
Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Max. Velocity= 0.66 fps, Min. Travel Time= 5.3 min Avg. Velocity = 0.34 fps, Avg. Travel Time= 10.4 min						
Peak Storage= 58 cf @ 12.89 hrs Average Depth at Peak Storage= 0.02' , Surface Width= 20.17' Bank-Full Depth= 0.50' Flow Area= 33.3 sf, Capacity= 185.74 cfs						

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100.00' x 0.50' deep Parabolic Channel, n= 0.030 Stream, clean & straight Length= 210.0' Slope= 0.0548 '/' Inlet Invert= 220.50', Outlet Invert= 209.00'



Summary for Reach AP1: Analysis Point #1

Inflow Are	ea =	7.094 ac, 2	4.80% Impe	ervious,	Inflow De	epth > 0	.53" for	· FP1	event
Inflow	=	1.59 cfs @	12.21 hrs,	Volume	=	0.314 af			
Outflow	=	1.59 cfs @	12.21 hrs,	Volume	=	0.314 af	, Atten=	0%,	Lag= 0.0 mir

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach AP2: Analysis Point #2

Inflow A	rea =	0.431 ac, 52.9	8% Impervious,	Inflow Depth > 0.	90" for FP1	event
Inflow	=	0.45 cfs @ 12	.10 hrs, Volume	e= 0.033 af		
Outflow	=	0.45 cfs @ 12	.10 hrs, Volume	e= 0.033 af,	, Atten= 0%, I	_ag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Pond 1P: STORMTECH 1

Inflow Area	a =	0.749 ac, 8	87.68% Imp	ervious, l	Inflow Depth >	1.48"	for FP1	event	
Inflow	=	0.44 cfs @	12.36 hrs,	Volume=	0.092	2 af			
Outflow	=	0.34 cfs @	13.07 hrs,	Volume=	: 0.085	5 af, At	tten= 23%,	Lag= 4	3.1 min
Discarded	=	0.00 cfs @	0.00 hrs,	Volume=	: 0.000) af		-	
Primary	=	0.34 cfs @	13.07 hrs,	Volume=	: 0.085	5 af			

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 224.01' @ 13.07 hrs Surf.Area= 0.075 ac Storage= 0.031 af

Plug-Flow detention time= 115.1 min calculated for 0.085 af (93% of inflow) Center-of-Mass det. time= 77.9 min (881.5 - 803.6)

Volume	Invert	Avail.Stora	ge Storage Description
#1	223.60'	0.135	af ADS_StormTech SC-740 +Cap x 128 Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap 128 Chambers in 8 Rows
Device	Routing	Invert	Outlet Devices
#1	Primary	223.60'	8.0" Round Culvert

L= 35.0° CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 223.60' / 223.42' S= 0.0051 '/' Cc= 0.900

Type III 24-hr	FP1 Ra	infall=2.00"
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			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.35 sf
#2	Discarded	223.60'	2.000 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 220.83'

Discarded OutFlow Max=0.00 cfs @ 0.00 hrs HW=223.60' (Free Discharge) **2=Exfiltration** (Controls 0.00 cfs)

Primary OutFlow Max=0.34 cfs @ 13.07 hrs HW=224.01' TW=0.00' (Dynamic Tailwater) **1=Culvert** (Barrel Controls 0.34 cfs @ 2.15 fps)

Summary for Pond 2P: STORMTECH 2

Inflow Area	=	0.412 ac, 8	2.28% Imperv	vious, Inflow D	Depth > 1.	.07" for	FP1 event
Inflow	=	0.20 cfs @	12.34 hrs, Vo	olume=	0.037 af		
Outflow	=	0.18 cfs @	12.88 hrs, Vo	olume=	0.035 af	, Atten=7	7%, Lag= 32.3 min
Discarded	=	0.00 cfs @	0.00 hrs, Vo	olume=	0.000 af		
Primary	=	0.18 cfs @	12.88 hrs, Vo	olume=	0.035 af		

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 221.11' @ 12.88 hrs Surf.Area= 0.028 ac Storage= 0.009 af

Plug-Flow detention time= 70.3 min calculated for 0.035 af (96% of inflow) Center-of-Mass det. time= 45.8 min (860.6 - 814.8)

Volume	Invert	Avail.Stora	ge Storage Description
#1	220.80'	0.051	af ADS_StormTech SC-740 +Cap x 48 Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap 48 Chambers in 8 Rows
Device	Routing	Invert	Outlet Devices
#1	Discarded	220.80'	2.000 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 215.39'
#2	Primary	220.80'	6.0" Round Culvert L= 48.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 220.80' / 220.50' S= 0.0063 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.20 sf

Discarded OutFlow Max=0.00 cfs @ 0.00 hrs HW=220.80' (Free Discharge)

Primary OutFlow Max=0.18 cfs @ 12.88 hrs HW=221.11' TW=220.52' (Dynamic Tailwater) ←2=Culvert (Barrel Controls 0.18 cfs @ 2.03 fps)

Summary for Pond 3P: Pond 3P

Inflow Area	=	0.437 ac, 6	8.66% Imp	ervious,	Inflow Depth	i > 1.3	3" for F	P1 event	
Inflow	=	0.60 cfs @	12.09 hrs,	Volume	= 0.0)48 af			
Outflow	=	0.07 cfs @	12.75 hrs,	Volume	= 0.0)44 af, J	Atten= 88	%, Lag=	39.9 min
Primary	=	0.07 cfs @	12.75 hrs,	Volume	= 0.0)44 af			

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr FP1 Rainfall=2.00" Printed 10/29/2021 C Page 37

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Starting Elev= 129.08' Storage= 0 cf Peak Elev= 212.35' @ 12.75 hrs Surf.Area= 2,010 sf Storage= 1,001 cf

Plug-Flow detention time= 194.3 min calculated for 0.044 af (92% of inflow) Center-of-Mass det. time= 152.5 min (930.3 - 777.9)

Volume	Inv	ert Avail.	.Storage	Storage	Description		
#1	210.4	19'	6,106 cf	Custom	Stage Data (Irreg	ular)Listed below (F	Recalc)
Elevatio	on	Surf.Area	Perim.	Voids	Inc.Store	Cum.Store	Wet.Area
210 /	10	<u>(34-11)</u>	152.0				(34-10)
210.4	19 50	930	100.0	0.0	0	0	930
210.0		930	153.0	40.0	4	4	932
212.0	0	1,720	190.0	40.0	/83	/8/	1,974
212.0)1)-	1,720	190.0	5.0	1	/88	1,976
212.2	25	1,863	195.0	5.0	21	809	2,136
212.2	26	2,010	200.0	100.0	19	828	2,293
212.5	51	2,010	200.0	100.0	503	1,331	2,343
213.0	00	2,316	210.0	100.0	1,059	2,390	2,684
213.8	30	2,835	234.0	100.0	2,057	4,447	3,551
214.0	00	3,900	254.0	100.0	671	5,117	4,329
214.2	25	4,010	256.0	100.0	989	6,106	4,432
Device	Routing	Inv	ert Outle	et Devices	6		
#1	Primary	210.	50' 8.0''	Round C	Culvert		
	-		L= 2	6.0' CPF	, projecting, no he	adwall, Ke= 0.900	
			Inlet	/ Outlet Ir	1vert= 210.50' / 210).30' S= 0.0077 '/'	Cc= 0.900
			n= 0	.013 Cori	rugated PE, smoot	h interior, Flow Are	a= 0.35 sf
#2	Device 1	210.	83' 1.5"	Vert. Ori	fice/Grate C= 0.6	00 Limited to weir	flow at low heads
#3	Device 1	213.	00' 24.0 '	" Horiz. C	Drifice/Grate C= 0).600	
			Limit	ed to weil	r flow at low heads		

Primary OutFlow Max=0.07 cfs @ 12.75 hrs HW=212.35' TW=0.00' (Dynamic Tailwater)

-1=Culvert (Passes 0.07 cfs of 1.63 cfs potential flow)

2=Orifice/Grate (Orifice Controls 0.07 cfs @ 5.81 fps)

-3=Orifice/Grate (Controls 0.00 cfs)

Summary for Pond 4P: Drip Edge

Inflow Area	ı =	0.121 ac,10	0.00% Imp	ervious, Inflow [Depth >	1.77"	for FP1	event	
Inflow	=	0.23 cfs @	12.09 hrs,	Volume=	0.018	af			
Outflow	=	0.04 cfs @	12.56 hrs,	Volume=	0.018	af, Atte	en= 83%,	Lag= 28.	1 min
Discarded	=	0.04 cfs @	12.56 hrs,	Volume=	0.018	af		-	
Primary	=	0.00 cfs @	0.00 hrs,	Volume=	0.000	af			

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 229.60' @ 12.56 hrs Surf.Area= 756 sf Storage= 211 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 31.7 min (798.6 - 767.0)

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Type III 24-hr	FP1 Ra	infall=2.00"
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Volume	Inver	t Avail.Stor	rage Storage	Description	
#1	228.90)' 1,24	10 cf Custom 3,100 cf	Stage Data (Pr Overall x 40.0%	Prismatic)Listed below (Recalc) 1% Voids
Elevatio	on S	Surf.Area	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
228.9	90	756	0	0	
229.0	00	756	76	76	
230.0	00	756	756	832	
232.0	00	756	1,512	2,344	
233.0	00	756	756	3,100	
Device	Routing	Invert	Outlet Devices	5	
#1	Discarded	228.90'	2.000 in/hr Ex Conductivity to	ofiltration over	r Surface area Elevation = 220.83'
#2	Primary	232.00'	156.0' long x Head (feet) 0 2.50 3.00 Coef. (English 3.30 3.31 3.3	(1.0' breadth B .20 0.40 0.60 () 2.69 2.72 2.	Broad-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.75 2.85 2.98 3.08 3.20 3.28 3.31

Discarded OutFlow Max=0.04 cfs @ 12.56 hrs HW=229.60' (Free Discharge) **1=Exfiltration** (Controls 0.04 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=228.90' TW=0.00' (Dynamic Tailwater) **2=Broad-Crested Rectangular Weir** (Controls 0.00 cfs)

Summary for Pond 5P: Drip Edge

Inflow Area	ı =	0.076 ac,10	0.00% Imp	ervious, Inflov	w Depth >	1.77	‴ for	FP1	event	
Inflow	=	0.14 cfs @	12.09 hrs,	Volume=	0.011	af				
Outflow	=	0.03 cfs @	12.50 hrs,	Volume=	0.011	af, A	Atten=	78%,	Lag=	24.5 min
Discarded	=	0.03 cfs @	12.50 hrs,	Volume=	0.011	af			•	
Primary	=	0.00 cfs @	0.00 hrs,	Volume=	0.000	af				

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 229.33' @ 12.50 hrs Surf.Area= 634 sf Storage= 110 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 18.0 min (785.0 - 767.0)

Volume	Invert Av	/ail.Storage	Storage	Description	
#1	228.90'	1,040 cf	Custor 2,599 cf	n Stage Data (Pr f Overall x 40.0%	ismatic) Listed below (Recalc) 6 Voids
Elevation	Surf.Are	a Inc	.Store	Cum.Store	
(feet)	(sq-f	t) (cubi	c-feet)	(cubic-feet)	
228.90	63	4	0	0	
229.00	63	4	63	63	
230.00	63	4	634	697	
232.00	63	4	1,268	1,965	
233.00	63	4	634	2,599	

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Device	Routing	Invert	Outlet Devices
#1	Discarded	228.90'	2.000 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 220.83'
#2	Primary	232.00'	132.0' long x 1.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00
			Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31
			3.30 3.31 3.32

Discarded OutFlow Max=0.03 cfs @ 12.50 hrs HW=229.33' (Free Discharge) **1=Exfiltration** (Controls 0.03 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=228.90' TW=220.80' (Dynamic Tailwater) ←2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 6P: Drip Edge

Inflow Area	ı =	0.204 ac,10	0.00% Impe	rvious,	Inflow Depth >	1.77"	for FF	1 event	
Inflow	=	0.38 cfs @	12.09 hrs, '	Volume	= 0.030	af			
Outflow	=	0.00 cfs @	0.00 hrs, `	Volume	= 0.000	af, At	ten= 100	%, Lag=	0.0 min
Primary	=	0.00 cfs @	0.00 hrs, `	Volume	= 0.000	af		-	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 221.07' @ 24.00 hrs Surf.Area= 1,509 sf Storage= 1,310 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= (not calculated: no outflow)

Volume	Inv	ert Avail.Sto	orage Storag	je Description	
#1	218.9	90' 2,4	75 cf Custo 6,187 d	m Stage Data (Prismatic) Listed below (Recalc) cf Overall x 40.0% Voids	
Elevatio (fee	n t)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
218.9 219.0 220.0 222.0 223.0	0 0 0 0 0	1,509 1,509 1,509 1,509 1,509	0 151 1,509 3,018 1,509	0 151 1,660 4,678 6,187	
Device	Routing	Invert	Outlet Devic	ces	
#1	Primary	222.00'	312.0' long Head (feet) 2.50 3.00 Coef. (Englis 3.30 3.31 3	x 1.0' breadth Broad-Crested Rectangular Weir 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 sh) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3. 3.32	2.00 31

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=218.90' TW=0.00' (Dynamic Tailwater) **1=Broad-Crested Rectangular Weir** (Controls 0.00 cfs)

Summary for Pond CB1: CB1

 Inflow Area =
 0.129 ac,100.00% Impervious, Inflow Depth > 1.77" for FP1 event

 Inflow =
 0.24 cfs @ 12.09 hrs, Volume=
 0.019 af

 Outflow =
 0.24 cfs @ 12.09 hrs, Volume=
 0.019 af, Atten= 0%, Lag= 0.0 min

 Primary =
 0.24 cfs @ 12.09 hrs, Volume=
 0.019 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 212.35' @ 12.83 hrs Flood Elev= 215.17'

Device	Routing	Invert	Outlet Devices
#1	Primary	211.92'	15.0" Round Culvert
	-		L= 20.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 211.92' / 211.82' S= 0.0050 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf

Primary OutFlow Max=0.20 cfs @ 12.09 hrs HW=212.23' TW=212.15' (Dynamic Tailwater) -1=Culvert (Outlet Controls 0.20 cfs @ 1.28 fps)

Summary for Pond CB2: CB2

Inflow Area	a =	0.300 ac,10	0.00% Imper\	vious, Inflow De	pth > 1.77"	for FP1	event
Inflow	=	0.56 cfs @	12.09 hrs, V	olume=	0.044 af		
Outflow	=	0.56 cfs @	12.09 hrs, V	olume=	0.044 af, At	ten= 0%,	Lag= 0.0 min
Primary	=	0.56 cfs @	12.09 hrs, V	olume=	0.044 af		

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 212.35' @ 12.79 hrs Flood Elev= 215.17'

Device	Routing	Invert	Outlet Devices
#1	Primary	211.72'	15.0" Round Culvert
			L= 20.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 211.72' / 211.62' S= 0.0050 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf

Primary OutFlow Max=0.54 cfs @ 12.09 hrs HW=212.15' TW=211.78' (Dynamic Tailwater) ☐ 1=Culvert (Barrel Controls 0.54 cfs @ 2.18 fps)

Summary for Pond CB3: CB3

Inflow Area	a =	0.293 ac,	0.00% Impervious,	Inflow Depth >	0.32" for	FP1 event
Inflow	=	0.07 cfs @	12.17 hrs, Volume	= 0.008 a	af	
Outflow	=	0.07 cfs @	12.17 hrs, Volume	= 0.008 a	af, Atten= (0%, Lag= 0.0 min
Primary	=	0.07 cfs @	12.17 hrs, Volume	= 0.008 a	af	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 225.15' @ 12.17 hrs Flood Elev= 229.00'

Type III 24-hr FP1 Rainfall=2.00" Printed 10/29/2021 _C Page 41

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Device	Routing	Invert	Outlet Devices
#1	Primary	225.00'	12.0" Round Culvert L= 120.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 225.00' / 224.40' S= 0.0050 '/' Cc= 0.900
			II- 0.013 Collugated PE, shooth intenor, Flow Area- 0.79 si

Primary OutFlow Max=0.07 cfs @ 12.17 hrs HW=225.15' TW=0.00' (Dynamic Tailwater) ☐ 1=Culvert (Barrel Controls 0.07 cfs @ 1.37 fps)

Summary for Pond FP1: FocalPoint 1

Inflow Area	=	0.410 ac, 8	5.11% Impervi	ious, Inflow D	epth > 1.40"	for FP1 e	event
Inflow	=	0.65 cfs @	12.09 hrs, Vo	lume=	0.048 af		
Outflow	=	0.23 cfs @	12.36 hrs, Vo	lume=	0.048 af, Atte	en= 64%,	Lag= 16.0 min
Primary	=	0.23 cfs @	12.36 hrs, Vo	lume=	0.048 af		

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 229.83' @ 12.37 hrs Surf.Area= 80 sf Storage= 344 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 8.4 min (811.6 - 803.2)

Volume	Invert	Avail.Stor	rage S	storage D	escription		
#1	228.81'	3	36 cf 1	0.00'W x	8.00'L x 2.25	'H FocalPoint	
			1	80 ct Ove	erall x 20.0%	Voids	(-
#2	228.80	32	27 ct S	urface B	owl Area (Pr	ismatic)Listed below	/ (Recalc) -Impervious
		36	53 cf 1	otal Avail	lable Storage		
Elevatio	on Si	urf.Area	Inc.S	tore	Cum.Store		
(fee	et)	(sq-ft)	(cubic-f	eet)	(cubic-feet)		
228.8	80	250		0	0		
228.8	81	250		2	2		
229.8	81	400		325	327		
Device	Routing	Invert	Outlet	Devices			
#1	Device 2	229.81'	15.0"	Horiz. Ori	ifice/Grate)= 0.600	
#0	Drimon	225 661			iow at iow nea	aus	
#2	Phillary	223.00	1 5.0		projecting no	boodwall Ko- 0.00	0
			L- 10.	J CFF, Outlet Inv	projecting, no	225 56' S- 0.0100	
			n = 0.0	13 Corru	anted PE sm	223.30 $3-0.0100$	7 - 0.00
#3	Drimony	228 81	100.00	0 in/br E	viltration ov	or Surface area	1.20 SI
#3	Filliary	220.01	Condu		Groupdwater	Elovation - 220.92'	Phase In- 0.01'
			Condu		Gioundwaler	LIEVALION - 220.03	F 1103C-111- 0.01

Primary OutFlow Max=0.23 cfs @ 12.36 hrs HW=229.82' TW=223.93' (Dynamic Tailwater)

2=Culvert (Passes 0.02 cfs of 8.78 cfs potential flow) **1=Orifice/Grate** (Weir Controls 0.02 cfs @ 0.40 fps)

-3=Exfiltration (Controls 0.21 cfs)

Summary for Pond FP2: FocalPoint 2

Inflow Area	=	0.339 ac, 9	0.79% Impe	ervious,	Inflow Depth	ו> 1.5	57" for	FP1	event	
Inflow	=	0.59 cfs @	12.09 hrs,	Volume	= 0.0	044 af				
Outflow	=	0.21 cfs @	12.36 hrs,	Volume	= 0.0	044 af,	Atten= 6	65%,	Lag= 10	6.6 min
Primary	=	0.21 cfs @	12.36 hrs,	Volume	= 0.0	044 af				

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 229.67' @ 12.36 hrs Surf.Area= 80 sf Storage= 286 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 6.9 min (795.0 - 788.1)

Volume	Invert	Avail.Stor	rage	Storage De	escription			
#1	228.81'	3	36 cf	10.00'W x	8.00'L x 2.25	5'H FocalF	Point	
				180 cf Ove	rall x 20.0%	Voids		
#2	228.80'	32	27 cf	Surface Bo	owl Area (Pr	rismatic)L	isted belov	v (Recalc) -Impervious
		36	63 cf	Total Availa	able Storage			
Elevatio (fee	on Su et)	urf.Area (sq-ft)	Inc. (cubic	Store -feet)	Cum.Store (cubic-feet)			
228.8	30	250		0	0			
228.8	81	250		2	2			
229.8	81	400		325	327			
Device	Routing	Invert	Outle	t Devices				
#1	Device 2	229.81'	15.0"	' Horiz. Orif	fice/Grate (C= 0.600		
#2	Primary	225.66'	15.0 " L= 10 Inlet	' Round Cu).0' CPP, p / Outlet Inve	ow at low he ulvert projecting, no ert= 225.66' /	headwall 225.56'	, Ke= 0.90 S= 0.0100	00 '/' Cc= 0.900
#3	Primary	228.81'	n= 0. 100.0 Cond	013 Corrug 000 in/hr Ex luctivity to C	Gated PE, sm cfiltration ov Groundwater	ver Surfac Elevation	or, Flow <i>F</i> e area = 220.83'	Area= 1.23 st Phase-In= 0.01'
Primary	OutFlow M	ax=0.21 cfs @	0 12.3	6 hrs HW=:	229.67' TW=	=223.93'	(Dynamic [·]	Tailwater)

-2=Culvert (Passes 0.00 cfs of 8.58 cfs potential flow)

1=Orifice/Grate (Controls 0.00 cfs)

-3=Exfiltration (Controls 0.21 cfs)

Summary for Pond FP3: FocalPoint 3

Inflow Area	=	0.336 ac, 7	78.26% Impe	ervious,	Inflow Depth >	1.31"	for FP1	event
Inflow	=	0.50 cfs @	12.09 hrs,	Volume	= 0.037	af		
Outflow	=	0.20 cfs @	12.34 hrs,	Volume	= 0.037	af, At	ten= 61%,	Lag= 14.9 min
Primary	=	0.20 cfs @	12.34 hrs,	Volume	= 0.037	af		

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 226.38' @ 12.34 hrs Surf.Area= 80 sf Storage= 203 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow)

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Volume	Inve	rt Avail.Sto	rage	Storage D	escription		
#1	225.74	4' :	36 cf	10.00'W x	8.00'L x 2.25'	H FocalPoint	
#2	225.73	3' 32	28 cf	Surface E	Sowl Area (Pris	smatic)Listed below	(Recalc) -Impervious
		36	64 cf	Total Avai	lable Storage		
Elevatio	on s	Surf.Area	Inc.	Store	Cum.Store		
(fee	et)	(sq-ft)	(cubic	-feet)	(cubic-feet)		
225.	73	250		0	0		
225.7	74	250		3	3		
226.7	74	400		325	328		
Device	Routing	Invert	Outle	t Devices			
#1	Device 2	226.74'	15.0"	Horiz. Or	ifice/Grate C	= 0.600	
			Limite	ed to weir f	low at low hea	ds	
#2	Primary	222.49'	12.0"	Round C	ulvert		
			L= 10	0.0' CPP,	projecting, no	headwall, Ke= 0.90	0
			Inlet /	Outlet Inv	ert= 222.49' / 2	222.39' S= 0.0100	'/' Cc= 0.900
			n= 0.0	013 Corru	gated PE, smc	ooth interior, Flow A	rea= 0.79 sf
#3	Primary	225.74'	100.0	00 in/hr E	xfiltration ove	er Surface area	
			Cond	uctivity to	Groundwater E	Elevation = 215.39'	Phase-In= 0.01'

Center-of-Mass det. time= 5.2 min (814.8 - 809.5)

Primary OutFlow Max=0.20 cfs @ 12.34 hrs HW=226.38' TW=221.08' (Dynamic Tailwater)

-2=Culvert (Passes 0.00 cfs of 5.49 cfs potential flow) -1=Orifice/Grate (Controls 0.00 cfs)

-3=Exfiltration (Controls 0.20 cfs)

Summary for Pond FP4: FocalPoint 4

Inflow Area	=	0.121 ac,10	0.00% Impe	ervious,	Inflow Depth	h> 1.7	'7" for	FP1	event
Inflow	=	0.23 cfs @	12.09 hrs,	Volume	= 0.0	018 af			
Outflow	=	0.19 cfs @	12.15 hrs,	Volume	= 0.0	015 af,	Atten=	17%,	Lag= 3.8 min
Primary	=	0.19 cfs @	12.15 hrs,	Volume	= 0.0	015 af			

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 192.83' @ 12.14 hrs Surf.Area= 80 sf Storage= 157 cf

Plug-Flow detention time= 124.7 min calculated for 0.015 af (82% of inflow) Center-of-Mass det. time= 54.5 min (821.4 - 767.0)

Volume	Invert	Avail.Storage	Storage Description
#1	192.80'	36 cf	10.00'W x 8.00'L x 2.25'H FocalPoint
			180 cf Overall x 20.0% Voids
#2	192.29'	328 cf	193.7 (Prismatic) Listed below (Recalc) - Impervious
		364 cf	Total Available Storage

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Elevation Surf.Area (feet) (sq-ft)		Inc.Store (cubic-feet)	Cum.Store (cubic-feet)				
192.2	192.29 250		0 0				
192.3	30	250	3	3			
193.3	30	400	325	328			
Device	Routing	Invert	Outlet Devices				
#1	Device 2	193.80'	15.0" Horiz. Orifice/Grate C= 0.600				
#2	Primary	189.80'	6.0" Round Culvert L= 15.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 189.80' / 189.70' S= 0.0067 '/' Cc= 0.900 n= 0.013 Corrugated PE smooth interior Flow Area= 0.20 sf				
#3	Primary	192.80'	100.000 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 188.00' Phase-In= 0.01'			Phase-In= 0.01'	

Primary OutFlow Max=0.19 cfs @ 12.15 hrs HW=192.83' TW=0.00' (Dynamic Tailwater) 2=Culvert (Passes 0.00 cfs of 1.24 cfs potential flow) 1=Orifice/Grate (Controls 0.00 cfs) -3=Exfiltration (Controls 0.19 cfs)

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S	Runoff Area=102,651 sf 0.77% Impervious Runoff Depth>3.79" Flow Length=350' Tc=9.6 min CN=72 Runoff=9.15 cfs 0.744 af
Subcatchment2S: Subcatchment2S	Runoff Area=17,857 sf 85.11% Impervious Runoff Depth>6.24" Tc=6.0 min CN=94 Runoff=2.67 cfs 0.213 af
Subcatchment3S: Subcatchment3S	Runoff Area=14,768 sf 90.79% Impervious Runoff Depth>6.48" Tc=6.0 min CN=96 Runoff=2.24 cfs 0.183 af
Subcatchment4S: Subcatchment4S	Runoff Area=12,745 sf 0.00% Impervious Runoff Depth>3.89" Flow Length=350' Tc=9.6 min CN=73 Runoff=1.17 cfs 0.095 af
Subcatchment 5S: Subcatchment 5S	Runoff Area=14,630 sf 78.26% Impervious Runoff Depth>6.13" Tc=6.0 min CN=93 Runoff=2.17 cfs 0.172 af
Subcatchment6S: Subcatchment6S	Runoff Area=104,590 sf 0.00% Impervious Runoff Depth>4.00" Flow Length=597' Tc=14.7 min CN=74 Runoff=8.56 cfs 0.800 af
Subcatchment7S: Subcatchment7S	Runoff Area=5,959 sf 0.00% Impervious Runoff Depth>4.00" Tc=6.0 min CN=74 Runoff=0.63 cfs 0.046 af
Subcatchment7S1: SubcatchmentCB1	Runoff Area=5,639 sf 100.00% Impervious Runoff Depth>6.72" Tc=6.0 min CN=98 Runoff=0.86 cfs 0.072 af
Subcatchment7S2: SubcatchmentCB2	Runoff Area=7,419 sf 100.00% Impervious Runoff Depth>6.72" Tc=6.0 min CN=98 Runoff=1.14 cfs 0.095 af
Subcatchment8S: Subcatchment8S	Runoff Area=5,280 sf 100.00% Impervious Runoff Depth>6.72" Tc=6.0 min CN=98 Runoff=0.81 cfs 0.068 af
Subcatchment9S: Subcatchment9S	Runoff Area=3,313 sf 100.00% Impervious Runoff Depth>6.72" Tc=6.0 min CN=98 Runoff=0.51 cfs 0.043 af
Subcatchment 10S: Subcatchment 10S	Runoff Area=8,865 sf 100.00% Impervious Runoff Depth>6.72" Tc=6.0 min CN=98 Runoff=1.36 cfs 0.114 af
Subcatchment11S: Subcatchment11S	Runoff Area=18,787 sf 52.98% Impervious Runoff Depth>5.44" Tc=6.0 min CN=87 Runoff=2.59 cfs 0.195 af
Subcatchment 12S: Subcatchment 11S	Runoff Area=5,279 sf 100.00% Impervious Runoff Depth>6.72" Tc=6.0 min CN=98 Runoff=0.81 cfs 0.068 af
Reach 1R: Flow Through Wetland n=0.030 L=2	Avg. Flow Depth=0.04' Max Vel=1.03 fps Inflow=0.77 cfs 0.168 af 10.0' S=0.0548 '/' Capacity=185.74 cfs Outflow=0.76 cfs 0.168 af
Reach AP1: Analysis Point #1	Inflow=23.83 cfs 2.519 af

Outflow=23.83 cfs 2.519 af

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Reach AP2: Analysis Poir	t #2		Inflow=2.59 Outflow=2.59	cfs 0.195 af cfs 0.195 af
Pond 1P: STORMTECH1	Peak Ele Discarded=0.00 cfs 0.000 af	v=225.30' Storage Primary=1.55 cfs(=0.114 af Inflow=5.08 0.385 af Outflow=1.55	cfs 0.396 af cfs 0.385 af
Pond 2P: STORMTECH 2	Peak Ele Discarded=0.00 cfs 0.000 af	v=222.35' Storage Primary=0.77 cfs(=0.040 af Inflow=2.57 0.168 af Outflow=0.77	cfs 0.171 af cfs 0.168 af
Pond 3P: Pond 3P	Peak Ele	v=213.22' Storage	=2,916 cf Inflow=2.63 Outflow=2.07	cfs 0.213 af cfs 0.184 af
Pond 4P: Drip Edge	Peak E Discarded=0.05 cfs 0.060 af	lev=232.01' Stora Primary=0.53 cfs	ge=941 cf Inflow=0.81 0.008 af Outflow=0.58	cfs 0.068 af cfs 0.068 af
Pond 5P: Drip Edge	Peak E Discarded=0.04 cfs 0.043 af	lev=231.73' Stora Primary=0.00 cfs(ge=719 cf Inflow=0.51 0.000 af Outflow=0.04	cfs 0.043 af cfs 0.043 af
Pond 6P: Drip Edge	Peak Ele	v=222.02' Storage	=1,881 cf Inflow=1.36 Outflow=1.77	cfs 0.114 af cfs 0.071 af
Pond CB1: CB1	15.0" Round Culvert n=0	Peak Ele 0.013 L=20.0' S=0	v=213.31' Inflow=0.86 .0050 '/' Outflow=0.86	cfs 0.072 af cfs 0.072 af
Pond CB2: CB2	15.0" Dound Culvert n=0	Peak Ele	v=213.30' Inflow=2.00	cfs 0.168 af

Peak Elev=213.30' Inflow=2.00 cfs 0.168 af 15.0" Round Culvert n=0.013 L=20.0' S=0.0050 '/' Outflow=2.00 cfs 0.168 af

 Pond CB3: CB3
 Peak Elev=225.66'
 Inflow=1.17 cfs
 0.095 af

 12.0"
 Round Culvert
 n=0.013
 L=120.0'
 S=0.0050 '/'
 Outflow=1.17 cfs
 0.095 af

 Pond FP1: FocalPoint 1
 Peak Elev=230.15' Storage=349 cf Inflow=2.67 cfs 0.213 af Outflow=2.77 cfs 0.213 af Outflow=2.77 cfs 0.213 af Outflow=2.77 cfs 0.213 af Outflow=2.24 cfs 0.183 af Outflow=2.32 cfs 0.183 af Outflow=2.32 cfs 0.183 af Outflow=2.32 cfs 0.183 af Outflow=2.57 cfs 0.172 af Outflow=2.57 cfs 0.171 af Peak Elev=193.99' Storage=346 cf Inflow=0.81 cfs 0.068 af Outflow=1.25 cfs 0.065 af

Total Runoff Area = 7.525 ac Runoff Volume = 2.908 af Average Runoff Depth = 4.64" 73.58% Pervious = 5.537 ac 26.42% Impervious = 1.988 ac Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S	Runoff Area=102,651 sf 0.77% Impervious Runoff Depth>0.29" Flow Length=350' Tc=9.6 min CN=72 Runoff=0.45 cfs 0.057 af
Subcatchment2S: Subcatchment2S	Runoff Area=17,857 sf 85.11% Impervious Runoff Depth>1.40" Tc=6.0 min CN=94 Runoff=0.65 cfs 0.048 af
Subcatchment3S: Subcatchment3S	Runoff Area=14,768 sf 90.79% Impervious Runoff Depth>1.57" Tc=6.0 min CN=96 Runoff=0.59 cfs 0.044 af
Subcatchment4S: Subcatchment4S	Runoff Area=12,745 sf 0.00% Impervious Runoff Depth>0.32" Flow Length=350' Tc=9.6 min CN=73 Runoff=0.07 cfs 0.008 af
Subcatchment5S: Subcatchment5S	Runoff Area=14,630 sf 78.26% Impervious Runoff Depth>1.31" Tc=6.0 min CN=93 Runoff=0.50 cfs 0.037 af
Subcatchment6S: Subcatchment6S	Runoff Area=104,590 sf 0.00% Impervious Runoff Depth>0.35" Flow Length=597' Tc=14.7 min CN=74 Runoff=0.55 cfs 0.070 af
Subcatchment7S: Subcatchment7S	Runoff Area=5,959 sf 0.00% Impervious Runoff Depth>0.35" Tc=6.0 min CN=74 Runoff=0.04 cfs 0.004 af
Subcatchment7S1: SubcatchmentCB1	Runoff Area=5,639 sf 100.00% Impervious Runoff Depth>1.77" Tc=6.0 min CN=98 Runoff=0.24 cfs 0.019 af
Subcatchment7S2: SubcatchmentCB2	Runoff Area=7,419 sf 100.00% Impervious Runoff Depth>1.77" Tc=6.0 min CN=98 Runoff=0.32 cfs 0.025 af
Subcatchment8S: Subcatchment8S	Runoff Area=5,280 sf 100.00% Impervious Runoff Depth>1.77" Tc=6.0 min CN=98 Runoff=0.23 cfs 0.018 af
Subcatchment9S: Subcatchment9S	Runoff Area=3,313 sf 100.00% Impervious Runoff Depth>1.77" Tc=6.0 min CN=98 Runoff=0.14 cfs 0.011 af
Subcatchment10S: Subcatchment10S	Runoff Area=8,865 sf 100.00% Impervious Runoff Depth>1.77" Tc=6.0 min CN=98 Runoff=0.38 cfs 0.030 af
Subcatchment11S: Subcatchment11S	Runoff Area=18,787 sf 52.98% Impervious Runoff Depth>0.90" Tc=6.0 min CN=87 Runoff=0.45 cfs 0.033 af
Subcatchment 12S: Subcatchment 11S	Runoff Area=5,279 sf 100.00% Impervious Runoff Depth>1.77" Tc=6.0 min CN=98 Runoff=0.23 cfs 0.018 af
Reach 1R: Flow Through Wetland n=0.030 L=2	Avg. Flow Depth=0.02' Max Vel=0.66 fps Inflow=0.18 cfs 0.035 af 10.0' S=0.0548 '/' Capacity=185.74 cfs Outflow=0.18 cfs 0.035 af
Reach AP1: Analysis Point #1	Inflow=1.59 cfs_0.314 af

Outflow=1.59 cfs 0.314 af

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Inflow=0.45 cfs 0.033 af

Reach AP2: Analysis Point #2

•	Outflow=0.45 cfs	0.033 af
Pond 1P: STORMTECH 1	Peak Elev=224.01' Storage=0.031 af Inflow=0.44 cfs Discarded=0.00 cfs 0.000 af Primary=0.34 cfs 0.085 af Outflow=0.34 cfs	0.092 af 0.085 af
Pond 2P: STORMTECH2	Peak Elev=221.11' Storage=0.009 af Inflow=0.20 cfs Discarded=0.00 cfs 0.000 af Primary=0.18 cfs 0.035 af Outflow=0.18 cfs	0.037 af 0.035 af
Pond 3P: Pond 3P	Peak Elev=212.35' Storage=1,001 cf Inflow=0.60 cfs Outflow=0.07 cfs	0.048 af 0.044 af
Pond 4P: Drip Edge	Peak Elev=229.60' Storage=211 cf Inflow=0.23 cfs Discarded=0.04 cfs 0.018 af Primary=0.00 cfs 0.000 af Outflow=0.04 cfs	0.018 af 0.018 af
Pond 5P: Drip Edge	Peak Elev=229.33' Storage=110 cf Inflow=0.14 cfs Discarded=0.03 cfs 0.011 af Primary=0.00 cfs 0.000 af Outflow=0.03 cfs	0.011 af 0.011 af
Pond 6P: Drip Edge	Peak Elev=221.07' Storage=1,310 cf Inflow=0.38 cfs Outflow=0.00 cfs	0.030 af 0.000 af
Pond CB1: CB1	Peak Elev=212.35' Inflow=0.24 cfs 15.0" Round Culvert n=0.013 L=20.0' S=0.0050 '/' Outflow=0.24 cfs	0.019 af 0.019 af
Pond CB2: CB2	Peak Elev=212.35' Inflow=0.56 cfs 15.0" Round Culvert n=0.013 L=20.0' S=0.0050 '/' Outflow=0.56 cfs	0.044 af 0.044 af
Pond CB3: CB3	Peak Elev=225.15' Inflow=0.07 cfs 12.0" Round Culvert n=0.013 L=120.0' S=0.0050 '/' Outflow=0.07 cfs	0.008 af 0.008 af
Pond FP1: FocalPoint 1	Peak Elev=229.83' Storage=344 cf Inflow=0.65 cfs Outflow=0.23 cfs	0.048 af 0.048 af
Pond FP2: FocalPoint 2	Peak Elev=229.67' Storage=286 cf Inflow=0.59 cfs Outflow=0.21 cfs	0.044 af 0.044 af
Pond FP3: FocalPoint 3	Peak Elev=226.38' Storage=203 cf Inflow=0.50 cfs Outflow=0.20 cfs	0.037 af 0.037 af
Pond FP4: FocalPoint 4	Peak Elev=192.83' Storage=157 cf Inflow=0.23 cfs Outflow=0.19 cfs	0.018 af 0.015 af

Total Runoff Area = 7.525 ac Runoff Volume = 0.421 af Average Runoff Depth = 0.67" 73.58% Pervious = 5.537 ac 26.42% Impervious = 1.988 ac

APPENDIX III

Charts, Graphs, and Calculations



21137 - FOCAL POINT	Type III 24-hr	1.22-in Rair	nfall=1.22"
Prepared by {enter your company name here}		Printed	2/10/2022
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Time span=0.00-24.00 hrs, dt=0.01 hrs, 2401 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment2S: Subcatchment2S	Runoff Area=17,980 sf 82.31% Impervious Runoff Depth>0.69" Tc=6.0 min CN=94 Runoff=0.33 cfs 1,032 cf
Subcatchment3S: Subcatchment3S	Runoff Area=14,764 sf 87.15% Impervious Runoff Depth>0.76" Tc=6.0 min CN=95 Runoff=0.30 cfs 931 cf
Subcatchment5S: Subcatchment5S	Runoff Area=16,022 sf 73.94% Impervious Runoff Depth>0.57" Tc=6.0 min CN=92 Runoff=0.25 cfs 762 cf
Subcatchment11S: Subcatchment11S	Runoff Area=7,712 sf 91.44% Impervious Runoff Depth>0.83" Tc=6.0 min CN=96 Runoff=0.17 cfs 534 cf
Pond FP1: FocalPoint 1	Peak Elev=226.81' Storage=95 cf Inflow=0.33 cfs 1,032 cf Outflow=0.15 cfs 1,033 cf
Pond FP2: FocalPoint 2	Peak Elev=226.71' Storage=83 cf Inflow=0.30 cfs 931 cf Outflow=0.14 cfs 931 cf
Pond FP3: FocalPoint 3	Peak Elev=223.48' Storage=45 cf Inflow=0.25 cfs 762 cf Outflow=0.15 cfs 762 cf
Pond FP4: FocalPoint 4	Peak Elev=190.97' Storage=53 cf Inflow=0.17 cfs 534 cf Outflow=0.07 cfs 534 cf

Total Runoff Area = 56,478 sf Runoff Volume = 3,258 cf Average Runoff Depth = 0.69" 17.55% Pervious = 9,914 sf 82.45% Impervious = 46,564 sf

Summary for Subcatchment 2S: Subcatchment 2S

Runoff = 0.33 cfs @ 12.09 hrs, Volume= 1,032 cf, Depth> 0.69"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 1.22-in Rainfall=1.22"

6.0					Direct Entry,		
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)			
Тс	Length	Slope	e Velocity	Capacity	Description		
	3,181 14,799	UT	17.69% Pervious Area 82.31% Impervious Area				
	17 980	94	Weighted Average				
	3,181	74	>75% Ġras	s cover, Go	iood, HSG C		
	809	98	Paved park	ing, HSG C	C		
	13,990	98	Paved park	ing, HSG C	C		
A	Area (sf)	CN	Description				

Summary for Subcatchment 3S: Subcatchment 3S

Runoff = 0.30 cfs @ 12.09 hrs, Volume= 931 cf, Depth> 0.76"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 1.22-in Rainfall=1.22"

A	rea (sf)	CN	Description				
	12,867	98	Paved park	ing, HSG C	2		
	1,897	74	>75% Gras	s cover, Go	bod, HSG C		
	14,764 1,897	95	Weighted Average 12.85% Pervious Area				
	12,807		87.15% imp	bervious Ar	ea		
Tc (min)	Length (feet)	Slope (ft/ft	e Velocity) (ft/sec)	Capacity (cfs)	Description		
6.0					Direct Entry,		

Summary for Subcatchment 5S: Subcatchment 5S

Runoff = 0.25 cfs @ 12.09 hrs, Volume= 762 cf, Depth> 0.57"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 1.22-in Rainfall=1.22"

21137 - FOCAL POINT

 Type III 24-hr
 1.22-in Rainfall=1.22"

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 LLC
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rea (sf)	CN	Description			
10,782	98	Paved park	ing, HSG C	0	
1,064	98	Paved park	ing, HSG C	C	
4,176	74	>75% Gras	s cover, Go	ood, HSG C	
16,022	92	Weighted A	verage		
4,176		26.06% Pervious Area			
11,846		73.94% Impervious Area			
	<u></u>	.,	o		
Length	Slope	e Velocity	Capacity	Description	
(feet)	(ft/ft) (ft/sec)	(cfs)		
				Direct Entry,	
	rea (sf) 10,782 1,064 4,176 16,022 4,176 11,846 Length (feet)	rea (sf) CN 10,782 98 1,064 98 4,176 74 16,022 92 4,176 11,846 Length Slope (feet) (ft/ft	rea (sf) CN Description 10,782 98 Paved park 1,064 98 Paved park 4,176 74 >75% Gras 16,022 92 Weighted A 4,176 26.06% Per 11,846 73.94% Imp Length Slope Velocity (feet) (ft/ft) (ft/sec)	rea (sf)CNDescription10,78298Paved parking, HSG (1,06498Paved parking, HSG (4,17674>75% Grass cover, G16,02292Weighted Average4,17626.06% Pervious Area11,84673.94% Impervious ALengthSlopeVelocity(feet)(ft/ft)(ft/sec)(cfs)	

Summary for Subcatchment 11S: Subcatchment 11S

Runoff	=	0.17 cfs @	12.09 hrs,	Volume=	534 cf, Depth>	0.83"
					ee . e., _ ee	

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 1.22-in Rainfall=1.22"

A	rea (sf)	CN	Description						
	7,052	98	Paved park	ing, HSG C	C				
	660	74	>75% Gras	s cover, Go	ood, HSG C				
	7,712	96	Weighted A	verage					
	660		8.56% Pervious Area						
	7,052		91.44% Imp	pervious Are	ea				
Тс	Length	Slop	e Velocity	Capacity	Description				
(min)	(feet)	(ft/ft	:) (ft/sec)	(cfs)					
6.0					Direct Entry,				

_...**,**,

Summary for Pond FP1: FocalPoint 1

Inflow Area	a =	17,980 sf, 82.31% Impervi	ous, Inflow Depth > 0	.69" for 1.22-in event
Inflow	=	0.33 cfs @ 12.09 hrs, Volur	ne= 1,032 cf	
Outflow	=	0.15 cfs @ 11.99 hrs, Volur	ne= 1,033 cf,	Atten= 54%, Lag= 0.0 min
Primary	=	0.15 cfs @ 11.99 hrs, Volur	ne= 1,033 cf	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 226.81' @ 12.28 hrs Surf.Area= 66 sf Storage= 95 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 2.4 min (825.5 - 823.1)

Volume	Invert	Avail.Storage	Storage Description
#1	225.34'	30 cf	6.00'W x 11.00'L x 2.25'H FocalPoint
			149 cf Overall x 20.0% Voids
#2	226.08'	467 cf	Surface Bowl Area (Prismatic)Listed below (Recalc) - Impervious
		497 cf	Total Available Storage

21137 - FOCAL POINT

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Elevatio	on	Surf.Area	Inc.Store	Cum.Store			
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)			
226.0)8	66	0	0			
226.0)9	66	1	1			
227.3	34	200	166	167			
228.3	34	400	300	467			
Device	Routing	Invert	Outlet Devices				
#1	Device 2	228.84'	15.0" Horiz. Ori	fice/Grate	C= 0.600 ads		
#2	Primary	225.34'	15.0" Round Culvert L= 30.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 225.34' / 225.04' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf				
#3	Primary	225.34'	100.000 in/hr E	xfiltration ov	er Surface area		

Primary OutFlow Max=0.15 cfs @ 11.99 hrs HW=225.41' (Free Discharge)

2=Culvert (Passes 0.00 cfs of 0.02 cfs potential flow) **1=Orifice/Grate** (Controls 0.00 cfs)

-3=Exfiltration (Exfiltration Controls 0.15 cfs)

Summary for Pond FP2: FocalPoint 2

Inflow Area	a =	14,764 sf,	87.15% Im	pervious,	Inflow Depth	> 0.76	6" for 1.2	2-in event
Inflow	=	0.30 cfs @ 1	2.09 hrs, \	/olume=	931	l cf		
Outflow	=	0.14 cfs @ 1	1.99 hrs, \	/olume=	931	l cf, At	tten= 54%,	Lag= 0.0 min
Primary	=	0.14 cfs @ 1	1.99 hrs, \	/olume=	931	l cf		

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 226.71' @ 12.27 hrs Surf.Area= 60 sf Storage= 83 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 2.3 min (817.2 - 814.9)

Volume	Inve	rt Avail.Sto	rage	Storage D	escription	
#1	225.3	4' 2	27 cf	10.00'W x	6.00'L x 2.25'l	H FocalPoint
				135 cf Ov	erall_x 20.0%	/oids
#2	226.0	<u>8' 5'</u>	19 cf	Surface E	Bowl Area (Pris	smatic) Listed below (Recalc) -Impervious
		54	46 cf	Total Avai	lable Storage	
Elevation		Surf.Area	Inc	.Store	Cum.Store	
(feet)		(sq-ft)	(cubi	c-feet)	(cubic-feet)	
226.08		60		0	0	
226.09		60		1	1	
227.34		250		194	194	
228.34		400		325	519	
Device F	Routing	Invert	Outle	et Devices		
#1 [Device 2	228.84'	15.0 Limit	" Horiz. Or ted to weir	fice/Grate Cate Cate Cate Cate Cate Cate Cate C	= 0.600 ds
#2 F	Primary	225.34'	15.0	" Round C	Culvert	

21137 - FOCAL POINT

#3

Type III 24-hr 1.22-in Rainfall=1.22" Printed 2/10/2022 Page 6

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> L= 30.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 225.34' / 224.74' S= 0.0200 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf Primary 225.34' 100.000 in/hr Exfiltration over Surface area Phase-In= 0.01'

Primary OutFlow Max=0.14 cfs @ 11.99 hrs HW=225.42' (Free Discharge)

-2=Culvert (Passes 0.00 cfs of 0.02 cfs potential flow)

1=Orifice/Grate (Controls 0.00 cfs)

-3=Exfiltration (Exfiltration Controls 0.14 cfs)

Summary for Pond FP3: FocalPoint 3

Inflow A	rea =	16,022 sf, 73.94% Impervious,	Inflow Depth > 0.57" for 1.22-in event
Inflow	=	0.25 cfs @ 12.09 hrs, Volume=	762 cf
Outflow	=	0.15 cfs @ 12.21 hrs, Volume=	762 cf, Atten= 41%, Lag= 6.9 min
Primary	=	0.15 cfs @ 12.21 hrs, Volume=	762 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 223.48' @ 12.21 hrs Surf.Area= 54 sf Storage= 45 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 1.1 min (838.4 - 837.4)

Volume	Inver	t Avail.Sto	rage	Storage D	escription		
#1	222.32	'	24 cf	9.00'W x 6	6.00'L x 2.25'l	H FocalPoint	
				122 cf Ove	erall x 20.0%	Voids	
#2	223.06	' 4	59 cf	Surface B	owl Area (Pr	ismatic)Listed below	/ (Recalc) -Impervious
		43	84 cf	Total Avai	lable Storage		
Elevatio	on S	urf.Area	Inc	.Store	Cum.Store		
(fee	et)	(sq-ft)	(cubio	c-feet)	(cubic-feet)		
223.0	06	54		0	0		
223.0	07	54		1	1		
224.3	32	200		159	159		
225.3	32	400		300	459		
Device	Routing	Invert	Outle	et Devices			
#1	Device 2	225.82'	12.0	" Horiz. Or	ifice/Grate	C= 0.600	
			Limit	ed to weir f	low at low hea	ads	
#2	Primary	222.32'	12.0	" Round C	ulvert		
			L= 2	0.0' CPP,	projecting, no	headwall, Ke= 0.90	0
			Inlet	/ Outlet Inv	ert= 222.32' /	222.12' S= 0.0100	'/' Cc= 0.900
			n= 0	.013 Corru	gated PE, sm	ooth interior, Flow A	vrea= 0.79 sf
#3	Primary	222.32'	100.	000 in/hr E	xfiltration ov	er Surface area	
			Cond	ductivity to	Groundwater	Elevation = 215.39'	Phase-In= 0.01'

Primary OutFlow Max=0.15 cfs @ 12.21 hrs HW=223.48' (Free Discharge)

2=Culvert (Passes 0.00 cfs of 2.42 cfs potential flow) **1=Orifice/Grate** (Controls 0.00 cfs)

-3=Exfiltration (Controls 0.15 cfs)

Summary for Pond FP4: FocalPoint 4

Inflow Area	a =	7,712 sf,	91.44% Impervious,	Inflow Depth >	0.83" for 1.22-in	event
Inflow	=	0.17 cfs @	12.09 hrs, Volume=	534 cf		
Outflow	=	0.07 cfs @	11.97 hrs, Volume=	534 cf	, Atten= 57%, La	g= 0.0 min
Primary	=	0.07 cfs @	11.97 hrs, Volume=	534 cf		-

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 190.97' @ 12.29 hrs Surf.Area= 32 sf Storage= 53 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 2.8 min (808.4 - 805.6)

<u>Volume</u>	Invert	Avail.Stor	rage	Storage D	escription	
#1	189.50'	1	4 cf	4.00'W x 8	3.00'L x 2.25'H	I FocalPoint
				72 cf Over	all_x 20.0% V	loids
#2	190.24'	33	34 cf	Surface B	owl Area (Pri	ismatic)Listed below (Recalc) -Impervious
		34	8 cf	Total Avai	lable Storage	
Elevatio	n Si	urf Area	Inc	Store	Cum Store	
	11 OC t)	(sq_ft)	(cubic	-feet)	(cubic-feet)	
	4	(34-11)	(Cubic	<u>-icci)</u>		
190.2	4	24		0	0	
190.2	5	24		0	0	
191.5	0	150		109	109	
192.5	0	300		225	334	
Device	Routing	Invert	Outle	et Devices		
#1	Device 2	193.00'	12.0	" Horiz, Or	ifice/Grate C	c = 0.600
			l imit	ed to weir f	low at low hea	ads
#2	Drimory	180 50'	12 0	" Pound C	ulvort	
#2	i iiiiai y	109.00	12.0		projecting no	boodwall Ko= 0.000
						$\frac{11640}{400} \frac{100}{100} $
			Inlet	/ Outlet Inv	ert= 189.50 /	189.40° S= 0.0100 /° Cc= 0.900
			n= 0	.013 Corru	gated PE, smo	ooth interior, Flow Area= 0.79 sf
#3	Primary	189.50'	100.	000 in/hr E	xfiltration over	er Surface area Phase-In= 0.01'

Primary OutFlow Max=0.07 cfs @ 11.97 hrs HW=189.54' (Free Discharge)

2=Culvert (Passes 0.00 cfs of 0.00 cfs potential flow) **1=Orifice/Grate** (Controls 0.00 cfs)

-3=Exfiltration (Exfiltration Controls 0.07 cfs)

^{0.25} ac (A) ^{0.16} ac **(B)**

54.6 sf

⁶⁶ sf

11 ft

FOCALPOINT -1 **NEW HAMPSHIRE AOT PROJECTS**

- 1. Determine FocalPoint bed area (minimum 174 sf/acre of impervious area ex: 0.2 acres = 35 sf) See step 2 to determine if minimum size is appropriate.
 - Tributary impervious area:
 - Tributary pervious area:
 - Minimum FocalPoint bed area required: = ((A x 1.0) + (B x 0.4)) * 174
 - FocalPoint bed area provided:
 - Dimensions of proposed FocalPoint:
- 2. Model a Type II & III 24-hr rainfall event that generates the water quality volume to demonstrate that the entire storm volume is treated prior to activation of the overflow (typically set at 6 - 12 in above the mulch). Note: a 1.2 - 1.3 in rainfall event usually generates 1.0 in of runoff. Contact ACE for a sample HydroCAD node

=	001 C12
	091 ft3
=	<u> </u>
=	⁶ in
(typic	ally 6 - 12 in)
=	467 ft ³
=	^{226.81} in
	= = =(typic =

3. Size the Harco PVC domed overflow riser. Note: ACF recommends installation of a Fabco domed overflow filter kit for overflow protection.

 Domed overflow riser diameter: 	=	¹⁵ ir
Rim elevation of overflow riser:	=	228.84
 6 in invert in elevation from FocalPoint: 	=	225.34
• <u>15</u> invert out elevation:	=	225.34

4. Flood control - peak flow attenuation of major storms

The treated flow and bypass flow can be routed to a detention system such as an open pond or a subsurface solution like an expanded R-Tank system. (contact ACF for additional information on designing expanded R-Tank systems)

- 5. Prepare a landscape plan for the FocalPoint bed area
- 6. Design review and installation oversight by manufacturer's representative
 - The design has been reviewed by ACF Environmental
 - Engineer will coordinate installation inspection with ACF Environmental



=_____





FOCALPOINT -2 NEW HAMPSHIRE AOT PROJECTS

- 1. Determine FocalPoint bed area (minimum 174 sf/acre of impervious area ex: 0.2 acres = 35 sf) See step 2 to determine if minimum size is appropriate.
 - Tributary impervious area:
 - Tributary pervious area:
 - Minimum FocalPoint bed area required: = ((A x 1.0) + (B x 0.4)) * 174
 - FocalPoint bed area provided:
 - Dimensions of proposed FocalPoint:
- 2. Model a Type II & III 24-hr rainfall event that generates the water quality volume to demonstrate that the entire storm volume is treated prior to activation of the overflow (typically set at 6 12 in above the mulch). Note: a 1.2 1.3 in rainfall event usually generates 1.0 in of runoff.

Contact ACF for a sample HydroCAD node. Water quality volume (WQv) goal: Type II & III 24-hr rainfall depth to generate WQv:

- Temporary storage depth provided:
- Temporary storage volume provided at above depth:
- Peak ponding depth from Type III 24-hr storm event:

3. Size the Harco PVC domed overflow riser.

 Domed overflow riser diameter: 	=	¹⁵ in
Rim elevation of overflow riser:	=	228.84
 6 in invert in elevation from FocalPoint: 	=	225.34
• <u>15</u> invert out elevation:	=	225.34

4. Flood control - peak flow attenuation of major storms

The treated flow and bypass flow can be routed to a detention system such as an open pond or a subsurface solution like an expanded R-Tank system. (contact ACF for additional information on designing expanded R-Tank systems)

- 5. Prepare a landscape plan for the FocalPoint bed area
- 6. Design review and installation oversight by manufacturer's representative
 - The design has been reviewed by ACF Environmental
 - Engineer will coordinate installation inspection with ACF Environmental



= _____(typically 6 - 12 in)

=_____

= _____ 519 ft³

1007 ft³ 1.22 in

⁶ in

226.71 in



FOCALPOINT - 3 NEW HAMPSHIRE AOT PROJECTS

- 1. Determine FocalPoint bed area (minimum 174 sf/acre of impervious area ex: 0.2 acres = 35 sf) See step 2 to determine if minimum size is appropriate.
 - Tributary impervious area:
 - Tributary pervious area:
 - Minimum FocalPoint bed area required: = ((A x 1.0) + (B x 0.4)) * 174
 - FocalPoint bed area provided:
 - Dimensions of proposed FocalPoint:
- Model a Type II & III 24-hr rainfall event that generates the water quality volume to demonstrate that the entire storm volume is treated prior to activation of the overflow (typically set at 6 12 in above the mulch). Note: a 1.2 1.3 in rainfall event usually generates 1.0 in of runoff.

Contact ACF for a sample HydroCAD node.

 Water quality volume (WQv) goal: 	=	949 ft ³
 Type II & III 24-hr rainfall depth to generate WQv: 	=	1.22 in
Temporary storage depth provided:	=	<u>6</u> in
		(typically 6 - 12 in)
 Temporary storage volume provided at above depth: 	=	459 ft ³
 Peak ponding depth from Type III 24-hr storm event: 	=	^{223.48} in

3. Size the Harco PVC domed overflow riser. Note: ACF recommends installation of a Fabco domed overflow filter kit for overflow protection.

Note: Act recommends instandion of a rubeo domed ov		on protection
 Domed overflow riser diameter: 	=	12 ir
Rim elevation of overflow riser:	=	225.82
• 6 in invert in elevation from FocalPoint:	=	222.32
• <u>12</u> invert out elevation:	=	222.32

4. Flood control - peak flow attenuation of major storms

The treated flow and bypass flow can be routed to a detention system such as an open pond or a subsurface solution like an expanded R-Tank system. (contact ACF for additional information on designing expanded R-Tank systems)

- 5. Prepare a landscape plan for the FocalPoint bed area
- 6. Design review and installation oversight by manufacturer's representative
 - The design has been reviewed by ACF Environmental
 - Engineer will coordinate installation inspection with ACF Environmental



FOCALPOINT - 4 **NEW HAMPSHIRE AOT PROJECTS**

- 1. Determine FocalPoint bed area (minimum 174 sf/acre of impervious area ex: 0.2 acres = 35 sf) See step 2 to determine if minimum size is appropriate.
 - Tributary impervious area:
 - Tributary pervious area:
 - Minimum FocalPoint bed area required: = ((A x 1.0) + (B x 0.4)) * 174
 - FocalPoint bed area provided:
 - Dimensions of proposed FocalPoint:

- ^{0.162} ac (A) ^{0.015} ac **(B)** =_____ 21.10 sf = ²⁹ sf 8 ft
- 2. Model a Type II & III 24-hr rainfall event that generates the water quality volume to demonstrate that the entire storm volume is treated prior to activation of the overflow (typically set at 6 - 12 in above the mulch). Note: a 1.2 - 1.3 in rainfall event usually generates 1.0 in of runoff. Contact ACE for a sample HydroCAD node

• Water quality volume (WQv) goal:	=	555_ft ^a
• Type II & III 24-hr rainfall depth to generate WQv:	=	1.22_ in
Temporary storage depth provided:	=	6 in
	(typic	ally 6 - 12 in)
 Temporary storage volume provided at above depth: 	=	<u>334</u> ft ³
• Peak ponding depth from Type III 24-hr storm event:	=	^{190.97} in

3. Size the Harco PVC domed overflow riser. Note: ACE recommends installation of a Eaboa demod overflow filter kit for overflow protection

Note. Acr recomments instantion of a rabco domed over now	Inter Kit für Överni	ow protection.
 Domed overflow riser diameter: 	=	¹² in
Rim elevation of overflow riser:	=	193.0
• 6 in invert in elevation from FocalPoint:	=	189.5
• <u>12</u> " invert out elevation:	=	189.5

• ^{12"} invert out elevation:

4. Flood control - peak flow attenuation of major storms

The treated flow and bypass flow can be routed to a detention system such as an open pond or a subsurface solution like an expanded R-Tank system. (contact ACF for additional information on designing expanded R-Tank systems)

- 5. Prepare a landscape plan for the FocalPoint bed area
- 6. Design review and installation oversight by manufacturer's representative
 - The design has been reviewed by ACF Environmental
 - Engineer will coordinate installation inspection with ACF Environmental



DESIGNING WITH FOCALPOINT IN NEW HAMPSHIRE

The New Hampshire Department of Environmental Services has approved the FocalPoint (High Performance Modular Biofiltration System) for use on AoT site development projects in the State of New Hampshire.

SIZING CRITERIA SUMMARY

- The surface area of the media within FocalPoint must be a minimum of 174 sf per 1.0 acre of impervious area (26 sf per 0.15 acres). The thickness of the media is to be no less than 1.5 ft (18 in).
- The system must be modelled in HydroCAD (or similar TR-55 modeling software) to demonstrate that the entire volume of a 1.22 in Type II or III 24-hr storm is treated prior to activation of the bypass/overflow (typically set at 6 12 in above the mulch surface). Note: A 1.22 in rainfall event typically generates 1.0 in of runoff.
- The R-Tank modular underdrain can be expanded beyond the footprint of the FocalPoint media bed for expanded infiltration and peak flow attenuation/detention post treatment.

FOCALPOINT SYSTEMS:



FOCALPOINT ACCESSORIES:



Pretreatment - Rain Guardian Turret



Pretreatment - Rain Guardian Foxhole



Pretreatment - PreTx



Bypass protection - Domed overflow with filter insert

For additional information please visit: www.acfenvironmental.com

Contact Rob Woodman - Senior Stormwater Engineer Cell: 207.272.4431 | Email: rwoodman@acfenv.com





This worksheet may be useful when designing a BMP **that does not fit into one of the specific worksheets already provided** (i.e. for a technology which is not a stormwater wetland, infiltration practice, etc.)

Water Quality Volume (WQV)

0.41	ас	A = Area draining to the practice
0.25	ас	A _I = Impervious area draining to the practice
0.61	decimal	I = Percent impervious area draining to the practice, in decimal form
0.60	unitless	Rv = Runoff coefficient = 0.05 + (0.9 x l)
0.25	ac-in	WQV= 1" x Rv x A
891	cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")

Water Quality Flow (WQF)

1	inches	P = Amount of rainfall. For WQF in NH, P = 1".
0.60	inches	Q = Water quality depth. Q = WQV/A
96	unitless	CN = Unit peak discharge curve number. CN =1000/(10+5P+10Q-10*[Q ² + 1.25*Q*P] ^{0.5})
0.5	inches	S = Potential maximum retention. S = (1000/CN) - 10
0.093	inches	Ia = Initial abstraction. Ia = 0.2S
6.0	minutes	T _c = Time of Concentration
	cfs/mi²/in	${\sf q}_{\sf u}$ is the unit peak discharge. Obtain this value from TR-55 exhibits 4-II and 4-III.
-	cfs	WQF = $q_u \times WQV$. Conversion: to convert "cfs/mi ² /in * ac-in" to "cfs" multiply by 1mi ² /640ac.



This worksheet may be useful when designing a BMP **that does not fit into one of the specific worksheets already provided** (i.e. for a technology which is not a stormwater wetland, infiltration practice, etc.)

Water Quality Volume (WQV)

0.33 a	ас	A = Area draining to the practice
0.29 a	ас	A ₁ = Impervious area draining to the practice
0.88 0	decimal	I = Percent impervious area draining to the practice, in decimal form
0.84 ı	unitless	Rv = Runoff coefficient = 0.05 + (0.9 x l)
0.28 a	ac-in	WQV= 1" x Rv x A
1,007 (cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")

Water Quality Flow (WQF)

1	inches	P = Amount of rainfall. For WQF in NH, P = 1".
0.84	inches	Q = Water quality depth. $Q = WQV/A$
99	unitless	CN = Unit peak discharge curve number. CN =1000/(10+5P+10Q-10*[Q ² + 1.25*Q*P] ^{0.5})
0.1	inches	S = Potential maximum retention. S = (1000/CN) - 10
0.030	inches	Ia = Initial abstraction. Ia = 0.2S
6.0	minutes	T _c = Time of Concentration
	cfs/mi²/in	${\sf q}_{\sf u}$ is the unit peak discharge. Obtain this value from TR-55 exhibits 4-II and 4-III.
-	cfs	WQF = $q_u \times WQV$. Conversion: to convert "cfs/mi ² /in * ac-in" to "cfs" multiply by 1mi ² /640ac.



This worksheet may be useful when designing a BMP **that does not fit into one of the specific worksheets already provided** (i.e. for a technology which is not a stormwater wetland, infiltration practice, etc.)

Water Quality Volume (WQV)

0.37	ас	A = Area draining to the practice
0.27	ас	A _I = Impervious area draining to the practice
0.73	decimal	I = Percent impervious area draining to the practice, in decimal form
0.71	unitless	Rv = Runoff coefficient = 0.05 + (0.9 x l)
0.26	ac-in	WQV= 1" x Rv x A
949	cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")

Water Quality Flow (WQF)

1	inches	P = Amount of rainfall. For WQF in NH, P = 1".
0.71	inches	Q = Water quality depth. Q = WQV/A
97	unitless	CN = Unit peak discharge curve number. CN =1000/(10+5P+10Q-10*[Q ² + 1.25*Q*P] ^{0.5})
0.3	inches	S = Potential maximum retention. S = (1000/CN) - 10
0.062	inches	la = Initial abstraction. la = 0.2S
6.0	minutes	T _c = Time of Concentration
	cfs/mi ² /in	${\sf q}_{\sf u}$ is the unit peak discharge. Obtain this value from TR-55 exhibits 4-II and 4-III.
-	cfs	WQF = $q_u \times WQV$. Conversion: to convert "cfs/mi ² /in * ac-in" to "cfs" multiply by $1 \text{mi}^2/640 \text{ac}$.



This worksheet may be useful when designing a BMP **that does not fit into one of the specific worksheets already provided** (i.e. for a technology which is not a stormwater wetland, infiltration practice, etc.)

Water Quality Volume (WQV)

0.18	ас	A = Area draining to the practice
0.16	ac	A _i = Impervious area draining to the practice
0.89	decimal	I = Percent impervious area draining to the practice, in decimal form
0.85	unitless	Rv = Runoff coefficient = 0.05 + (0.9 x l)
0.15	ac-in	WQV= 1" x Rv x A
555	cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")

Water Quality Flow (WQF)

1	inches	P = Amount of rainfall. For WQF in NH. P = 1".
0.85	inches	Q = Water quality depth. Q = WQV/A
99	unitless	CN = Unit peak discharge curve number. CN =1000/(10+5P+10Q-10*[Q ² + 1.25*Q*P] ^{0.5})
0.1	inches	S = Potential maximum retention. S = (1000/CN) - 10
0.028	inches	la = Initial abstraction. la = 0.2S
6.0	minutes	T _c = Time of Concentration
	cfs/mi²/in	${\sf q}_{\sf u}$ is the unit peak discharge. Obtain this value from TR-55 exhibits 4-II and 4-III.
-	cfs	WQF = $q_u \times WQV$. Conversion: to convert "cfs/mi ² /in * ac-in" to "cfs" multiply by 1mi ² /640ac.

Pollutant R	cant Removal Efficiencies for Best for Use in Pollutant Loading ype BMP ype BMP wet Pond Wet Pond vater Wet Extended Detention Pond Micropool Extended Detention Pond Multiple Pond System Pocket Pond Pocket Pond Shallow Wetland eater Extended Detention Wetland Pond/Wetland System Gravel Wetland Infiltration Trench (≥75 ft from surface water) Infiltration Trench (<75 ft from surface water) ion Infiltration Basin (<75 ft from surface water) Infiltration Basin (<75 ft from surface water) Drip Edges Aboveground or Underground Sand Filter that infiltrates WQV (≥75 ft from surface water) Aboveground or Underground Sand Filter that infiltrates WQV (≥75 ft from surface water)		ent Practices	Values Accepted fo Loading Analyses			
ВМР Туре	ВМР	Notes	Lit. Ref.	TSS	TN	ТР	
	Wet Pond		B, F	70%	35%	45%	
Stormwater	Wet Extended Detention Pond		А, В	80%	55%	68%	
Ponds	Micropool Extended Detention Pond	TBA					
	Multiple Pond System	TBA					
	Pocket Pond	TBA					
	Shallow Wetland		A, B, F, I	80%	55%	45%	
Stormwater	Extended Detention Wetland		A, B, F, I	80%	55%	45%	
Wetlands	Pond/Wetland System	TBA					
	Gravel Wetland		Н	95%	85%	64%	
	Infiltration Trench (≥75 ft from surface water)		B, D, I	90%	55%	60%	
	Infiltration Trench (<75 ft from surface water)		B, D, I	90%	10%	60%	
Infiltration Practices	Infiltration Basin (≥75 ft from surface water)		A, F, B, D, I	90%	60%	65%	
	Infiltration Basin (<75 ft from surface water)		A, F, B, D, I	90%	10%	65%	
	Dry Wells			90%	55%	60%	
	Drip Edges			90%	55%	60%	
	Aboveground or Underground Sand Filter that infiltrates WQV (≥75 ft from surface water)		A, F, B, D, I	90%	60%	65%	
	Aboveground or Underground Sand Filter that infiltrates WQV (<75 ft from surface water)		A, F, B, D, I	90%	10%	65%	
	Aboveground or Underground Sand Filter with underdrain		A, I, F, G, H	85%	10%	45%	
Filtering	Tree Box Filter	TBA					
Practices	Bioretention System		I, G, H	90%	65%	65%	
	Permeable Pavement that infiltrates WQV (≥75 ft from surface water)		A, F, B, D, I	90%	60%	65%	
	Permeable Pavement that infiltrates WQV (<75 ft from surface water)		A, F, B, D, I	90%	10%	65%	
	Permeable Pavement with underdrain		Use TN and TP values for sand filter w/ underdrain and outlet pipe	90%	10%	45%	

Pollutant R	emoval Efficiencies for Best M for Use in Pollutant Loading	lanageme Analysis	ent Practices	Values Load	Accept ing Ana	ted for lyses
BMP Type	ВМР	Notes	Lit. Ref.	TSS	TN	ТР
Treatment Swales	Flow Through Treatment Swale	TBA				
Vegetated Buffers	Vegetated Buffers		A, B, I	73%	40%	45%
	Sediment Forebay	TBA				
	Vegetated Filter Strip		A, B, I	73%	40%	45%
	Vegetated Swale		A, B, C, F, H, I	65%	20%	25%
Pre-	Flow-Through Device - Hydrodynamic Separator		A, B, G, H	35%	10%	5%
Treatment Practices	Flow-Through Device - ADS Underground Multichamber Water Quality Unit (WQU)		G, H	72%	10%	9%
	Other Flow-Through Devices	TBA				
	Off-line Deep Sump Catch Basin		J, K, L, M	15%	5%	5%

RIP RAP CALCULATIONS Wadleigh Road Rochester NH

Jones & Beach Engineers, Inc.

P.O. Box 219 Stratham, NH 03885 10-Feb-22

Rip Rap equations were obtained from the *Stormwater Management and Erosion Control Handbook for Urban and Developing Areas in New Hampshire.* Aprons are sized for the 10-Year storm event.

TAILWATER < HALF THE D_0

$$\begin{split} & L_a = (1.8 \text{ x } \text{Q}) / \text{D}_0^{-3/2} + (7 \text{ x } \text{D}_o) \\ & W = L_a + (3 \text{ x } \text{D}_o) \text{ or defined channel width} \\ & d_{50} = (0.02 \text{ x } \text{Q}^{4/3}) / (\text{T}_w \text{ x } \text{D}_0) \end{split}$$

Culvert or	Tailwater	Discharge	Diameter	Length of	Width of	
Catch Basin	(Feet)	(C.F.S.)	of Pipe	Rip Rap	Rip Rap	
(Sta. No.)	T_w	Q	Do	L _a (feet)	W (feet)	d ₅₀ -Median Stone
						Rip Rap
15" ADS (CB2)	0.47	1.36	1.25	10.5	14	d50 (feet)
12" ADS (Stormtech #1)	0.14	0.33	1	7.6	11	
15" ADS (Swale)	0.19	0.59	1.25	9.5	13	0.05
8" ADS (Under Walkway)	0.11	0.11	0.67	5.1	7	0.03
18" ADS (18" Culvert)	0.32	1.8	1.5	12.3	17	0.04
Box Culvert	0.4	10.52	2	20.7	10	0.01
						0.09
						0.58

TAILWATER > HALF THE D_0

$$\begin{split} &L_a = (3.0 \ x \ Q) \ / \ D_0^{\ 3/2} + (7 \ x \ D_o) \\ &W = (0.4 \ x \ L_a) + (3 \ x \ D_o) \ or \ defined \ channel \ width \\ &d_{50} = (0.02 \ x \ Q^{4/3}) \ / \ (T_w \ x \ D_0) \end{split}$$

Culvert or	Tailwater	Discharge	Diameter	Length of	Width of	
Catch Basin	(Feet)	(C.F.S.)	of Pipe	Rip Rap	Rip Rap	
(Sta. No.)	T_w	Q	D _o	L _a (feet)	W (feet)	d ₅₀ -Median Stone Rip Rap
6" ADS (Pond #3)	0.5	0.21	0.5	4.6	10	d50 (feet)
4" ADS (Stormtech #2)	0.33	0.25	0.33	6.3	3	

0.01 0.03

Table 7-24 Recommended Rip Rap Gradation Ranges												
d_{50} Size =	0.25	Feet	3	Inches								
% of Weight Smaller		Size of Stone (Inches)										
Than the Given d ₅₀ Size		From		То								
100%		5		6								
85%		4		5								
50%		3		5								
15%		1		2								

Table 7-24 Recommended Rip Rap Gradation Ranges										
d ₅₀ Size =	0.5	Feet	6	Inches						
% of Weight Smaller		Siz	e of Stone (In	ches)						
Than the Given d ₅₀ Size	From To									
100%		9		12						
85%		8		11						
50%		6		9						
15%		2		3						



Extreme Precipitation Tables

Northeast Regional Climate Center

Data represents point estimates calculated from partial duration series. All precipitation amounts are displayed in inches.

Smoothing	Yes
State	New Hampshire
Location	
Longitude	70.980 degrees West
Latitude	43.285 degrees North
Elevation	0 feet
Date/Time	Mon, 18 Oct 2021 11:28:33 -0400

Extreme Precipitation Estimates

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.26	0.40	0.49	0.65	0.81	1.02	1yr	0.70	0.97	1.19	1.53	1.97	2.55	2.83	1yr	2.26	2.72	3.14	3.86	4.43	1yr
2yr	0.32	0.49	0.61	0.80	1.01	1.28	2yr	0.87	1.16	1.49	1.89	2.41	3.08	3.44	2yr	2.73	3.31	3.81	4.54	5.18	2yr
5yr	0.37	0.57	0.72	0.96	1.23	1.58	5yr	1.06	1.44	1.85	2.36	3.03	3.88	4.40	5yr	3.44	4.23	4.86	5.71	6.45	5yr
10yr	0.41	0.64	0.81	1.10	1.43	1.85	10yr	1.23	1.69	2.18	2.80	3.60	4.63	5.30	10yr	4.10	5.09	5.84	6.79	7.63	10yr
25yr	0.47	0.75	0.95	1.31	1.74	2.28	25yr	1.50	2.08	2.70	3.51	4.53	5.84	6.77	25yr	5.17	6.51	7.46	8.54	9.53	25yr
50yr	0.52	0.84	1.08	1.51	2.03	2.69	50yr	1.75	2.45	3.20	4.17	5.40	6.96	8.16	50yr	6.16	7.85	8.98	10.16	11.27	50yr
100yr	0.59	0.96	1.23	1.74	2.37	3.17	100yr	2.04	2.88	3.78	4.94	6.42	8.30	9.84	100yr	7.35	9.46	10.81	12.11	13.35	100yr
200yr	0.66	1.07	1.39	2.00	2.76	3.73	200yr	2.39	3.40	4.48	5.88	7.66	9.91	11.87	200yr	8.77	11.41	13.01	14.42	15.81	200yr
500yr	0.78	1.28	1.67	2.43	3.40	4.63	500yr	2.93	4.22	5.58	7.37	9.65	12.53	15.21	500yr	11.09	14.62	16.65	18.19	19.78	500yr

Lower Confidence Limits

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.24	0.36	0.44	0.60	0.73	0.90	1yr	0.63	0.88	0.92	1.25	1.47	2.01	2.44	1yr	1.78	2.35	2.91	3.32	3.96	1yr
2yr	0.31	0.48	0.59	0.80	0.99	1.17	2yr	0.85	1.15	1.35	1.80	2.32	2.99	3.34	2yr	2.64	3.21	3.69	4.41	5.03	2yr
5yr	0.35	0.54	0.67	0.91	1.16	1.40	5yr	1.00	1.36	1.60	2.12	2.75	3.59	4.04	5yr	3.18	3.88	4.52	5.32	6.02	5yr
10yr	0.38	0.59	0.73	1.02	1.32	1.59	10yr	1.14	1.56	1.81	2.40	3.09	4.10	4.66	10yr	3.63	4.48	5.22	6.12	6.86	10yr
25yr	0.44	0.67	0.83	1.19	1.57	1.90	25yr	1.35	1.86	2.11	2.81	3.58	4.88	5.62	25yr	4.32	5.40	6.34	7.32	8.08	25yr
50yr	0.49	0.74	0.92	1.33	1.79	2.19	50yr	1.54	2.14	2.37	3.16	3.98	5.56	6.46	50yr	4.92	6.22	7.35	8.40	9.30	50yr
100yr	0.55	0.83	1.03	1.49	2.05	2.51	100yr	1.77	2.45	2.68	3.55	4.41	6.33	7.43	100yr	5.60	7.14	8.53	9.64	10.58	100yr
200yr	0.61	0.92	1.16	1.68	2.34	2.88	200yr	2.02	2.82	3.01	3.99	4.89	7.19	8.54	200yr	6.36	8.21	9.89	11.06	12.05	200yr
500yr	0.71	1.06	1.37	1.98	2.82	3.49	500yr	2.43	3.41	3.54	4.65	5.62	8.47	10.27	500yr	7.50	9.87	12.02	13.27	14.26	500yr

Upper Confidence Limits

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.28	0.43	0.53	0.71	0.87	1.07	1yr	0.75	1.05	1.23	1.70	2.15	2.78	3.05	1yr	2.46	2.93	3.38	4.16	4.76	1yr
2yr	0.33	0.50	0.62	0.84	1.04	1.24	2yr	0.89	1.21	1.45	1.93	2.51	3.20	3.57	2yr	2.83	3.44	3.95	4.69	5.34	2yr
5yr	0.39	0.60	0.75	1.02	1.30	1.57	5yr	1.13	1.53	1.83	2.46	3.16	4.18	4.75	5yr	3.70	4.57	5.21	6.10	6.86	5yr
10yr	0.46	0.70	0.87	1.21	1.57	1.89	10yr	1.35	1.85	2.21	3.00	3.81	5.15	5.91	10yr	4.56	5.68	6.51	7.44	8.32	10yr
25yr	0.56	0.85	1.06	1.51	1.98	2.43	25yr	1.71	2.38	2.84	3.90	4.91	6.81	7.90	25yr	6.03	7.60	8.67	9.86	10.78	25yr
50yr	0.65	0.98	1.23	1.76	2.37	2.93	50yr	2.05	2.86	3.44	4.74	5.96	8.41	9.86	50yr	7.44	9.48	10.78	12.10	13.24	50yr
100yr	0.76	1.14	1.43	2.07	2.84	3.52	100yr	2.45	3.44	4.17	5.79	7.25	10.39	12.30	100yr	9.20	11.83	13.41	14.88	16.15	100yr
200yr	0.88	1.33	1.68	2.44	3.40	4.25	200yr	2.93	4.16	5.07	7.06	8.81	12.88	15.38	200yr	11.40	14.79	16.68	18.28	19.74	200yr
500yr	1.09	1.61	2.08	3.02	4.29	5.44	500yr	3.70	5.31	6.53	9.21	11.43	17.14	20.66	500yr	15.17	19.87	22.28	24.05	25.74	500yr





USDA Natural Resources Conservation Service Web Soil Survey National Cooperative Soil Survey


Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
BzB	Buxton silt loam, 3 to 8 percent slopes	21.2	3.7%
CsC	Charlton fine sandy loam, 8 to 15 percent slopes, very stony	0.5	0.1%
DeA	Deerfield loamy fine sand, 0 to 3 percent slopes	11.8	2.1%
Gv	Gravel and borrow pits	13.0	2.3%
HaA	Hinckley loamy sand, 0 to 3 percent slopes	9.0	1.6%
НсВ	Hollis-Charlton fine sandy loams, 3 to 8 percent slopes	20.3	3.5%
HdC	Hollis-Charlton very rocky fine sandy loams, 8 to 15 percent slopes	164.7	28.7%
MI	Mixed alluvial land, wet	13.6	2.4%
PbB	Paxton fine sandy loam, 3 to 8 percent slopes	2.1	0.4%
PdB	Paxton fine sandy loam, 0 to 8 percent slopes, very stony	11.5	2.0%
PdC	Paxton fine sandy loam, 8 to 15 percent slopes, very stony	9.2	1.6%
Ru	Rumney fine sandy loam	31.4	5.5%
Sb	Saugatuck loamy sand	3.1	0.5%
SwA	Swanton fine sandy loam, 0 to 3 percent slopes	5.3	0.9%
W	Water	8.5	1.5%
WdA	Windsor loamy sand, 0 to 3 percent slopes	219.2	38.3%
WdE	Windsor loamy sand, 15 to 60 percent slopes	19.0	3.3%
WfB	Windsor loamy fine sand, clay subsoil variant, 0 to 8 percent slopes	6.2	1.1%
WfC	Windsor loamy fine sand, clay subsoil variant, 8 to 15 percent slopes	3.4	0.6%
Totals for Area of Interest		573.0	100.0%

SITE-SPECIFIC SOIL SURVEY REPORT For 29 Wadleigh Road, Rochester, NH By Gove Environmental Services, Inc.

1. MAPPING STANDARDS

Site-Specific Soil Mapping Standards for New Hampshire and Vermont. SSSNNE Special Publication No. 3, Version 7.0, July 2021. This map product is within the technical standards of the National Cooperative Soil Survey. It is a special product, intended for the submission to NH DES Alteration of Terrain. It was produced by a professional soil scientist and is not a product of the USDA Natural Resource Conservation Service.

Hydrologic Soil Group was determined using SSSNNE Special Publication No. 5, Ksat Values for New Hampshire Soils, September 2009.

OVERVIEW:

The site is primarily bedrock-controlled glacial till. The central portion of the site is dominated by exposed bedrock and very shallow soils, found on the large hill. Away from the central portion on the flatter slopes, the bedrock is deeper than 40 inches and the soils are moderately well drained with a mineral restrictive layer. Smaller hills rising above the flatter slope are also shallow-to-bedrock soils. Several streams pass through the wetland areas and dump into Axe Handle Brook.

Scale of soil map:

Approximately 1" equals 30'

Contours:

Intervals of 2 feet

2. DATE SOIL MAP PRODUCED

Date(s) of on-site field work: 11-2-2021

Date(s) of test pits: 10-1-2021

Test pits recorded by:

Jones & Beach Engineers

3. GEOGRAPHIC LOCATION AND SIZE OF SITE

City or town where soil mapping was conducted: Rochester

Location: 29 Wadleigh Road, Tax mapb137, lot 3501.

Size of area: approximately 8 acres

Was the map for the entire lot? Yes

If no, where was the mapping conducted on the parcel: n/a

4. PURPOSE OF THE SOIL MAP

Was the map prepared to meet the requirement of Alteration of Terrain? Yes

If no, what was the purpose of the map? n/a

Who was the map prepared for? Jones & Beach Engineers

5. SOIL IDENTIFICATION LEGEND

SSSS SYM.	SSSS MAP NAME	HISS SYM.	HYDROLOGIC SOIL GRP.
32	Boxford silt loam	343	С
141	Hollis-Rock Outcrop-Chatfield compl	ex 228	D
449	Scituate very stony	323	С
547	Walpole very stony	523	С

SLOPE PH	IASE:				
0-8%	В	8-15%	С	15-25%	D
25%+	E				

6. SOIL MAP UNIT DESCRIPTIONS - SOIL DESCRIPTIONS - PHOTOS

SSSS SYM.	SSSS MAP NAME	HISS SYM.	HYDROLOGIC SOIL GRP.
32	Boxford silt loam	343	С

This marine silt and clay map unit makes up a small area of the overall site. It is located on the southeastern end of the site. The soil has a silt loam topsoil and subsoil, with a silty clay loam substratum. The estimated seasonal high water table ranges from 15 to 20 inches deep. Due to the silty textures and the high water table, the hydrologic group is a C.

141 Hollis-Rock Outcrop-Chatfield complex 228 D

The bedrock-controlled glacial till is found on the dominant hill of the site where the cell tower is located and also on other low hills that are on the site and near Axe Handle Brook. This is a complex, because the bedrock is variable from exposed ledge to 3 feet to refusal. Due to the majority of this complex being either exposed bedrock or Hollis soils, the hydrologic soil group is D. This soil makes up a large component of the site. Inclusions would be pockets of soils between the outcrops that are deeper than 40 inches.



449	Scituate very stony	323	С

This dense substratum glacial till soil is the other large component of the upland areas. It lies between the 141 hills on the flatter slopes. The topsoil and subsoil are fine sandy loams, with a dense substratum of loamy sand. Estimated seasonal high water tables range from 20 to 28", and are typically at or slightly above the dense restrictive layer. Because of the seasonal high water table and the mineral restrictive layer, the hydrologic group is C.

547	Walpole very stony	523	С

This soil is the dominant wetland hydric soil type on site. The soil is typically fine sandy loam topsoil and subsoil, with a loamy sand substratum. Estimated water tables are at the surface to a depth of 12 inches. Inclusions would be areas of dense substratum and, in the wetland on the south side of the site, inclusions of Scitico silt loam adjacent the Boxford map unit would be found. The hydrologic group is C. Each of the wetland map units have stream channels that flow northeast to Axe Handle Brook.

7. RESPONSIBLE SOIL SCIENTIST

Name: James P. Gove

Certified Soil Scientist Number: 004

8. OTHER DISTINGUISHING FEATURES OF SITE

Is the site in a natural condition? For the most part.

If no, what is the nature of the disturbance? The placement of the cell tower and access road to the tower.

Stamp of CSS





85 Portsmouth Avenue, PO Box 219, Stratham, NH 03885 603.772.4746 - JonesandBeach.com

STORMWATER MANAGEMENT OPERATION AND MAINTENANCE MANUAL

Wadleigh Road Apartments Tax Map 137 Lot 35-1 Route 125 Rochester, NH 03839

Prepared for:

Groen Construction 120 Washington Street Suite 302 Rochester, NH 03839

> <u>Prepared by:</u> Jones & Beach Engineers, Inc. 85 Portsmouth Avenue P.O. Box 219 Stratham, NH 03885 (603) 772-4746 February 10, 2022 JBE Project No. 21137

Inspection and Maintenance of Facilities and Property

A. Maintenance of Common Facilities or Property

1. The Apartment Complex, future owners and assigns are responsible to perform the maintenance obligations or hire a Professional Engineer to review the site on an annual basis for maintenance and certification of the stormwater system. The Owner shall keep receipts and records of all maintenance companies hired throughout the year to submit along with the following form. The annual report and certification shall be submitted to City of Rochester DPW upon request.

B. General Inspection and Maintenance Requirements

- 1. Permanent stormwater and sediment and erosion control facilities to be maintained on the site include, but are not limited to, the following:
 - a. Catch basins and drain manholes
 - b. Culverts
 - c. Swales
 - d. Vegetation and landscaping
 - e. Parking lots and roadways
 - f. Riprap inlet and outlet protection aprons
 - g. Bio-retention systems
 - h. Focal Point Bioretention
 - i. Stormtech Underground Detention System
 - j. Roof drains
 - k. Rock Slope Ptetection
 - 1. Invasive Species Control
- 2. Maintenance of permanent measures shall follow the following schedule:
 - a. Normal winter roadway and parking lot maintenance including plowing and snow removal.
 - b. Road and parking lot sweeping at the end of every winter, preferably at the start of the spring rain season.



- c. **Inspection** of culvert inlets and outlets at least **once per month** during the rainy season (March to November). Any debris is to be removed and disposed of properly by owner or owner's agent.
- d. **Annual inspection** of the site for erosion, destabilization, settling, and sloughing. Any needed repairs are to be conducted immediately.
- e. **Annual inspection** of site's vegetation and landscaping. Any areas that are bare shall be reseeded and mulched with hay or, if the case is extreme, loamed and seeded or sodded to ensure adequate vegetative cover. Landscape specimens shall be replaced in kind, if they are found to be dead or dying.
- f. Annual inspection of catch basins and drain manholes to determine if they need to be cleaned. Catch basins are to be cleaned if the depth of deposits is greater than one-half the depth from the basin bottom to the invert of the lowest pipe or opening into or out of the basin. If a catch basin significantly exceeds the one-half depth standard during the inspection, then it should be cleaned more frequently. If woody debris or trash accumulates in a catch basin, then it should be cleaned on a weekly basis. Manholes should be cleaned of any material upon inspection. Catch basins and manholes can be cleaned either manually or by specially designed equipment including, but not limited to, bucket loaders and vacuum pumps. Before any materials can be disposed, it is necessary to perform a detailed chemical analysis to determine if the materials should be stored, treated, and disposed. Grease hoods are to be wiped clean and the rags disposed of properly. Debris obscuring the grate inlet should also be removed.
- g. Permanent stone slope protection should be **inspected annually** in order to ensure that they are in good condition. Any loose rocks or any signs of erosion under the slope should be repaired or replaced immediately. Woody vegetation should not be allowed to become established in riprap areas, and/or any debris removed from the void spaces between the rocks. If the riprap is adjacent to a stream or other waterbody, the water should be kept clear of obstructions, debris, and sediment deposits
- h. Rock riprap inlets and outlets should be **inspected annually** in order to ensure that it has not been displaced, undermined, or otherwise damaged. Displaced rock should be replaced, or additional rock added in order to maintain the structure(s) in their undamaged state. Woody vegetation should not be allowed to become established in riprap areas, and/or any debris removed from the void spaces between the rocks. If the riprap is adjacent to a stream or other waterbody, the water should be kept clear of obstructions, debris, and sediment deposits.
- i. Raingarden Bioretention Cells:
 - Visually inspect monthly and repair erosion. Use small stones to stabilize erosion along drainage paths.



- Check the pH once a year if plantings are not surviving. Apply an alkaline product, such as limestone, if needed.
- Re-mulch any void areas by hand as needed.
- Every 6 months, in the spring and fall, add a fresh mulch layer.
- Once every 2 to 3 years, in the spring, remove old mulch layer before applying new one.
- Immediately after the completion of cell construction, water plant material for 14 consecutive days unless there is sufficient natural rainfall.
- When trees have taken root, or at least by 6 months, remove stakes and wires.
- Once a month (more frequently in the summer), residents are encouraged to visually inspect vegetation for disease or pest problems and treat as required.
- Twice a year, from March 15th to April 30th and October 1st to November 30th, remove and replace all dead and diseased vegetation considered beyond treatment.
- During times of extended drought, look for physical features of stress (unrevived wilting, yellow, spotted or brown leaves, loss of leaves, etc.). Water in the early morning as needed.
- Weed regularly, if needed.
- Prune excess growth annually or more often, if desired. Trimmed materials may be recycled back in with replenished mulch or land filled if there is a concern of heavy metals accumulation.
- After rainstorms, inspect the cell and make sure that drainage paths are clear and that ponding water dissipates over 4-6 hours. (Water may pond for longer times during the winter and early spring.)
- KEEP IN MIND, THE BIORETENTION CELL IS NOT A POND. IT SHOULD NOT PROVIDE A BREEDING GROUND FOR MOSQUITOES. MOSQUITOES NEED AT LEAST FOUR (4) DAYS OF STANDING WATER TO DEVELOP AS LARVA.
- j. FocalPoint Biofiltration Systems
 - A. Maintenance Requirements
 - 1. Annual maintenance generally consists of two (2) scheduled visits unless otherwise specified.
 - 2. Each maintenance visit consists of the following:
 - 1. Complete system inspection
 - 2. Removal of foreign debris, silt, plant material, trash and mulch (if needed)
 - 3. Evaluation of biofiltration media
 - 4. Evaluation of plant health



- 5. Inspection of underdrain/storage system via Observation/Maintenance Port
- 6. Properly dispose of all maintenance refuse items (trash, mulch, etc.)
- 7. Take photographs documenting plant growth and general system health
- 8. Update and store maintenance records
- 9. To ensure long term performance of the HPMBS, continuing annual maintenance should be performed per the manufacturer's Operations and Maintenance Manual.
- 3. If sediment accumulates beyond an acceptable level in the underdrain/storage system, it will be necessary to flush the underdrain. This can be done by pumping water into the Observation/Maintenance Port or adjacent overflow structure, allowing the turbulent flows through the underdrain to re-suspend the fine sediments. If multiple Observation/Maintenance Ports have been installed, water should be pumped into each port to maximize flushing efficiency.

Sediment-laden water can be pumped out and either captured for disposal or filtered through a Dirtbag filter bag, if permitted by the locality.

k. Vegetated Buffers:

Inspect buffer at least annually for signs of erosion, sediment buildup, or vegetation loss. If a meadow buffer, provide periodic mowing as needed to maintain a healthy stand of herbaceous vegetation. If a forested buffer, then the buffer should be maintained in an undisturbed condition, unless erosion occurs. If erosion of the buffer (forested or meadow) occurs, eroded areas should be repaired and replanted with vegetation similar to the remaining buffer. Corrective action should include eliminating the source of the erosion problem, and may require retrofit with a level spreader. Remove debris and accumulated sediment, based on inspection.

1. Roof Drip Edges:

The following recommendations will help assure that the roof drip edges are maintained to preserve its effectiveness.

In the spring and fall, visually inspect the area around the edges and repair any erosion. Use small stones to stabilize erosion along drainage paths. Inspect stone area to ensure that it has not been displaced, undermined, or otherwise damaged. Displaced rock should be replaced, or additional rock added in order to maintain the structure(s) in their undamaged state. Woody vegetation should not be allowed to become established in



stone areas, and/or any debris removed from the void spaces between the stones. Also inspect the roof collection and piping (if any) and clean and repair as necessary.

m. Roof Drains:

Roof drains should be **inspected annually**, preferably in the fall after leaf drop. Drains should be kept clear, and any debris that may clog a drain such as tennis balls, baseballs, beverage cans, etc. should be removed during each inspection. Every drain should have a clean "leaf" grate present to prevent clogging of the drainpipes. A roof inspection in the late fall should also include the removal of leaves. Outfalls should be inspected to assure a clear drainage path.

WHAT TO LOOK FOR:

Although improper roof drainage can best be observed immediately after a rain storm, most impacted drainage conditions will leave "tell-tale" indications even after standing water has evaporated:

- 1. Accumulated Debris. Debris frequently accumulates in ponding areas. Because water eventually evaporates from impacted areas, a concentric pattern of debris or dirt is a good indication of a ponding condition.
- 2. Visible Sagging or Deflection.
- 3. Discoloration of Curbs and Walls. The discoloration may be due to a build-up of snow or ice, or it may be an indication that water may "back up" during very severe rain storms.
- n. Invasive Species Control

An invasive plant is a non-native plant that is able to persist and proliferate outside of cultivation, resulting in ecological and/or economic harm. These plants readily colonize disturbed areas and habitat edges, such as transportation and river corridors. Once established in these areas, invasive plants often continue to spread to adjacent habitats. All invasive plant species are aggressive competitors with the ability to significantly reduce diversity of native plant and animal species.

For additional information refer to the "New Hampshire Department of Transportation: *Best Management Practices for Roadside Invasive Plants*"

1. Invasive Plant Prevention:

Invasive plants spread by a variety of mechanisms, including birds, wind, and water. Human activities are also a major factor in the spread of these plants, from gardening and transport of nursery stock to erosion control and wildlife plantings. Routine maintenance and construction activities along transportation corridors can



also play a significant role in the spread of invasive plants by dispersing or introducing seeds and other viable plant materials.

Eliminating or reducing the spread and establishment of invasive plants requires a proactive approach, in which there are two key elements. First, new introductions, especially those that occur due to human activities, must be avoided to the maximum extent possible. Second, there must be an emphasis on early detection and eradication of new populations. Control measures are far more likely to be successful, as well as significantly less expensive, on small, young populations rather than on larger, more established populations, as shown in Figure 1.



Figure 1. Typical invasive species population curve (from the University of Arizona and USGS Desert Laboratory http://wwwpaztcn.wr.usgs.gov)

2. Best Management Practices

Soil Disturbance and Stabilization:

• BMP #1: Minimize soil disturbance whenever possible. Invasive plants readily colonize areas of disturbed soil. Monitor recent work sites for the emergence of invasive plants for a minimum of two years after project completion.



- BMP #2: Stabilize disturbed soils as soon as possible by seeding and/or using mulch, hay, rip-rap, or gravel that is free of invasive plant material. Seeds of native species should be used whenever possible. Species on the prohibited invasive plant list should never be planted.
- BMP #3: Materials such as fill, loam, mulch, hay, rip-rap, and gravel should not be brought into project areas from sites where invasive plants are known to occur. If the absence of invasive plant parts in these materials cannot be guaranteed, recent work sites should be monitored for the emergence of invasive plants for a minimum of two years after project completion.

Movement and Maintenance of Equipment:

- BMP #4: If work in areas containing invasive plants cannot be avoided, then the movement of maintenance and construction equipment should be from areas not infested by invasive plants to areas infested by invasive plants whenever possible. This is especially important during ditch cleaning and shoulder scraping activities.
- BMP #5: Locate and use staging areas that are free of invasive plants to avoid spreading seeds and other viable plant parts.
- BMP #6: If equipment must be used in areas where invasive plants occur, all equipment, machinery, and hand tools should be cleaned of all visible soil and plant material before leaving the project site. Equipment should be cleaned at the site of infestation. Acceptable methods of cleaning include, but are not limited to: *f* Portable wash station that contains runoff from washing equipment (containment must be in compliance with wastewater discharge regulations); *f* High pressure air; Brush, broom, or other hand tools (used without water).
- BMP #7: If equipment must be used in areas containing Japanese knotweed, phragmites, or purple loosestrife, aboveground plant material should be cut and properly disposed of (see BMP #11) prior to the start of work. If excavation occurs in these areas, see BMPs #13-16.

Mowing:

• BMP #8: These invasive plants have the ability to sprout from stem and root fragments: purple loosestrife, phragmites, and Japanese knotweed. Mowing these plants should be avoided whenever possible. Staking roadside populations of these plants as "do not mow" is one way to accomplish this. If these plants are cut, all plant material must be rendered nonviable and extra care should be taken to avoid spreading plant fragments (see BMP #11).



- BMP #9: In areas where invasive plants occur and the plants listed in BMP #8 (purple loosestrife, phragmites, and Japanese knotweed) are not present, an attempt should be made to mow the right-of-way prior to seed maturation (approximately August 1st). This could be accomplished by identifying specific roads that are either heavily infested with invasive plants or roads that are in sensitive habitat areas, and making those roads a priority in the mowing schedule.
- BMP #10: Mowing equipment should be cleaned at least daily, as well as prior to transport (see BMP #6). This is particularly important if mowing occurs after seed maturation (after August 1st).

Disposal of Plants:

- BMP #11: When invasive plants are cut or removed for roadside maintenance, construction, or control of plants, the spread of viable plant material must be avoided by rendering plant material nonviable. The following methods can be used to destroy plant material:
 - Drying/Liquefying: For large amounts of plant material or for plants with rigid stems, place the material on asphalt, tarps, or heavy plastic, and cover with tarps or heavy plastic to prevent the material from blowing away. For smaller amounts of plant material or for plants with pliable stems, bag the material in heavyduty (3-mil or thicker) garbage bags. Keep plant material covered or bagged for at least one month. Material is nonviable when it is partially decomposed, very slimy, or brittle. Once material is nonviable, it can be disposed of in a landfill or brush pile. Recommended for: Japanese knotweed, purple loosestrife, phragmites.
 - Brush Piles: Plant material from most invasive plants can be piled on site to dry out. However, when piling purple loosestrife, phragmites, and Japanese knotweed, care must be taken to pile stems so that cut surfaces are not in contact with the soil. Recommended for: Woody shrubs, trees, and vines; spotted knapweed; large quantities of purple loosestrife, phragmites, and Japanese knotweed. NOT recommended for: any invasive plant with seeds or fruit attached, unless plants can be piled within the limits of the infestation.
 - Burying: Plant material from most invasive plants can be buried a minimum of three feet below grade. This method is best used on a job site that already has disturbed soils. Recommended for: any invasive plant. NOT recommended for: Japanese knotweed, unless other options are not feasible and knotweed can be buried at the site of infestation at least five feet below grade. *f*
 - Burning: Plant material should be taken to a designated burn pile. (All necessary permits must be obtained before burning.) Recommended for: any invasive plant, especially purple loosestrife, phragmites, Japanese knotweed.



- Herbicide: Herbicide applications must be carried out by a licensed applicator with a permit from the NH Department of Agriculture Division of Pesticide Control. Recommended for: any invasive plant, especially purple loosestrife, phragmites, Japanese knotweed.
- BMP #12: Invasive plant material must be covered during transport.

Excavated Material:

- BMP #13: Excavated material taken from sites that contain invasive plants cannot be used away from the site of infestation until all viable plant material is destroyed. Excavated material from areas containing invasive plants may be reused within the exact limits of the infestation.
- BMP #14: Any excavated material that contains viable plant material and is not reused within the limits of the infestation must be stockpiled on an impervious surface until viable plant material is destroyed OR the material must be disposed of by burying a minimum of three feet below grade. Japanese knotweed must be buried at least five feet below grade.
- BMP #15: Whenever possible, excavation should be avoided in areas containing Japanese knotweed, purple loosestrife, and phragmites. If excavation does occur in these areas, the BMPs described in Section II must be followed.
- BMP #16: Soil and other materials containing invasive plants must be covered during transport.

See attached sample forms as a guideline.

Any inquiries in regards to the design, function, and/or maintenance of any one of the above mentioned facilities or tasks shall be directed to the project engineer:

Jones & Beach Engineers, Inc. 85 Portsmouth Avenue P.O. Box 219 Stratham, NH 03885

T#: (603) 772-4746 F#: (603) 772-0227

Commitment to maintenance requirements



I agree to complete and/or observe all of the required maintenance practices and their respective schedules as outlined above.

Signature

Print Name

Title

Date



Annual Operations and Maintenance Report

The Wadleigh Road Apartments, future owners and assigns are responsible to perform the maintenance obligations or hire a Professional Engineer to review the site on an annual basis for maintenance and certification of the stormwater system. The Owner or Authorized Agent shall keep receipts and records of all maintenance companies hired throughout the year to submit along with the following form. The annual report and certification shall be submitted to the City of Rochester DPW upon request.

Construction Activity	Date of Inspection	Who Inspected	Findings of Inspector
Catch basins and drain manholes			
Culverts			
Swales			
Vegetation and landscaping			
Parking lots and roadways			



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Bio-retention system		
Essal Dainta		
Focal Points		
Stormtech		
Ladonomound		
Onderground		
Detention System		
-		
Inlet Protection		
milet i fotection		
Slava Dratastian		
Slope Protection		
Outlet Protection		







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Designed and Produced in NH UBMISSION MJK ARD LAZ S5 Portsmouth Ave. Ciauil Engineering Services	S, Inc. Plan Name: 603-772-4746 Project:
UBMISSION MJK ARD LAZ LAZ 85 Portsmouth Ave. Civil Engineering Services PO Box 219 FA Stratham, NH 03885 E-MAIL: JBE@JONESAN	Bit Construction Project: 603-772-4746 Owner of Record: IDBEACH.COM Owner of Record:





RESIDENTIAL DEVELOPMENT "WADLEIGH ROAD APARTMENTS" TAX MAP 137, LOT 35-1 WADLEIGH ROAD, ROCHESTER, NH



LOCUS MAP SCALE 1" = 1000"

CIVIL ENGINEER / SURVEYOR

JONES & BEACH ENGINEERS, INC.

EMAIL: BJONES@JONESANDBEACH.COM

STEPHEN G. PERNAW & COMPANY, INC.

GOVE ENVIRONMENTAL SERVICES, INC.

8 CONTINENTAL DR., BUILDING 2, UNIT H

LAZ

BY

CONTACT: STEPHEN G. PERNAW

EMAIL: SGP@PERNAW.COM

WETLAND CONSULTANT

EXETER, NH 03833-7526

85 PORTSMOUTH AVENUE

STRATHAM, NH 03885

CONTACT: BRAD JONES

TRAFFIC ENGINEER

CONCORD, NH 03302

PO BOX 219

(603) 772-4746

P.O. BOX 1821

(603) 731-8500

(603) 778-0644 CONTACT: JAMES GOVE EMAIL: JGOVE@GESINC.BIZ

LANDSCAPE DESIGNER LM LAND DESIGN, LLC 11 SOUTH ROAD BRENTWOOD, NH 03833 (603) 770-7728 CONTACT: LISE McNAUGHTON LMLANDDESIGN@GMAIL.COM

> WATER AND SEWER ROCHESTER DEPARTMENT OF PUBLIC WORKS 45 OLD DOVER ROAD ROCHESTER, NH 03867 (603) 332-4096 CONTACT: MICHAEL BEZANSON, P.E.

ELECTRIC EVERSOURCE ENERGY 74 OLD DOVER ROAD ROCHESTER, NH 03867 (603) 332-7507 CONTACT: PIERRE BOUGIE

TELEPHONE

CONSOLIDATED COMMUNICATIONS 1575 GREENLAND ROAD GREENLAND, NH 03840 (603) 427-5525 CONTACT: JOE CONSIDINE

CABLE TV COMCAST COMMUNICATION CORPOR 334-B CALEF HIGHWAY EPPING, NH 03042-2325 (603) 679-5695

NATURAL GAS

UNITIL SERVICE CORP. 325 WEST ROAD PORTSMOUTH, NH 03801 (603) 294-5261 MACLEAND@UNITIL.COM

 Design: LAZ
 Draft:
 LAZ
 Date:
 9/8/21

 Checked:
 BAJ
 Scale:
 AS NOTED
 Project No.: 2113

 Drawing Name:
 21137-PLAN.dwg
 THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN

ISSION FROM JONES & BEACH ENGINEERS, INC. (JBE). ANY ALTERATIONS. AUTHORIZED OR OTHERWISE, SHALL BE AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.



2/10/22 5 REVISED PER CITY COMMENTS 4 1/14/22 REVISED PER CITY COMMENTS 3 12/14/21 REVISED PER CITY COMMENTS 2 12/6/21 REVISED PER CONSERVATION COMMISSION COMMENTS 1 9/21/21 ISSUED FOR PLANNING BOARD BEV. DATE REVISION



Plan Name

Owner of Record: 120

SHEET INDEX

CS	COVER SHEET
OVR EX	OVERVIEW EXISTING CONDITIONS PLAN
C1-C2	EXISTING CONDITIONS PLAN
OVR S	OVERVIEW SITE PLAN
C3-C4	SITE PLAN
C5-C6	GRADING AND DRAINAGE PLAN
C7	EROSION CONTROL PLAN
P1-P2	ROAD PLAN AND PROFILE
P3-P4	SEWER PROFILE
U1-U2	UTILITY PLAN
L1	LANDSCAPE PLAN
L2-L3	LIGHTING PLAN
D1-D5	DETAIL SHEETS
D6	SELECT CROSS SECTIONS
E1	EROSION AND SEDIMENT CONTROL DETAILS
T1	TRUCK TURNING PLAN

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COVER SHEET			DRAWING No.	AND AND AND AND AND AND AND AND AND AND
WADLEIGH ROAD APARTMEN ROCHESTER, NH	ITS		CS	CT NAME 21137
SSG, LLC ATTN: FENTON GROEN WASHINGTON STREET, ROCHESTER, N	H 03839	JI	SHEET 1 OF 27 SE PROJECT NO. 21137	PROJE











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S	ITE NOTES:	LOCU	S SCALE: 1	"=1000'			
1.	THE INTENT OF TH TAX MAP 137, LOT SERVED BY ELECT	THE INTENT OF THIS PLAN IS TO SHOW A LAYOUT FOR A FIFTY-TWO (52) UNIT APARTMENT COMPLEX ON TAX MAP 137, LOT 35-1, ACCESS FOR THE SITE WILL BE FROM WADLEIGH ROAD. PROJECT TO BE					
2	ZONING DISTRICT: HIGHWAY COMMERCIAL LOT AREA MINIMUM = 20,000 SF LOT AREA MINIMUM = 20,000 SF LOT AREA PER DWELLING UNIT = 7,500 SF BUILDING SETBACK = 20' SIDE SETBACK = 10' REAR SETBACK = 10' PAVETLAND SETBACK = 50 PAVETLAND SETBACK = 50' REAR SETBACK = 10' MAX.LOT COVERATIONS PARING CALCULATIONS:						
ß	2 SPACES PER UN SPACES PROVIDED	TOTAL NUMBER OF UNITS = 52. 2 SPACES PER UNIT = 104 SPACES REQUIRED SPACES PORVED = 104 SPACES (NOTITING 5 HANDLAR ADDRESS)					
4. 54310'22"W 335.84'	THIS PLAN SET HAS BEED ON DATA OF TANED (INCLUDING D HANDLOP ACCESSIBLE SPACES) THIS PLAN SET HAS BEED ON DATA OFTAINED FROM ON-STE FEED SURVEY AND DXSTING MUNICIPAL APPROVALS BASED ON DATA OFTAINED FROM ON-STE FEED SURVEY AND DXSTING MUNICIPAL RECORDS AND LIDAR CONTOUR INFORMATION. THROUGHOUT THE CONSTRUCTION PROCESS, THE CONTRACTOR SHALL INFORM THE ENGINEER IMMEDIATELY OF ANY FIELD DISCREPANCY FROM DATA AS SHOWN ON THE DESIGN PLANS, INCLUDING ANY UNFORESEN CONTROLTIONS, SUBSTREACE OR OTHERWISE FOR EVALUATION AND RECOMMENDATIONS. ANY CONTRADICTION ETWEEN ITEMS ON THIS PLAN/PLAN SET, OR EDWEENT THE PLANS AND ON-STE CONDITIONS, MUST BE RESOLVED BEFORE REALTED CONSTRUCTION HAS BEEN INITIATED. CONTRACTOR TO ALWAYS CONTACT DIG SAFE PRIOR TO DIGGING UNSTE OR OFFSTE TO ENSURE SAFETY AND OBEY THE LAW.						
1 5.	ALL CONSTRUCTION SHALL CONFORM TO TOWN STANDARDS AND REGULATIONS, AND NHOOT STANDARD SPECIFICATIONS FOR ROAD AND BRIDGE CONSTRUCTION, WHICHEVER IS MORE STRINGENT.						
6.	SUBJECT PROPERTY IS PARTIALLY LOCATED WITHIN FEDERALLY DESIGNATED 100 YEAR FLOOD HAZARD ZONE A. REFERENCE FEMA COMMUNITY PANEL NO. 33017 C02110, DATED MAY 17, 2005.						
7.	LANDOWNERS ARE I WETLAND REGULATION	RESPONSIBLE FOR COMPLYING WITH AL ONS, INCLUDING PERMITTING REQUIRED	L APPLICABLE UNDER THESE	LOCAL, STATE AND FEDERAL REGULATIONS.			
8.	ALL CONSTRUCTION PREVENTION PLAN REQUIRED.	ALL CONSTRUCTION ACTIVITIES SHALL BE PERFORMED IN ACCORDANCE WITH THE STORMWATER POLLUTION PREVENTION PLAN (S.W.P.P.P.). THIS DOCUMENT IS TO BE KEPT ONSITE AT ALL TIMES AND UPDATED AS					
9.	PRIOR TO THE START OF CONSTRUCTION, THE CONTRACTOR SHALL COORDINATE WITH THE ENGINEER, ARCHITECT AND/OR OWNER, IN ORDER TO OBTAIN AND/OR PAY ALL THE NECESSARY LOCAL PERMITS, FEES AND BONDS.						
10.	ALL PROPOSED SIGNAGE SHALL CONFORM WITH THE TOWN ZONING REGULATIONS, UNLESS A VARIANCE IS OTHERWISE REQUESTED.						
12.	ALL SCHAGE AND PAYEMENT MARKINGS SHALL BE IN ACCORDANCE WITH THE LATEST EDITION OF THE MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES (M.U.T.C.D.) AND INDOT STANDARDS AND SPECIFICATIONS (NON-REFLECTORIZED PAVEMENT MARKINGS), UNLESS OTHERWISE NOTED.						
13.	ALL PARKING STALLS SHALL BE SEPARATED USING 4" WOE SOLD STRIPES. STRIPING SHALL BE 100% ACTIVIC TYPE, LOW VOC, FAST DRYING, IN A COLOR OF WHITE.						
/ 14.	ALL SIGN BANG SHALL BE 18" IN WIDTH IN A COLOR OF WHITE; ALL TRAFFIC ARROWS SHALL BE PAINTED IN A COLOR OF WHITE.						
15.	ALL CONDITION TO BE SLOPED GRAVITE WITH A MINIMUM RADIUS OF 2', UNLESS OTHERWISE NOTED. ALL BUILDING DIMENSIONS SHALL BE VERIFIED WITH THE ARCHITECTURAL AND STRUCTURAL PLANS PROVIDED BY THE OWNER. ANY DISCREPANCIES SHOULD BE BROUGHT TO THE ATTENTION OF THE ENGINEER AND OWNER PRIOR TO THE START OF CONSTRUCTION. BUILDING DIMENSIONS AND AREAS TO BE TO OUTSIDE OF MASORY, UNLESS OTHERWISE NOTED.						
16.	SNOW TO BE STORE OFFSITE TO AN APP	D AT EDGE OF PAVEMENT AND IN ARE ROVED SNOW DUMPING LOCATION.	eas shown on	THE PLANS, OR TRUCKED			
8 17.	ALL CONSTRUCTION ACTIVITIES SHALL CONFORM TO LABOR OCCUPATIONAL SAFETY AND HEALTH ADMINISTRATION (OSHA) RULES AND RECULATIONS.						
, 18.	THE FOLLOWING VARIANCES HAVE BEEN RECEIVED BY THE CITY OF ROCHESTER ZONING BOARD OF ADJUSTMENT: SECTION 275-20.2.K.3 FOR APARTMENT USE SECTION 275-20.2.K.3 FOR APARTMENT USE SECTION 275-10.2E BUILDING SIZE TABLE 19-B BUILDING HEIGHT						
19.	A CONDITIONAL USE	PERMIT WILL BE REQUIRED FOR ALL Y	Vork within W	ETLAND BUFFERS.			
20,	THE CERTIFICATE OF	OCCUPANCY.	I THE DOPENSE	OF THE APPLICANT PRIOR TO			
22.	TO ANY BLASTING W ADDITIONAL CITY PEI CITY DPW STOR CITY WATER AN	AMITS REQUIRED: MWATER PERMIT D SEWER CONNECTION PERMIT		COJECT PARCEL			
23.	CITY ROW EXCA STATE PERMITS RED	CATION and DRIVEWAY PERMIT	TA	A MAP 137, LOT 35-1			
120	NHDES WETLANI NHDES ALTERAT NHDES SEWER (NHDOT DRIVEWA) permit Non of terrain permit Sonncection permit Y permit	APPLICANT GROEN CONSTRUCTION 120 WASHINGTON STREET SUITE 302				
			ROCHESTER NH 03839 TOTAL LOT AREA				
				8.4 ACRES±			
	SITE P	LAN		DRAWING No.			
WADLEIGH ROAD APARTMENTS ROCHESTER, NH				C3			
SSG WASHING	TON STREET, I	ROCHESTER, NH 03839		SHEET 6 OF 27 JBE PROJECT NO. 21137			









INVASIVE SPECIES NOTES:

- PRIOR TO ANY DISTURBANCE IN AREAS OF JAPANESE KNOTWEED, THE LIMITS OF THE INVASIVE VEGETATION SHALL BE DELINEATED BY A QUALIFIED PROFESSIONAL. 1.
- PRIOR TO EXCAVATION IN INFESTED AREAS, ABOVE OROUND PLANT MATERIAL SHALL BE CAREFULLY CUIT TO AVOID DISPERSING PLANT MATERIAL, BAGGED IN BLACK PLASTIC BAGS AND LANDFILLED, OR PROPERLY DISPOSED OF USING ANOTHER APPROVED METHOD.
- Excavation in Areas of Japanesse knotweed shall ditend six (6) feet Beyond the lateral limit of the plant surface growth to a depth of five (3) feet but not below proosed subgrade or slope limits.
- SOIL EXCAVATED FROM AREAS INFESTED WITH JAPANESE INFOTWEED MUST BE BURIED AT LEAST THREE (5) FEET BELOW GRADE OR PROPERTY DISPOSED OF USING ANOTHER APPROVED METHOD.
- 5. SOIL FROM THESE AREAS MUST NOT BE USED IN OTHER AREAS OF THE SITE. EQUIPMENT THAT OPERATES WITHIN AREAS OF INVASIVE VEGETATION MUST BE CLEANED OF ALL PLANT MATERIAL AND SOLL AT THE SITE OF INFESTATION BEFORE MOVING TO A NOTHER WORK AREA.
- 7. STAGING AREAS AND STOCKPILES SHOULD NOT BE LOCATED IN AREAS OF INVASIVE VEGETATION.
- STOCKPILES OF SOIL CONTAMINATED WITH INVASIVE SPECIES MUST BE ON AN IMPERVIOUS SURFACE AND COVERED.
- 9. SOIL CONTAINING INVASIVE PLANT MATERIAL MUST BE COVERED IF TRANSPORTED.
- 10. MONITOR INVASIVE SPECIES AREAS FOLLOWING GRADING FOR REGROWTH AND TREAT

EROSION CONTROL NOTES:

PROT OVER CATC (TYP) STONE INLET PROTECTION

ALL

- A NHDES WETLAND PERMIT IS REQUIRED FOR ALL WORK WITHIN THE JUSRISDICTIONAL WETLAND. TOTAL WETLAND IMPACT SHOWN = 4,000 SF
- A CONDITIONAL USE PERMIT IS REQUIRED FOR ALL WORK WITHIN THE WETLAND BUFFER AREA. TOTAL BUFFER IMPACT AREA SHOWN = 24,000 SF
- 3. ALL STOCKPILES TO BE SURROUNDED BY SILT SOXX.
- UNDERGROUND FACILITIES UTILITIES AND STRUCTURES HAVE BEEN PLOITED FROM FIELD OBSERVATION AND THER LOCATION MUST BE CONSIDERED APPROXIMATE ONLY. NEITHER JONES & BEACH ENGINEERS, INC., NOR ANY OF THEIR EMPLOYEES TAKE RESPONSIBILITY FOR THE LOCATION OF ANY UNDERGROUND STRUCTURES AND/OR UTILITIES NOT SHOWN THAT MAY EVIST. IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO HAVE ALL UNDERGROUND STRUCTURES AND/OR UTILITIES LOCATED PRIOR TO EXCAVATION WORK BY CALLING AND-DIG-REF (RAB-3LAL-7233) NDERGROUND STRUCTURES
- 5. ALL BENCHMARKS AND TOPOGRAPHY SHOULD BE FIELD VERIFIED BY THE CONTRACTOR.
- 6. SITE GRADING SHALL NOT PROCEED UNTIL EROSION CONTROL MEASURES HAVE BEEN INSTALLED. SEE CONSTRUCTION SEQUENCE ON SHEET ET.
- 7. ALL SWALES AND DETENTION PONDS ARE TO BE STABILIZED PRIOR TO DIRECTING RUNOFF TO THEM. ALL SWALES AND ANY SLOPES GREATER THAN 3:1 SHALL BE STABILIZED WITH NORTH AMERICAN GREEN SCI506N EROSION CONTROL BLANKETS (OR AN EQUIVALENT APPROVED IN WRITING BY THE ENGINEER), UNLESS OTHERWISE SPECIFIED.
- IN AREAS WHERE CONSTRUCTION IS PROPOSED ADJACENT TO ABUTING PROPERTES, THE CONTRACTOR SHALL INSTALL GRANGE CONSTRUCTION FENCING ALONG PROPERTY LINES IN ALL AREAS.
- 10. STONE INLET PROTECTION SHALL BE PLACED AT ALL CATCH BASINS AND CULVERT INLETS. SEE DETAILS WITHIN THE DETAIL SHEETS.
- 11. LAND DISTURBING ACTIVITIES SHALL NOT COMMENCE UNTIL APPROVAL TO DO SO HAS BEEN RECEIVED BY ALL GOVERNING AUTHORITIES. THE GENERAL CONTRACTOR SHALL STRICTLY ADHERE TO THE EPA SWPPP DURING CONSTRUCTION OPERATIONS.
- 12. NO LAND CLEARING OR GRADING SHALL BEGIN UNTIL ALL EROSION CONTROL MEASURES HAVE BEEN INSTALLED.
- 13. ALL EXPOSED AREAS SHALL BE SEEDED AS SPECIFIED WITHIN 3 DAYS OF FINAL GRADING.
- 14. SHOULD CONSTRUCTION STOP FOR LONGER THAN 3 DAYS, THE SITE SHALL BE SEEDED AS SPECIFIED. MAINTAIN EROSION CONTROL MEASURES AFTER EACH RAIN EVENT OF 0.5" OR GREATER IN A 24 HOUR PERIOD AND AT LEAST ONCE A WEEK.
- THIS PLAN SHALL NOT BE CONSIDERED ALL INCLUSIVE, AS THE GENERAL CONTRACTOR SHALL TAKE ALL NECESSARY PRECAUTIONS TO PREVENT SEDIMENT FROM LEAVING THE STE.
- 17. CONSTRUCTION VEHICLES SHALL UTILIZE THE STABILIZED CONSTRUCTION ENTRANCE TO THE EXTENT POSSIBLE THROUGHOUT CONSTRUCTION.
- THE GENERAL CONTRACTOR SHALL BE RESPONSIBLE TO TAKE WHATEVER MEANS NECESSARY TO ESTABLISH PERMANENT SOIL STABILIZATION.
- 19. SEDIMENT SHALL BE REMOVED FROM ALL SEDIMENT BASINS BEFORE THEY ARE 25% FULL.
- 20. ALL WORK SHALL BE DONE IN STRICT ACCORDANCE WITH PROJECT SPECIFICATIONS.

21. ADDITIONAL EROSION AND SEDIMENT CONTROL MEASURES SHALL BE INSTALLED, IF DEEMED NECESSARY BY ON-SITE INSPECTION BY ENGINEER AND/OR REGULATORY OFFICIALS.

- 22. SEE ALSO EROSION AND SEDIMENT CONTROL SPECIFICATIONS ON SHEET ET.
- 23. MARKERS SHALL BE PLACED ALONG WETLAND BOUNDARIES.

EROSION CONTROL PLAN WADLEIGH ROAD APARTMENTS ROCHESTER, NH

SSG, LLC ATTN: FENTON GROEN 120 WASHINGTON STREET, ROCHESTER, NH 03839

DRAWING No.







PRIOR TO THE START OF CONSTRUCTION, THE CONTRACTOR SHALL COORDINATE WITH THE ENGINEER, ARCHITECT AND/OR DWNER, IN ORDER TO OBTAIN AND/OR PAY ALL THE NECESSARY LOCAL PERMITS, CONNECTION FEES AND BONDS.

THE CONTRACTOR SHALL PROVIDE A MINIMUM NOTICE OF FOURTEEN (14) DAYS TO ALL CORPORATIONS, COMPANIES AND/OR LOCAL AUTHORITIES OWNING OR HAVING A JURISDICTION OVER UTILITIES RUNNING TO, THROUGH OR ACROSS PROJECT AREAS PRIOR TO DEMOLITICN AND/OR CONSTRUCTION ACTIVITIES.

THE LOCATION, SIZE, DEPTH AND SPECIFICATIONS FOR CONSTRUCTION OF PROPOSED PRIVATE UTILITY SERVICES SHALL BE TO THE STANDARDS AND REQUIREMENTS OF THE RESPECTIVE UTILITY COMPANY (ELECTRIC, TELEPHONE, CABLE TELEVISION, FIRE ALARM, GAS, WATER, AND SEWER).

A PRECONSTRUCTION MEETING SHALL BE HELD WITH THE OWNER, ENGINEER, ARCHITECT, CONTRACTOR, LOCAL OFFICIALS, AND ALL PROJECT-RELATED UTILITY COMPANIES (PUBLIC AND PRIVATE) PRIOR TO START OF CONSTRUCTION.

ALL CONSTRUCTION SHALL CONFORM TO THE CITY STANDARDS AND REGULATIONS, AND NHDES STANDARDS AND SPECIFICATIONS, WHICHEVER ARE MORE STRINGENT, UNLESS OTHERWISE SPECIFICAT.

ALL CONSTRUCTION ACTIVITIES SHALL CONFORM TO LABOR OCCUPATIONAL SAFETY AND HEALTH ADMINISTRATION (OSHA) RULES AND Regulations,

BUILDING TO BE SERVICED BY UNDERGROUND UTILITIES UNLESS OTHERWISE NOTED.

THE CONTRACTOR IS TO VERIEV LOCATION AND DEPTH OF ALL EXISTING UTILITY STUBS PRIOR TO CONSTRUCTION AND DISCONNECT AL EXISTING SERVICE CONNECTIONS AT THEIR RESPECTIVE MAINS IN ACCORDANCE WITH THE RESPECTIVE UTILITY COMPANY'S STANDARDS AND SPECIFICATIONS. ENGINEER TO BE NOTIFIED.

AS-BUILT PLANS SHALL BE SUBMITTED TO DEPARTMENT OF PUBLIC WORKS.

10. BIVERTS AND SHELVES: MANHOLES SHALL HAVE A BRICK PAVED SHELF AND INVERT, CONSTRUCTED TO CONFORM TO THE SIZE OF PIPE AND FLOW AT CHANGES IN DIRECTION. THE INVERTS SHALL BE LAD OUT IN CURVES OF THE LONGEST RADIUS POSSIBLE TANGENT TO THE CENTER LINE OF THE SENER PIPES. SHELVES SHALL BE CONSTRUCTED TO THE ELEVATION OF THE THROUGH CHANNEL UNDERLAYMENT OF INVERT, AND SHELF SHALL CONSIST OF BRICK MASONRY.

11. FRAMES AND COVERS: MANHOLE FRAMES AND COVERS SHALL BE OF HEAVY DUTY DESIGN AND PROWDE A 30 INCH DIA, CLEAR OPPNING. THE WORD "SEWER" OR DRAIN" SHALL BE CAST INTO THE CENTER OF THE UPPER FACE OF EACH COVER WITH RAISED, 3" LETTERS.

SHALLOW MANHOLE: IN LIEU OF A CONE SECTION, WHEN MANHOLE DEPTH IS LESS THAN 6 FEET, A REINFORCED CONCRETE SLAB COVER MAY BE USED HAVING AN ECCENTRIC ENTRANCE OPENING AND CAPABLE OF SUPPORTING H2D LOADS.

13. CONTRACTOR SHALL PLACE 2" WOE METAL WRE IMPREGNATED RED PLASTIC WARNING TAPE OVER ENTIRE LENGTH OF ALL GRAVITY SEWERS, SERVICES, AND FORCE MAINS.

ALL SANITARY STRUCTURE INTERIOR DIAMETERS (4' MIN) SHALL BE DETERMINED BY THE MANUFACTURER BASED ON THE PIPE CONFIGURATIONS SHOWN ON THESE PLANS.

PROPOSED RIM ELEVATIONS OF DRAINAGE AND SANITARY MANHOLES ARE APPROXIMATE. FINAL ELEVATIONS ARE TO BE SET FLUSH WITH FINISH GRADES. ADJUST ALL OTHER RIM ELEVATIONS OF MANHOLES, WATER GATES, GAS GATES AND OTHER UTILITIES TO FINISH GRADE AS SHOWN ON THE GRADURG AND DRAINAGE FLAN.

ALL WATER MAINS AND SERVICE PIPES SHALL HAVE A MINIMUM 12" VERTICAL AND 24" HORIZONTAL SEPARATION TO MANHOLES, OR CONTRACTOR SHALL INSTALL BOARD INSULATION FOR FREEZING PROTECTION.

WATER MAINS SHALL BE HYDROSTATICALLY PRESSURE TESTED FOR LEAKAGE PRIOR TO ACCEPTANCE. WATERMAINS SHALL BE TESTED AT 1.5 TIMES THE WORKING PRESSURE OR 150 PSI, WHICH EVER IS GREATER, TESTING SHALL BE CONDUCTED IN ACCORDANCE WITH SECTION 4 DF AWWA STANDARD C 800. WATERMAINS SHALL BE DISINFECTED AFTER THE ACCEPTANCE OF THE PRESSURE AND LEAKAGE TESTS ACCORDING TO AWWA STANDARD C 851.

ALL WATER AND SANITARY LEADS TO BUILDING(S) SHALL END S' OUTSIDE THE BUILDING LIMITS AS SHOWN ON PLANS AND SHALL BE PROVIDED WITH A TEMPORARY PLUG AND WITHESS AT END.

20. IF THE BUILDING IS REQUIRED TO HAVE A SPRINKLER SYSTEM, A PRECONSTRUCTION MEETING SHALL BE HELD BETWEEN THE CONTRACTOR, OWNER, ARCHITECT AND THE LOCAL FIRE DEPARTMENT PRIOR TO THE INSTALLATION. 21. THRUST BLOCKS SHALL BE PROVIDED AT ALL BENDS, TEES, MECHANICAL JOINTS AND FIRE HYDRANTS.

22. DIMENSIONS ARE SHOWN TO CENTERLINE OF PIPE OR FITTING.

23. REFER TO FIRE PROTECTION SHEETS FOR LOCATION AND DETAIL OF FIRE LINE LEAD IN TO BUILDING.

24. FIRE LINE SHALL BE STUBBED UP 1' ABOVE FINISH FLOOR ELEVATION IN SPRINKLER ROOM.

25. THE CONTRACTOR SHALL HAVE THE APPROVAL OF ALL GOVERNING AGENCIES HAVING JURISDICTION OVER FIRE PROTECTION SYSTEM PRIOR TO INSTALLATION.

25. CONTRACTOR TO FURNISH SHOP DRAWINGS FOR UTILITY RELATED ITEMS TO ENSURE CONFORMANCE WITH THE PLANS AND SPECIFICATIONS. SHOP DRAWINGS SHOULD BE SENT IN TRIPLICATE TO THE DESIGN ENGINEER FOR REVIEW AND APPROVAL PRIOR TO INSTALLATION.

27. EXISTING UTILITIES SHALL BE DIGSAFED BEFORE CONSTRUCTION.

28. ALL WATER LINES SHOULD HAVE TESTABLE BACKFLOW PREVENTERS AT THE ENTRANCE TO BUILDING. TESTABLE BACKFLOW PREVENTION DEVICES MUST BE REUSTERED WITH THE CITY UTILITY BILLING OFFICE. TEST RESULTS SHALL BE SUBMITTED TO UTILITY BILLING PRIOR TO DPW SIGN-OFF ON CERTIFATE OF OCCUPANCE.

ALL GRAVITY SEWER PIPE, MANHOLES, AND FORCE MAINS SHALL BE TESTED ACCORDING TO NIDES STANDARDS OF DESIGN AND CONSTRUCTION FOR SEWAGE AND WASTEWATER TREATMENT FACILITIES, CHAPTER ENV-WQ 700, ADOPTED ON 10-15-14.

30. ENV-WO 704.06 GRAVITY SEWER PIPE TESTING. GRAVITY SEWERS SHALL BE TESTED FOR WATER TRAINESS BY USE OF LOW-PRESSURE AIR TESTE CONFORMING WITH ASTIM F1417-82(2005) OR UNI-BELL PVC PIPE ASSOCIATION UNI-B-B. LINES SHALL BE CLEANED AND VISUALLY INSPECTED AND TRUE TO UNE AND GRADED. DEFLECTION TESTES SHALL I AVE PLACE AFTER 30 DAYS FOLLOWING INSTALLATION AND THE MAXMUM ALLOWABLE DEFLECTION OF FLORBLE SEMER PIPE SHALL BE SC OF AVERAGE WISIDE DIAMETER A ROOD BALL OR HAND THE MAXMUM ALLOWABLE DEFLECTION OF FLORBLE SEMER PIPE SHALL BE SC OF AVERAGE INSIDE PIPE TRAIL BE CLEANED AND THE MANDREL WITH A DUALETER OF AT LEAST 55% OF THE AVERAGE INSIDE PIPE DIAMETER A ROOD BALL OR THE DEFLECTION TEST SHALL BE CONDUCTED WITHOUT MECHANICAL PULLING DEVICES.

ENV-WO 704.17 SEWER MANHOLE TESTING, SHALL BE TESTED FOR LEAKAGE USING A VACUUM TEST PRIOR TO BACKFILLING AND PLACEMENT OF SHELVES AND INVERTS.

SANITARY SEWER LINES SHALL BE LOCATED AT LEAST TEN (10) FEET HORIZONTALLY FROM AN EXISTING OR PROPOSED WATER LINE, WHEN A SEWER LINE CROSSES UNDER A WATER LINE, THE SEWER PIPE JOINTS SHALL BE LOCATED AT LEAST & FEET HORIZONTALLY FROM THE WATERMAIN. THE SEWER LINE SHALL ALSO MAINTAIN A VERTICAL SEPARATION OF NOT LESS THAN 18 INCHES.

33. SEWERS SHALL BE BURIED TO A MINNUM DEPTH OF 6 FEET BELOW GRADE IN ALL ROADWAY LOCATIONS, AND TO A MINIMUM DEPTH OF 4 FEET BELOW GRADE IN ALL CROSS-COUNTRY LOCATIONS. PROVIDE TWO-INDES OF R-10 FOAM BOARD INSULATION 2-FOOT WIDE TO BE INSTALLED B-INDERS OVER SEWER PIPE IN AREAS WHERE DEPTH IS NOT ACHIEVED. A WAVER FROM THE DEPARTMENT OF ENVIRONMENTAL SERVICES WASTEWATER ENGINEERING BUREAU IS REQUIRED PRIOR TO INSTALLING SEWER AT LESS THAN MINIMUM COVER.

34. ALL WATER AND SANITARY LEADS TO BUILDING(S) SHALL END AT RIGHT OF WAY AS SHOWN ON PLANS AND SHALL BE PROVIDED WITH A TEMPORARY PLUG AND WITNESS AT END.

35. THE CONTRACTOR SHALL MINIMIZE THE DISRUPTIONS TO THE EXISTING SEWER FLOWS AND THOSE INTERRUPTIONS SHALL BE LIMITED TO FOUR (4) HOURS OR LESS AS DESIGNATED BY THE TOWN SEWER DEPARTMENT.

LIGHTING CONDUIT SHALL BE SCHEDULE 40 PVC, AND SHALL BE INSTALLED IN CONFORMANCE WITH THE NATIONAL ELECTRIC CODE. CONTRACTOR SHALL PROVIDE EXCAVATION AND BACKFILL.

37. ALL TRENCHING, PIPE LAYING, AND BACKFILLING SHALL BE IN ACCORDANCE WITH FEDERAL OSHA REGULATIONS,

38. DISINFECTION OF WATER MAINS SHALL BE CARRED OUT IN STRICT ACCORDANCE WITH AWAR STANDARD C651, LATEST EDITION. THE BASIC PROCEDURE TO BE FOLLOWED FOR DISINFECTING WATER MAINS IS AS FOLLOWS. O. PREVENT CONTAMINATING MATERIALS FROM ENTERING IS AS FOLLOWS. B. REMOVE, BY FLUSSING OR OTHER MEANS, THOSE MATERIALS THAT MAY HAKE DIRED THE WATER MAINS. C. CHLORNATE ANY RESOLUCION ON THAT MAY REDAIN, AND FLUSH THE CHLORNET WATER MAINS. C. CHLORNATE ANY RESOLUCION SYSTEM FROM BACKFLOW DUE TO HYDROSTATIC PRESSURE TEST AND DISINFECTION PROCEDURES.

OCCURES. B. DETERMINE THE BACTERIOLOGICAL QUALITY BY LABORATORY TEST AFTER DISINFECTION, f. MAKE FINAL CONNECTION OF THE APPROVED NEW WATER MAIN TO THE ACTIVE DISTRIBUTION SYSTEM

UTILITY PLAN	DRAWING No.
WADLEIGH ROAD APARTMENTS ROCHESTER, NH	U1
SSG, LLC ATTN: FENTON GROEN WASHINGTON STREET, ROCHESTER, NH 03839	SHEET 11 OF 27 JBE PROJECT NO 21137



11	Designed and Produced in NH	Plan Norma
J In Iones	& Beach Engineers Inc	Pian Name:
D	a beach Engineers, mc.	Project:
85 Portsmouth Ave. Civil	Engineering Services 603-772-4746	
PO Box 219 Stratham, NH 03885	FAX: 603-772-0227 E-MAIL: JBE@JONESANDBEACH.COM	Owner of Record:



THES: THIS STE WILL REQUIRE A USEPA NPDES PERMIT FOR STORMWATER DISCHARGE FOR THE CONSTRUCTION STEL THE CONSTRUCTION STE OPERATOR SHALL DEVELOP AND IMPLEMENT A CONSTRUCTION STORM WATER POLLUTION PREVENTION PLAN (SMPPP), WHICH SHALL REMAIN ON STE AND BE MADE ACCESSBLE TO THE PUBLIC. THE CONSTRUCTION STE OPERATOR SHALL SUBJIT A NOTICE OF INTERT (NOT) TO THE EPA REGIONAL OPERATOR STORMWATER/NOT/NOISEARCH/CPM. AUTHORIZATION STEL DAY WORK NO. STELE DAY HE NOT AT HTTP://OPPUBLEPA.GOV/MPDES/STORMWATER/NOT/NOISEARCH/CPM. AUTHORIZATION STELE DAY HE NOT AT HTTP://OPPUBLEPA.GOV/MPDES/STORMWATER/NOT/NOISEARCH/CPM. AUTHORIZATION STELE DAY HE NOT AT HTTP://OPPUBLEPA.GOV/MPDES/STORMWATER/NOT/NOISEARCH/CPM. AUTHORIZATION STELE DAY HE NOT STORM THAT AND ANYS AFTER ETHER OF THE FOLLOWING CONTINUES HALE BESINTED TO HE MPDES PERMITTING AUTHORITY WITHIN 30 DAYS AFTER ETHER OF THE FOLLOWING CONTINUES HALE BESINTED A. FINAL STABILIZENCH HAS BEEN ACHIEVED ON ALL PORTIONS OF THE STE FOR WHICH THE PERMITTER IS RESPONSIBLE; OR A. NOTHER OPERATOR/PERMITTEE HAS ASSUMED CONTROL OVER ALL AREAS OF THE STE THAT HAVE NOT BEEN FINALLY STABILIZED, PROVIDE DAY WITH A COPY OF THE NOTICE OF TERMINATION (NOT).

ALL ROAD AND DRAINAGE WORK SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE STANDARD SPECIFICATIONS FOR THE CITY, AND INHOT SPECIFICATIONS FOR ROAD AND BIRDGE CONSTRUCTION, WHICHEVER IS MORE STRINGENT.

DEVELOPER IS RESPONSIBLE FOR COMPLYING WITH ALL APPLICABLE LOCAL, STATE AND FEDERAL WETLAND REGULATIONS, INCLUDING ANY PERMITTING AND SETBACK REQUIREMENTS REQUIRED UNDER THESE REGULATIONS.

CONTRACTOR TO COORDINATE AND COMPLETE ALL WORK REQUIRED FOR THE RELOCATION AND/OR INSTALLATION OF ELECTRIC, CATV, TELEPHONE, AND FRE ALARM PER UTILITY DESIGN AND STANDARDS. LOCATIONS SHOWN ARE APPROXIMATE. LOW PROFILE STRUCTURES SHALL BE USED TO THE GRAFTEST EXTERM FOSSIBLE.

5. THIS PLAN HAS BEEN PREPARED BY JONES & BEACH ENGINEERS, INC. FOR MUNICIPAL AND STATE APPROVALS AND FOR CONSTRUCTION BASED ON DATA OBTAINED FROM ON-SITE FIELD SURVEY AND EXISTING MUNICIPAL RECORDS. THROUGHOUT THE CONSTRUCTION PROCESS. THE CONTRACTOR SHALL INFORM THE DENGREE MUNICIPAL CAND STATE DUSCREPANDED VERY SHOWN ON THE DESIGN PLANS. THIS INCLUDES ANY UNFORESEEN CONDITIONS, SUBSURFACE OR OTHERWISE, FOR EVALUATION AND RECOMMENDATIONS. ANY CONTRADICTION BETWEEN THEIS OF THIS PLAY/PLAN SET, OR BETWEEN THE PLANS AND ON-SITE CONSTRUCTIONS MUST BE RESULVED BEFORE RELATED CONSTRUCTION HAS BEEN INITIATED.

6. SILTATION AND EROSION CONTROLS SHALL BE INSTALLED PRIOR TO CONSTRUCTION, SHALL BE MAINTAINED DURING CONSTRUCTION, AND SHALL REDMAIN UNTIL SITE HAS BEEN STABILIZED WITH PERMANENT VEGETATION. SEE DETAIL SHEET EI FOR ADDITIONAL NOTES ON REVOSION CONTROL.

ALL DISTURBED AREAS NOT STABILIZED BY NOVEMBER 1nt SHALL BE COVERED WITH AN EROSION CONTROL BLANKET. PRODUCT TO BE SPECIFIED BY THE ENGINEER.

8. FINAL DRAINAGE, GRADING AND EROSION PROTECTION MEASURES SHALL CONFORM TO REGULATIONS OF THE PUBLIC WORKS DEPARTMENT.

9. CONTRACTOR TO VERIFY EXISTING UTILITIES AND TO NOTIFY ENGINEER OF ANY DISCREPANCY IMMEDIATELY.

10. ROADWAY INTERSECTIONS WITH SLOPE GRANITE CURB SHALL EXTEND AROUND RADIUS WITH 6' STRAIGHT PIECE ALONG TANGENT.

11. RETAINING WALLS SHALL BE DESIGNED AND STAMPED BY A LICENSED PROFESSIONAL ENGINEER. CONTRACTOR SHALL COORDINATE WITH MANUFACTURER PRIOR TO INSTALLATION.

8" PERFORATED ADS UNDER DRAIN PLACEMENT TO BE DETERMINED BY THE ENGINEER DURING TIME OF SUBGRADE INSPECTION CONTRACTOR TO ADJUST LOCATION IN THE FIELD ONLY WITH FROM APPROVAL OF PROJECT ENGINEER OR PUBLIC WORKS DEPARTMENT. CONTRACTOR TO INCLUDE 3000 LF IN BID PROC.

13. ENGINEER TO INSTALL PERMANENT BENCHMARK (REINFORCED GRANITE MARKER) AT LOCATIONS SHOWN ON PLANS, BENCH MARKS TO BE TIED TO STATE PLANE COORDINATE SYSTEM.

14. DRAINAGE INSPECTION AND MAINTENANCE SCHEDULE: SILT FENCING WILL BE INSPECTED DURING AND AFTER STORM EVENTS TO ENSURE THAT THE FENCE STILL HAS INTEGRATY AND IS NOT ALLOWING SEDUILENT TO PASS. SEDUILENT BUILD UP IN SWALES WILL BE REMOVED IF II IS DEEPER THAN SIX INCHES, AND IS TO BE REMOVED FROM SUMPS BELOW THE INITE! OF CULVENTS SEMIANNUALLY, AS WELL AS FROM CATCH BASINS, FOLLOWING MAJOR STORM EVENTS, THE STAGE DESCHARGE OUTLET STRUCTURES ARE TO BE INSPECTED AND ANY DEERIS REMOVED FROM THE ORIFICE, TRASH TRACK AND EMERGENCY SPILL WAY. INFREQUENTLY, SEDUMENT MAY ALSO HAVE TO BE REMOVED FROM THE SUMP OF THE STRUCTURE.

15. ALL DRAINAGE INFRASTRUCTURE SHALL BE INSTALLED AND STABILIZED PRIOR TO DIRECTING ANY RUNOFF TO IT.

16. DEEDNIGN PONDS RÉQUIRE TIMELY MARTENANCE AND SHOULD BE INSPECTED AFTER EVERY MAJOR STORM EVENT, AS WELL AS FREQUENTLY DURING THE FIRST YEAR OF OPERATION, AND ANNUALLY THEREAFTER. EVERY MAJOR STORM EVENT, AS WELL AS PROFESSIONAL ENGINEET SHOLLD BE RETAINED TO PERFORM A THOROUGH INSPECTION OF THE DETENTION POND AND ITS INFRASTRUCTURE. ANY DEBNS AND SEMILENT ACCUMULATIONS SHOULD BE REMOVED FROM THE CUTLET STRUCTURE(S) AND EMERCEVY SPLUAWY(S) AND DISPOSED OF RPOPERLY, DETENTION POND BEALLOWED AT DER'ST ONES ANNUALLY SO AS TO PREVENT THE ESTABLISHIENT OF WOODY VERETATION. THESE SHOULD BE REALIDED AT DIS ANNUALLY SO AS TO PREVENT THE ESTABLISHIENT OF WOODY VERETATION. THESE SHOULD INCREMS THE POTOTIAL FOR TAULIRE, ANS SHOWING SIGNS OF ENGISION OR THIN OR DYING VEGETATION SHOULD BE REPAIRED IMMEDIATELY BY WHATEVER MEANS SHOULD BE TRAPPED AND RECOGEND OF THIN OR DYING VEGETATION SHOULD BE REPAIRED IMMEDIATELY BY WHATEVER MEANS SHOULD BE TRAPPED AND RELOCATED IF THE PROBLEM PERSISTS.

17. THE DETENTION PONDS ARE TO BE CONSTRUCTED PRIMARILY THROUGH EXCAVATION. IN THOSE AREAS WHERE THE BERMS MUST BE CONSTRUCTED BY THE PLACEMENT OF FILL, THE ENTIRE EMBANKUENT AREA OF THE DETENTION PONDS SHALL BE EXCAVATED TO PROPOSED GRADE, STRIPPED OF ALL ORGANIC MATERIALS, COMPACTED TO AT LEAST 95% AND SCAFTED PROF TO THE PLACEMENT OF THE EMBANKUENT MATERIAL, IN THE EVENT THE FOUNDATION MATERIAL SCORPES DOES NOT ALLOW THE SPECIFIED COMPACTION, AN ADDITIONAL ONE FOOT (1) OF EXCAVATION AND THE PLACEMENT OF A ONE FOOSED DOES NOT ALLOW THE SPECIFIED COMPACTION, AN ADDITIONAL ONE SOUT (1) OF EXCAVATION AND THE PLACEMENT OF A ONE FOOT (1'T) THICK, THELVE FOOT (12') WIDE PAD OF THE MATERIAL DESCRIBED IN THE NOTE BELOW, COMPACTED TO 95% OF ASTM D-1557 MAY BE NECESSARY. PLACEMENT AND CONFACTION SHOULD OCCUR AT AL A MOSTURE CONTENT OF OPTIMUM PLUS OR MINUS 3%, AND NO FROZEN OR ORGANIC MATERIAL SHOULD BE PLACED WITHIN FOR ANY REASON.

18. EMBANIQUENT MATERIAL FOR THE BERMS SHALL BE CLEAN MINERAL SOL. WITH A CLAY COMPONENT FREE OF ROOTS, ORGANIC MATTER, AND OTHER DELETEROUS SUBSTANCES, AND SHALL CONTAIN NO ROCKS OR LUMPS OVER FOUR NOVES (4") IN DIAMETER. THIS MATERIAL SHOULD BE INSTALLED IN 6" LIFTS AND COMPACTED TO 95% OS ASTIN D-1557, AND SHOULD MEET THE FOLLOWING SPECIFICATIONS: 4" PASSING 100%, #4 SIEVE 25-70%, #200 SIEVE 10-29% (IN TOTAL SAMPLE).

19. ENBANKMENT IS TO HAVE 3:1 SIDE SLOPES (MAX.) AND IS TO BE BROUGHT TO SPECIFIED GRADES PRIOR TO THE ADDITION OF LOAM (4* MINIMUM) SO AS TO ALLOW FOR THE COMPACTION OF THE STRUCTURE OVER TIME WAILE MAINTAINING THE PROPER BERM ELEVATION.

20. COMPACTION TESTING SERVICES (LE. NUCLEAR DENSITY TESTS) ARE TO BE PERFORMED BY AN INDEPENDENT GEOTECHNICAL ENGINEER RETAINED BY THE CONTRACTOR FOR ROADWAY CONSTRUCTION, AND ON THE FOUNDATION OF THE BERM AND ON EVERY LIFT OF NEWLY PLACED MATERIAL.

PLAN AND PROFILE

WADLEIGH ROAD APARTMENTS ROCHESTER, NH

SSG, LLC ATTN: FENTON GROEN

120 WASHINGTON STREET, ROCHESTER, NH 03839

DRAWING No








	$T_{} = 0, D_{} = 1, D_{} = T_{}$	-
THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE).	Jones & Beach Engineers, Inc.	Project:
ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE. AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE. REV. DATE REVISION BY	Ve. Civil Engineering Services 603-772-4748 FAX: 603-772-0227 E-MAIL: JBE@JODESANDBEACH COM	Owner of Record:







BY

REVISION

SSG, LLC ATTN: FENTON GROEN 120 WASHINGTON STREET, ROCHESTER, NH 03839 Owner of Record:

- 1. THE CONTRACTOR SHALL LOCATE AND VERIFY THE EXISTENCE OF ALL UTILITIES PRIOR TO STARTING WORK.
- PLANTS FURNISHED IN CONTAINERS SHALL HAVE THE ROOTS WELL ESTABLISHED IN THE SOIL MASS AND SHALL HAVE AT LEAST ONE (1) GROWING SEASON. ROOT-BOUND PLANTS OR INADEQUATELY SIZED CONTAINERS TO SUPPORT THE PLANT MAY BE DEEMED UNACCEPTABLE.
- BY THE END OF THE GUARANTEE PERIOD, THE CONTRACTOR SHALL HAVE REPLACED ANY PLANT MATERIAL THAT IS MISSING, NOT ITRUE TO SIZE AS SPECIFIED, THAT HAS DIED, LOST NATURAL SHAPE DUE TO DEAD BRANCHES, EXCESSIVE PRUNING OR INADEQUATE OR IMPROPER CARE, OR THAT IS, IN THE OPINION OF THE LANDSCAFE ARCHITECT, IN UNHEALTHY OR UNSIGHTLY CONDITION.
- ALL LANDSCAPING ON THE PLANS SHALL BE MAINTAINED AND DEAD OR DYING VEGETATION SHALL BE REPLACED IN A TIMELY MANNER.

PLANT 1 INCH ABOVE SURROUNDING GROUND

3" PINE BARK MULCH ON WEED FABRIC, DO NOT COVER STEMS OR TRUNK, UNTIE AND CUT AWAY BURLAP FROM 1/3 OF ROOT BALL (MIN); IF SYNTHETIC WRAP IS USED,

REMOVE COMPLETELY SLOPE SOIL TO FORM SALICET

PLANT BACK FILL MIXTURE

- EXISTING OR COMPACTED SUBGRADE

8"--12" COMPACTED UNSCREEMED TOPSOIL REQUIRED WHERE SUBGRADE MATERIALS ARE ROCK AND GRAVEL

NOTE: LOOSEN ROOTS AT THE OUTER EDGE OF ROOT BALL OF CONTAINER GROWN SHRUBS.

DRAWING No.

L1

SHEET 17 OF 27 JBE PROJECT NO. 21137

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luentity	Botanical Neme	Common Name	Size
3	Ablee balsamee	BALSAM FIR	8-10 FT. HT
2	Acer palmatum "Bloodgood"	BLOODGOOD JAPANESE MAPLE	15 GALLON
3	Juniperus scopulorum "Wichits Blue"	WICHITA BLUE MT JUNIPER	7-8 FT. HT.
4	Picea pungeris	COLORADO SPRUCE	8-10 FT. HT
5	Pinus strobus	EASTERN WHITE PINE	10-12 FT HT
4	Primus semilata 'Kwanzan'	KWANZAN ORIENTAL CHERRY	2.5" CALIPER
6	Pyrus calleryana 'Chanticleer'	CHANTICLEER CALLERY PEAR	2.5" CALIPER
8	Thuật plicate Green Gianf	GREEN GIANT ARBORVITAE	7.8 FT HT
3	Tilla cordata 'Greenspire'	GREENSPIRE LITTLELEAF LINDEN	2 CALIDED
2	Hibiscus syriacus 'DVPazum'	BUILE SATIN BOSE OF SHARON	CONLIPER
37	liex giabra 'Shamrock'	SHAMROCK INKREPRY HOLLY	5 GALLON
18	Pennisetum orientale 'Karley Rose'	KARLEY ROSE FOUNTAIN GRASS	2 CALLON



SITE ELECTRICAL CONTRACTOR SHALL COORDINATE LOCATION OF EASEMENTS, UNDERGROUND UTILITIES AND DRAINAGE BEFORE DRILLING POLE BASES. CONTRACTOR SHALL INSTALL PROPOSED LIGHT POLES ACCORDING TO TOWN REGULATIONS ALL OUTDOOR LIGHTING SYSTEMS SHALL BE EQUIPPED WITH TIMERS TO REDUCE ILLUMINATION LEVELS TO NON-OPERATIONAL VALUES PER TOWN REGULATIONS, LIGHTING CONDUIT SHALL BE SCHEDULE 40 PVC, AND SHALL BE INSTALLED IN CONFORMANCE WITH THE NATIONAL ELECTRICAL CODE. CONTRACTOR SHALL PROVIDE EXCAVATION AND BACKFILL 518 ILLUMINATION READINGS SHOWN ARE BASED ON A TOTAL LLF OF 0.75 AT GRADE. ILLUMINATION READINGS SHOWN ARE IN UNITS OF FOOT-CANDLES. LIGHTING CALCULATIONS SHOWN ARE NOT A SUBSTITUTE FOR INDEPENDENT ENGINEERING ANALYSIS OF LIGHTING SYSTEM AND SAFETY, ALL LIGHTING FIXTURES SHALL BE FULL CUT-OFF DARK-SKY COMPLIANT, UNLESS OTHERWISE NL INDICATES THAT THIS LUMINAIRE SHALL BE ON A NIGHT LIGHT CIRCUIT, FL INDICATES THAT THIS LUMINAIRE SHALL BE A FLOOD LIGHT FIXTURE. MOUNTING BRACKET FOR THIS FL INTURE SHALL BE MOUNTED 25' ADOVE BOTTOM OF POLE BASE FOR ALL LIGHT POLES CLOSEST TO STOREPRONT. THESE DESIGNATIONS INDICATE WHAT PHASE LIGHTS ARE WIRED TO (TYP). THE PROPOSED LIGHTING CALCULATIONS AND DESIGN WAS PERFORMED BY CHARRON, INC., P.O. BOX 4550, MANCHESTER, MH 03108, ATTENTION KEN SWEDTEY. ALL LIGHTS SHOULD BE PURCHASED FROM THIS COMPANY, OR AN EQUAL LIGHTING DESIGN SHOULD BE SUBMITED FOR REVIEW IF EQUAL SUBSTITUTIONS ARE PROPOSED BY THE CONTRACTOR OR OWNER. McGrow_Edion McGraw-Edison **GLEON Galleon** GWC Galleon Wall Area / Site Luminale Nali Mount Lum (9467 Applecations @@@**@@@**@@@ 😂 😔 💆 Odamsaturi I Webidine Enlighted WaveLow Enlighted 1 64 19 6m m m 28 2940 m m 640 may m -COOPER States and PROPERTY PROF Luminaire Schedule Arrangement Back-Back Qty Descrip P5-2 GLEON-SAID-740-U-SWO SSS4A20SFN2 (20' AFG) GLEON-SA1C-740-U-SL3 / **S**3 Single SSS4A20SFN1 (20' AFG) GLEON-SA1C-740-U-T4FT / SSS4A20SFN1 (20' AFG) GWC-SA1A-740-U-SL3 / WALL MTD Single W3 Single 15' AFG LIGHTING PLAN DRAWING No. WADLEIGH ROAD APARTMENTS ROCHESTER, NH L2SSG, LLC ATTN: FENTON GROEN 120 WASHINGTON STREET, ROCHESTER, NH 03839 SHEET 18 OF 27 JBE PROJECT NO. 21137



Design: LAZ Draft: LAZ Date: 9/8/21			1				
Checked: BAJ Scale: 1"=30' Project No.:21137		5	2/10/22	REVISED PER CITY COMMENTS	LAZ	Designed and Produced in NH	
Drawing Name: 21137-PLAN.dwg	MICHAEL TA	4	1/14/22	REVISED PER CITY COMMENTS	LAZ		Plan Name:
THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN	PEDBUALS	3	12/14/21	REVISED PER CITY COMMENTS	LAZ	VIR Jones & Beach Engineers, Inc.	
PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE).	No.9848	2	12/6/21	REVISED PER CONSERVATION COMMISSION COMMENTS	LAZ		Project:
ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE	1 LICENSO	1	9/21/21	ISSUED FOR PLANNING BOARD	LAZ	85 Portsmouth Ave. Civil Engineering Services 603-772-4746	
AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.	STRONG. W	REV.	DATE	REVISION	BY	PO Box 219 FAX: 603-772-0227 Stratham, NH 03995	Owner of Record:
	and a latter a					CHINE, SEGONEANDBEACH.COM	



















				CHANNEL
TABLE 7-24REG	COMMENDED	RIP RAP GR	RADATIO	N RANGES
THICKNESS OF RIP	RAP = 1.	5 FEET		
d50 SIZE≈	0.50	FEET	6	INCHES
% of weight sma Than the given (ller 150 size	SIZE OF	STONE	(INCHES) TO
100%		9		12
85%		8		11
50%		6		9
15%		2		3

NOTES:

THE SUBGRADE FOR THE GEOTEXTILE FABRIC AND RIP RAP SHALL BE PREPARED TO THE LINES AND GRADES SHOWN ON THE PLANS.

2. THE RIP RAP SHALL CONFORM TO THE SPECIFIED GRADATION.

3. GEOTEXTLE FABRICS SHALL BE PROTECTED FROM PUNCTURE OR TEARING DURING THE PLACEMENT OF THE ROCK RD. DAMAGED AREAS IN THE FABRIC SHALL BE REPARED BY PLACING A PIECE OF FABRIC OVER THE DAMAGED AREA OR BY COMPLETE REPLACEMENT OF THE FABRIC. ALL OVERLAPS REQUIRED FOR REPARTS OR JOINING TWO PIECES OF FABRIC SHALL BE A MINIMUM OF 12 INCERS.

4. STONE FOR THE RIP RAP MAY BE PLACED BY EQUIPMENT AND SHALL BE CONSTRUCTED TO THE FULL LAYER THICKNESS IN ONE OPERATION AND IN SUCH A MANNER AS TO PREVENT SEGREGATION OF THE STONE SIZES.

5. OUTLETS TO A DEFINED CHANNEL SHALL HAVE 2:1 OR FLATTER SIDE SLOPES AND SHOULD BEGIN AT THE TOP OF THE CULVERT AND TAPER DOWN TO THE CHANNEL BOTTOM THROUGH THE LENGTH OF THE APRON.

6. <u>MANTENANCE:</u> THE OUTLET PROTECTION SHOULD BE CHECKED AT LEAST ANNUALLY AND AFTER EVERY MAJOR STORM, IF THE RIP RAP HAS BEEN DISPLACED, UNDERNINED OR DAMAGED, IT SHOULD BE REPARED INMEDIATELY. THE CHAINEL IMMEDIATELY BELOW THE OUTLET SHOULD BE CHECKED TO SEE THAT EROSION IS NOT OCCURENCE. THE DOWNSTREAM CHAINEL SHOLLD BE KEPT CLEAR OF OSSTRUCTIONS SUCH AS ALLEN TREES, DEBRIS, AND SEDMENT THAT COULD CHACE TOW PATTERNS AND/OR TALENDER DEPTHS ON THE PIPES. REPAIRS MUST BE CARRIED OUT IMMEDIATELY TO AVOID ADDITIONAL DAMAGE TO OUTLET FROLEDION.

RIP RAP OUTLET PROTECTION APRON

NOT TO SCALE



- 1. PREPARE SOIL BEFORE INSTALLING BLANKETS, INCLUDING ANY NECESSARY APPLICATION OF LINE, FERTUZZER, AND SEED, NOTE: WHEN USING CELL-O-SEED DO NOT SEED PREPARED AREA. CELL-O-SEED MUST BE INSTALLED WITH PAPER SIDE DOWN.
- 2. BEGIN AT THE TOP OF THE SLOPE BY ANCHORING THE BLANKET IN A 6" DEEP BY 6" WIDE TRENCH WITH APPROXIMATELY 12" OF BLANKET EXTENDED BEYOND THE UP-SLOPE PORTION OF THE TRENCH. ANCHOR THE BLANKET WITH A ROW OF STARLES/STAKES APPROXIMATELY 12" APART IN THE BOTTOM OF THE TRENCH. BACKTILL AND COMPACT THE TRENCH AFTER STAPLING. APPLY SEED TO COMPACTED SOIL AND FOLD REMAINING 12" PORTION OF BLANKET BACK OVER SEED AND COMPACTED SOIL. SECURE BLANKET OVER COMPACTED SOIL WITH A ROW OF STAPLES/STAKES SPACED APPROXIMATELY 12" APART ACROSS THE WIDTH OF THE BLANKET.
- 3. ROLL THE BLANKETS (A) DOWN OR (B) HORIZONTALLY ACROSS THE SLOPE. BLANKETS WILL UNROLL WITH APPROPRIATE SIDE AGAINST THE SOIL SURFACE. ALL BLANKETS WUST BE SECURELY FASTEMED TO SOIL SURFACE BY PLACING STAPLES/STAKES IN APPROPRIATE LOCATIONS AS SHOWN IN THE STAPLE PATTERN GUIDE. WHEN USING OPTIONAL DOT SYSTEMM, STAPLES/STAKES SHOULD BE PLACED THROUGH EACH OF THE COLORED DOTS SOURSEPONDING TO THE APPROPRIATE STAPLE PATTERN.
- 4. THE EDGES OF PARALLEL BLANKETS MUST BE STAPLED WITH APPROXIMATELY 2"--5" OVERLAP DEPENDING ON BLANKET TYPE. TO ENSURE PROPER SEAM ALIGNMENT, PLACE THE EDGE OF THE OVERLAPPING BLANKET BEING INSTALLED ON TOP) EVEN WITH THE COLORED SEAM STITCH ON THE PREVOUSLY INSTALLED BLANKET.
- CONSECUTIVE BLANKETS SPLICED DOWN THE SLOPE MUST BE PLACED END OVER END (SHINGLE STYLE) WITH AN APPROXIMATE 3" OVERLAP, STAPLE THROUGH OVERLAPPED AREA, APPROXIMATELY 12" APART ACROSS EMITTE BLANKET WITH, NOTE: IN LOOSE SOIL CONDITIONS, THE USE OF STAPLE OR STAKE LENGTHS GREATER THAN 6" MAY BE NECESSARY TO PROPERLY SECURE THE BLANKETS.



-800-772-2040

EROSION CONTROL BLANKET SLOPE INSTALLATION NORTH AMERICAN GREEN (800) 772-2040

NOT TO SCALE





TEMPORARY SEDIMENT BASIN

NOT TO SCALE

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		9/21/21	ISSUED FOR PLANNING BOARD	LAZ
-	2	12/6/21	REVISED PER CONSERVATION COMMISSION COMMENTS	LAZ
	3	12/14/21	REVISED PER CITY COMMENTS	LAZ
3[4	1/14/22	REVISED PER CITY COMMENTS	LAZ
11	5	2/10/22	REVISED PER CITY COMMENTS	LAZ



1. ALL STRUCTURES SHOULD BE INSPECTED AFTER EVERY RAINFALL AND REPAIRS MADE AS NECESSARY. SEDIMENT SHOLLD BE REMOVED FROM TRAPPING DEVICES AFTER THE SEDIMENT HAS REACHED A MAXMUN OF ONE HALF THE DEPTH OF THE TRAP. THE SEDIMENT SHOLLD BE DISPOSED IN A SUITABLE UPLAND AREA AND PROTECTED FROM EROSION BY EITHER STRUCTURE OR VEGETATIVE MEANS. THE TEMPORARY TRAPS SHOULD BE REMOVED AND THE AREA REPARED AS SOON AS THE CONTRIBUTING DRAINAGE AREA TO THE INTEL THAS BEEN COMPLETED; STABILIZED.

TEMPORARY CATCH BASIN INLET PROTECTION (Block and Gravel Drop Inlet Sediment Filter)

NOT TO SCALE



AMOCO 2004 GEOTEXTILE

PRE-CAST FOO

1

FINISH GRADE

NOTES:

NOT TO SCALE





SSG, LLC ATTN: FENTON GROEN 120 WASHINGTON STREET, ROCHESTER, NH 03839







Building Areas:

Level 1 Level 2 Level 3 Level 4	17,280sf 17,280sf 16,929sf 17,280sf 68,769sf
Total	68,769sf



Wadleigh Road Apts



Apartme	ent Count:		
	1 Bedroom	2 Bedrooms	Total
Level 1	4	4	8
Level 2	4	10	14
Level 3	5	10	15
Level 4	5	10	15
Totals	18	34	52









Wadleigh Road Apts







1 Level 3 Floor Plan 3/32" = 1'-0"



Wadleigh Road Apts

Wadleigh Rd. Rochester, NH 03839



LEVEL 4 FLOOR PLAN SIMILAR









2 East Elevation 3/32" = 1'-0"





EGGA A R C H I T E C T S ONE VERMON Street Newburyport, MA 01950 978-462-5515

Wadleigh Road Apts











Wadleigh Road Apts

Wadleigh Rd. Rochester, NH 03839

Rendering





1 Site Section 1" = 20'-0"





2 1" = 2







Wadleigh Road Apts





3 Site Section to Tumpike 1" = 30'-0"



KEY PLAN

Wadleigh Road Apts





