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April 10, 2022

Rochester Planning Board Attn. Nel Sylvian 31 Wakefield Street Rochester, NH 03867

RE: Response Letter 19 Old Gonic Road, Rochester, NH Tax Map 131, Lot 1

JBE Project No. 21090

Dear Mr. Sylvian,

We are in receipt of comments from Renee Bourdeau, P.E. and Emma Williamson EIT of Geosyntec dated March 10, 2022 and received on March 24, 2022. We have answered as many of the comments as we could, but we have undertaken a large revision to the plan set. Upon reviewing the amount of disturbance and the amount of material to be removed from the site, it was decided to redesign the layout.

The internal loop that was previously located on the highest point of the property has been eliminated. The units located in that area have been re-positioned around the larger loop road. With this change, we removed 4 units and a large amount of impervious surface. We have also redesigned the sewer and grading. The back of some of the units on the main loop will be walkout units from the upper floor, utilizing the back of the garage as a retaining wall.

This change reduces the ledge removal on the site as well as the total disturbance. This will also leave the land behind units on the main loop as woods for greater privacy. The slope on the back of the units is shown as 2:1 slope but may be steeper depending on how the ledge face can be established and the quality of the rock. We have also reduced the impervious coverage by approximately 17,000 SF and the disturbed area by 1.3 acres based on this redesign.

#### **NARRATIVE STORMWATER MANAGEMENT REPORT:**

- 1. New Comment: The SWPPP should be provided to the city prior to the preconstruction meeting. No further response from the Applicant is required.
- 2. New Comment: The SWPPP should be provided to the city prior to the preconstruction meeting.

RESPONSE: The SWPPP will be provided prior to the pre-con meeting.

3. New Comment: No further response is needed from the applicant,

- 4. New comment: No further response is needed from the applicant
- 5. New comment: No further response is needed from the applicant
- 6. New comment: § 218-8.B(1)(g)(i)) requires a description of the procedures to limit and/or optimize use of deicing materials and minimize off-site increase in chloride levels in adjacent surface and groundwater, regardless if it is in a chloride impaired area. This information should be included in the Narrative Stormwater Management and Erosion Control Report.

RESPONSE: The use of deicing materials will be no different here than from any City owned street. This site will be private, but not treated differently due to safety of the residents and insurance reasons. We do have stormwater treatment downstream of the road network.

7. New comment: The SWPPP should be provided to the city prior to the preconstruction meeting

**RESPONSE:** The SWPPP is will be provided prior to the pre-con meeting.

8. New comment: Copies of pertinent state permits should be provided to the city prior to the preconstruction meeting

RESPONSE: Copies of the State Permits will be provided once received.

#### SITE DEVELOPMENT PLAN REQUIREMENTS:

- 1. New comment: No further response is needed from the applicant
- 2. New comment: No further response is needed from the applicant
- 3. New comment: No further response is needed from the applicant
- 4. New comment: No further response is needed from the applicant
- 5. New comment: No further response from the applicant is needed regarding the locations of earth stockpiles, perimeters controls, construction sites entrances, stone check dams, and other erosion controls. The temporary sediment basin locations should be provided in the SWPPP and provided to the city prior to the preconstruction meeting.

RESPONSE: Temporary sediment basins will be added to the SWPPP plans.

6. New comment: The SWPPP should be provided to the city prior to the preconstruction meeting.

**RESPONSE:** The SWPPP will be provided prior to the pre-con meeting.

7. New comment: The SWPPP should be provided to the city prior to the preconstruction meeting.

RESPONSE: The SWPPP will be provided prior to the pre-con meeting.

8. New comment: The SWPPP should be provided to the city prior to the preconstruction meeting.

**RESPONSE:** The SWPPP will be provided prior to the pre-con meeting.



#### **TEMPORARY CONSTRUCTION STORMWATER DESIGN STANDARDS:**

- 1. New comment: No further response is needed from applicant.
- 2. New comment: The SWPPP should be provided to the city prior to the preconstruction meeting.

**RESPONSE:** The SWPPP will be provided prior to the pre-con meeting.

#### POST-CONSTRUCTION STOMWATER MANAGEMENT STANDARDS:

1. New comment: The Applicant has provided a waiver request from § 218-10 C(2), which are the groundwater recharge requirements. The Applicant has not requested a waiver from the site runoff volume requirements in § 218-10 C(3). If the Applicant is requesting a waiver from this section, the waiver request should be amended.

Additionally, as stated in § 218-10 C(3)(c), "if an increase in post-development peak rate or volume is anticipated due to site constraints that limit the ability to implement LID measures, the applicant shall demonstrate that the project will not cause adverse impacts to downstream properties, infrastructure, aquatic habitat or water quality degradation in downstream water bodies."

The Applicant currently makes a statement in only the waiver request as to the site constraints that limit the ability to meet the requirement. However, the Applicant has not demonstrated with supporting calculations to that the project will not cause adverse impacts to downstream properties, infrastructure, aquatic habitat or water quality degradation in downstream water bodies.

The Applicant should provide the calculations and supporting information before the Planning Board approves a Waiver Request

RESPONSE: Due to the size of the re-design and change to the site plan, we do not have a completed Drainage Analysis yet. We will have this in the next couple of weeks and will be submit that along with this amended waiver. It is typical that we cannot infiltrate into soils with HSG C or D, due to their saturation rate. That is the reason that NHDES Alteration of Terrain Bureau routinely waives these requirements when the soils are similar to the ones we have onsite.

- 2. New comment: No further response is needed from applicant.
- 3. New comment: The SWPPP should be provided to the city prior to the preconstruction meeting.

**RESPONSE:** The SWPPP will be provided prior to the pre-con meeting.

# STORMWATER MANAGEMENT DESIGN STANDARDS FOR NEW DEVELOPMENT:

1. New comment: The Applicant must demonstrate that the BMPs selected with achieve 50% removal of both total phosphorus and total nitrogen. The Applicant selected wet ponds. Wet ponds are only capable of removing 40% nitrogen load if designed treat 2-inches of runoff (Figure 3-18, Appendix F of MS4 Permit). The Applicant provided calculations for 0.90 inches of runoff which is sufficient for total phosphorus load. The Applicant should select a range of BMPs that are capable of achieve a 50% reduce in nitrogen



## RESPONSE: This will be addressed in the amended Drainage Analysis.

2. New comment: The Applicant has not provided a summary table indicating the total required Water Quality Volume for the site and how the proposed practices meet the proposed total volume. The Applicant should also distinguish between Analysis Points. The Applicant should provide a summary table in the Drainage Report to allow the city to easily review this information

RESPONSE: This will be addressed in the amended Drainage Analysis.

3. New comment: The Applicant has provided a waiver request from this section and indicates "we are unable to reduce the volume of stormwater to meet the level in pre-existing conditions". The Applicant has not included calculations demonstrating what the required Groundwater Recharge Volume is for the soil type on site and how much recharge to groundwater the Applicant is providing (if any). Further, in accordance with § 218-10.C(2)(b), if infiltration potential is limited or not practical, the Applicant must demonstrate that the stormwater volume from the site will not cause adverse impacts to downstream properties, infrastructure, aquatic habitat, or water quality degradation in downstream water bodies. The Applicant currently makes a statement that there would not be adverse impacts; however, there are no supporting calculations to demonstrate how this conclusion was made.

RESPONSE: This will be addressed in the amended Drainage Analysis.

4. New comment: See response to comment IV.1 above. The Applicant has provided a waiver request from § 218-10 C(2), which are the groundwater recharge requirements. The Applicant has not requested a waiver from the site runoff volume requirements in § 218-10 C(3). If the Applicant is requesting a waiver from this section, the waiver request should be amended.

Additionally, as stated in § 218-10 C(3)(c), "if an increase in post-development peak rate or volume is anticipated due to site constraints that limit the ability to implement LID measures, the applicant shall demonstrate that the project will not cause adverse impacts to downstream properties, infrastructure, aquatic habitat or water quality degradation in downstream water bodies."

The Applicant currently makes a statement in only the waiver request as to the site constraints that limit the ability to meet the requirement. However, the Applicant has not demonstrated with supporting calculations to that the project will not cause adverse impacts to downstream properties, infrastructure, aquatic habitat or water quality degradation in downstream water bodies.

The Applicant should provide the calculations and supporting information before the Planning Board approves a Waiver Request.

RESPONSE: This will be addressed in the amended Drainage Analysis.

#### STORMWATER DRAINAGE SYSTEM SPECIFICATIONS:

- 1. New comment: No further response is needed from the applicant.
- 2. New comment: Similar to comment IV.1 above, the Applicant has not demonstrated that the volume discharged from the site from the proposed wet ponds during the 25-year storm will not cause adverse off-site impacts.

RESPONSE: This will be addressed in the amended Drainage Analysis.



3. New comment: Based on the information provided, multiple drainpipes from the catch basins have velocities greater than 2 feet per second

RESPONSE: This will be addressed in the amended Drainage Analysis.

4. New comment: The Applicant should summarize the required velocities in a summary table or in a table on the detail sheet. The velocities entering the proposed swales are not provided within the Drainage Report, based on how the swales were modeled. The swales should be modeled as reaches. The maximum velocities within the swales modeled within the subcatchments all exceed I foot per second.

RESPONSE: This will be addressed in the amended Drainage Analysis.

#### POST- CONSTRUCTION INSPECTION MAINTENANCE AGREEMENT:

- 1. The Inspection and Maintenance Plan should include the following:
  - a. New comment: The Inspection and Maintenance Plan is applicable to the stormwater management features at the property. Based on the response from the Applicant, can additional information be provided how the rental unit occupants are supposed to know how to maintain the stormwater management features and provide sufficient funding for these features. This does not seem like a long-term Inspection and Maintenance Plan that will be successful. The Owner of the property should hold this responsibility. The Applicant should provide clarification.

RESPONSE: This will be addressed in the amended Drainage Analysis.

- b. New comment: No further response is needed from the applicant.
- c. New comment: No further response is needed from the applicant.
- d. New comment: The Inspection and Maintenance report should require that documentation be provided (e.g., photos) of any required maintenance. The I&M document should include a map of all BMPs with a numbering system (e.g., CB1, CB2, Wet Pond 1, Wet Pond 2, etc.) for clarity.

RESPONSE: This will be addressed in the amended Drainage Analysis.

- e. New comment: No further response is needed from the applicant.
- f. New comment: The sample deicing log was not included in the I&M document RESPONSE: This will be addressed in the amended Drainage Analysis.
  - g. New comment: No further response is needed from the applicant.
  - h. New comment: No further response is needed from the applicant.

#### **OTHER COMMENTS:**

1. New comment: No further response is needed from the applicant.



2. New comment: As currently designed the wet ponds have a 4-foot permanent pool. Wet ponds are typically considered unsuitable for residential areas due to the safety risk when they do not have a fence surrounding them. Based on review of the plans, it does not appear that any fencing is proposed around the ponds. A 10-foot safety bench is recommended around wet ponds. Currently the design does not incorporate a safety bench on the wet ponds.

RESPONSE: We will incorporate the bench and a fence if necessary. We typically find that fence becomes a maintenance headache, doesn't prevent access to most children and we aren't fencing the entire river bank area that they would also have access to. Therefore, we would prefer to not fence these ponds, but leave it up to the City to decide.

- 3. No further response is needed from the applicant.
- 4. New comment: No further response is needed from the applicant.
- 5. New comment: No further response is needed from the applicant.
- 6. New comment: The hood is shown on the Catch Basin Detail drawing; however, the treatment rates provided by the catch basins are not included in the Drainage Report. RESPONSE: This will be addressed in the amended Drainage Analysis.
- 7. New comment: No further response is needed from the applicant.
- 8. New comment: No further response is needed from the applicant.
- 9. New comment: No further response is needed from the applicant.
- 10. New comment: No further response is needed from the applicant.
- 11. The following comments are specific to the HydroCAD Report and Watershed Plans:
  - a. New comment: No further response is needed from the applicant.
  - b. New comment: The Applicant has not provided a summary table for the volume for each of the storm events. This information should be summarized in the Drainage Report, in the executive summary so the city can easily make this determination.

RESPONSE: This will be addressed in the amended Drainage Analysis.

- c. New comment: No further response is needed from the applicant.
- d. The height of the vertical grate/orifice opening on the outlet structure for Wet Pond 1 in the HydroCAD model says 10"; however, the detail table shows a change in elevation equal to over 13". The Applicant should reconcile these values.

RESPONSE: This will be addressed in the amended Drainage Analysis.

e. The applicant has requested to provide the following information in the SWPPP prior to the preconstruction meeting as an alternative to providing the information in the



application and response letter. The Planning Board should include this information as a condition if the application is approved.

- i. Anticipated project start and completion dates, and duration of grading and construction activities.
- ii. Documentation on what LID site planning and design strategies were used on-site or why using LID strategies are not feasible, as required under § 218-8.B(1)(d)
- iii. Description of the procedures to control waste, such as discarded building materials, construction debris, sanitary waste, concrete washout, chemicals, and litter.
- iv. Locations of temporary sediment basons
- v. Locations of equipment storage and staging areas and control procedures
- vi. Locations of vehicles fueling areas or equipment fueling areas and control procedures
- vii. Location of disposal facilities for solid waste, construction debris, sanitary waste, concrete washout, and plan for stump disposal and control procedures.
- viii. Location and description of proposed deicing material storage areas.

RESPONSE: This will be addressed in the amended Drainage Analysis.

Included with this response letter are the following:

- 1. Three (3) Full Size Plan Sets.
- 2. Sixteen (16) 11x17 Plan Sets (Folded).
- 3. Stephen Pernaw's Response to Sebago Technic's Memorandum
- 4. Jones and Beach Engineer Response to Sebago Technic's Memorandum

Thank you very much for your time.

Ver truly yours,

JONES & BEACH ENGINEERS, INC.

Joseph Coronati Vice President

cc: Green & Company (via email)

John O'Neil (via email)

Derek Caldwell, PE (via email)

Renee Bourdeau, PE (via email)





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VIA EMAIL

March 10, 2022

Dana Webber Assistant City Engineer City of Rochester 45 Old Dover Road Rochester, NH 03867-3445

Subject: Second Letter for Third Party Peer Review of Old Gonic Road Townhouses at

19 Old Gonic Road

#### Dear Dana:

As requested by the City of Rochester (City), Geosyntec Consultants, Inc. (Geosyntec) has reviewed the letter from Jones & Beach Engineers, Inc., the Applicant's engineer, dated February 15, 2022, in response to Geosyntec's first peer review letter for 19 Old Gonic Road in Rochester, New Hampshire (Site). Geosyntec has reviewed the following additional documents, prepared by Jones & Beach Engineers, Inc., in preparation of this second letter:

- Response Letter for 19 Old Gonic Road dated February 15, 2022 (8 pages)
- Waiver Request for Bayberry Common, Dated February 15, 2022 (1 page)
- Drainage Analysis, Sediment and Erosion Control Plan, Old Gonic Road Townhouses, dated November 23, 2021, revised February 15, 2022 (131 pages, including appendices)
- Memorandum Re: Old Gonic Road Sewer Capacity, prepared by Weston & Sampson, dated February 11, 2022 (3 pages)
- Proposed Site Plan, Old Gonic Road Townhouses, Tax Map 131, Lot 10, 19 Old Gonic Road, Rochester, NH, dated November 23, 2021, revised February 14, 2022 (47 sheets)

Based on the review of the above documents and the requirements outlined in Chapter 218, Geosyntec has the following comments for the Applicant. The normal text is Geosyntec's initial review comments, the *italicized* text is Jones & Beach Engineers' response, and the **bold** text is Geosyntec's response to Jones & Beach Engineers response.

#### I. Narrative Stormwater Management and Erosion Control Report

The Drainage Analysis Report provided was reviewed to ensure compliance with the Stormwater Management and Erosion Control Report (Report) requirements in § 218-8.B(1). The following comments should be addressed by the Applicant.

1. Anticipated project start and completion dates, and duration of grading and construction activities are not provided.

Applicant Response: This section 218-8 B of the Stormwater Management & Erosion Control allows for sites that require SWPPPs to have the SMECP requirements added into that document. We would like to request that we do this for this development. This information will be provided as part of EPA SWPPP documents as they will outline all of this information. The total length of construction will depend on market conditions and phasing.

# The SWPPP should be provided to the city prior to the preconstruction meeting. No further response from the Applicant required.

2. Documentation on what LID site planning and design strategies were used on-site or why using LID strategies are not feasible, as required under § 218-8.B(1)(d) is not provided.

Applicant Response: This section 218-8 B of the Stormwater Management & Erosion Control allows for sites that require SWPPPs to have the SMECP requirements added into that document. We would like to request that we do this for this development. We are utilizing wet ponds, swales, sediment forebays, catch basins with sumps and hoods and curbing.

### The SWPPP should be provided to the city prior to the preconstruction meeting.

3. Description of the proposed changes in impervious cover is not provided. However, the proposed impervious cover is included in the HydroCAD outputs.

Applicant Response: The total amount of impervious cover in existing and proposed conditions is listed in the drainage report as requested.

#### No further response is needed from the applicant.

4. Description of the calculations to demonstrate how the proposed project meets construction site erosion control standards are not provided.

Applicant Response: Rip rap sizing calculations have been provided in the drainage report. Sediment forebay sizing information is part of the Alteration of Terrain Permit application along with the BMP worksheets.

#### No further response is needed from the applicant.

5. Description of the calculations to demonstrate how the proposed project meets post-construction stormwater management design standards are not provided.

Applicant Response: The Drainage Analysis and plan set provide the information to see that the stormwater management standards have been met.

No further response is needed from the applicant.

> Description of the procedures to limit and/or optimize use of deicing materials and minimize off-site increases in chloride levels in adjacent surface and groundwater is not provided.

Applicant Response: This site is not located in a Chloride Impaired area and typically NHDES AOT does not require salt minimization plans for these sites. All of our stormwater treatment is downstream of the road network and the stormwater gets treated per AOT regulations prior to release.

§ 218-8.B(1)(g)(i)) requires a description of the procedures to limit and/or optimize use of deicing materials and minimize off-site increase in chloride levels in adjacent surface and groundwater, regardless if it is in a chloride impaired area. This information should be included in the Narrative Stormwater Management and Erosion Control Report.

7. Description of the procedures to control waste such as discarded building materials, construction debris, sanitary waste, concrete washout, chemicals, litter are not provided, with the exception of Site Notes #9 on drawing no. OVRS, which states that trash is to be handled with totes at each unit.

Applicant Response: The above will be addressed in the SWPPP Plan will be provided by the contractor prior to construction.

The SWPPP should be provided to the city prior to the preconstruction meeting.

8. Copies of pertinent state permits (AoT and wetlands), if applicable, are not provided.

Applicant Response: Copies of State permits will be provided when received.

Copies of pertinent state permits should be provided to the city prior to the preconstruction meeting.

#### II. Site Development Plan Requirements

The design was reviewed to ensure compliance with the requirements in § 218-8.B. The following comments should be addressed by the Applicant.

1. Drainage patterns and direction of flow of stormwater runoff using arrows 200-feet outside of the project boundary were not provided for the existing or proposed conditions on the site plans or watershed plans.

Applicant Response: We did not see this requirement in the site plan regulations, but we have added flow arrows on the watershed plans.

No further response from the applicant is needed.

2. The type of existing vegetation (including invasive species) is not shown (tree lines, trees and bushes, and wetland delineations are shown).

Applicant Response: The types of vegetation are called out on the plans; the woods are mixed growth and we have not found any invasive species to date.

No further response from the applicant is needed.

3. A limit of earth disturbance is not shown on the site plans.

Applicant Response: The limit of the earth disturbance is now shown on plan OVRG.

No further response from the applicant is needed.

4. A cut and fill plan is not provided.

Applicant Response: A plan has been added at the end of the set to show the areas of cut and fill.

No further response from the applicant is needed.

An Erosion and Sediment Control Plan is not provided to show the locations of earth stockpiles, perimeter controls, construction site entrances, temporary sediment basin, stone check dam, temporary culvert inlet protection check dam and any other erosion controls specified.

Applicant Response: All of this information is located on plans C9-C11 except temporary sediment basins. Those locations are determined by the site contractor and inspected as part of the SWPPP, and this site will have an Environmental Monitor as required by AOT as well.

No further response from the applicant is needed regarding the locations of earth stockpiles, perimeters controls, construction sites entrances, stone check dams, and other erosion controls.

The temporary sediment basin locations should be provided in the SWPPP and provided to the city prior to the preconstruction meeting.

6. Location of equipment storage and staging areas are not shown. Procedures should be added to the Drainage Analysis Report to reflect the added controls.

Applicant Response: The above will be addressed in the SWPPP Plan will be provided by the contractor prior to construction.

The SWPPP should be provided to the city prior to the preconstruction meeting.

7. Location of vehicle fueling areas or equipment fueling areas are not shown. Procedures should be added to the Drainage Analysis Report to reflect the added controls.

Applicant Response: The above will be addressed in the SWPPP Plan will be provided by the contractor prior to construction.

#### The SWPPP should be provided to the city prior to the preconstruction meeting.

8. Location of disposal facilities for solid waste, construction debris, sanitary waste, concrete washout, and plan for stump disposal (if applicable) are not shown.

Applicant Response: The above will be addressed in the SWPPP Plan will be provided by the contractor prior to construction.

#### The SWPPP should be provided to the city prior to the preconstruction meeting.

#### III. Temporary Construction Stormwater Management Design Standards

The design was reviewed to ensure compliance with the requirements in § 218-9.A. The following comments should be addressed by the Applicant.

1. Stabilization notes on the site plans and within the Drainage Analysis Report should be updated to reflect the requirements under § 218-9.A(8)(a), which state that temporary stabilization measures should be in place within 5 calendar days for exposed soil areas that are within 100-feeet of a surface water body or a wetland.

Applicant Response: This note has been added to our stabilization notes on Sheet E1.

#### No further response is needed from applicant.

Procedures to control waste such as discarded building materials, concrete truck washout, chemicals, litter, and sanitary waste during the construction process that may cause adverse impacts to water quality are not provided.

Applicant Response: The above will be addressed in the SWPPP Plan will be provided by the contractor prior to construction.

#### The SWPPP should be provided to the city prior to the preconstruction meeting.

#### IV. Post-Construction Stormwater Management Design Standards

The design was reviewed to ensure compliance with the requirements in § 218-10. The following comments should be addressed by the Applicant.

1. Calculations are not provided that demonstrate that stormwater discharge from the proposed stormwater drainage system will not cause flooding or functional impairments to streets, adjacent properties, downstream properties, soils, or vegetation. Calculations show that the peak discharge for post-development does not exceed the pre-development discharge; however, calculations are not provided that demonstrate that the post-development runoff volume does not exceed the pre-development volume.

Applicant Response: Due to the soils onsite, infiltration of stormwater is not possible, therefore we are requesting a waiver to this requirement. We will also be requesting the

same waiver from the AOT regulations, which is typically granted when in Hydrologic Soil Group C or worse.

The Applicant has provided a waiver request from § 218-10 C(2), which are the groundwater recharge requirements. The Applicant has not requested a waiver from the site runoff volume requirements in § 218-10 C(3). If the Applicant is requesting a waiver from this section, the waiver request should be amended.

Additionally, as stated in § 218-10 C(3)(c), "if an increase in post-development peak rate or volume is anticipated due to site constraints that limit the ability to implement LID measures, the applicant shall demonstrate that the project will not cause adverse impacts to downstream properties, infrastructure, aquatic habitat or water quality degradation in downstream water bodies."

The Applicant currently makes a statement in only the waiver request as to the site constraints that limit the ability to meet the requirement. However, the Applicant has not demonstrated with supporting calculations to that the project will not cause adverse impacts to downstream properties, infrastructure, aquatic habitat or water quality degradation in downstream water bodies.

The Applicant should provide the calculations and supporting information before the Planning Board approves a Waiver Request.

Provide a specific planting plan for the bioretention systems. Native plants should be
proposed in a density sufficient to prevent surface erosion and to achieve water quality
treatment requirements. Also, an alternative to bark or wood fiber mulch should be
considered as this tends to float, does not reduce erosion at the inlet, and clogs overflow
structures.

Applicant Response: The Bioretention Ponds have been removed from the plans and replaced with Wet Ponds. No plantings are proposed.

No further response is needed from applicant.

3. Proposed deicing material storage areas are not described or shown on the site plans.

Applicant Response: The above will be addressed in the SWPPP Plan will be provided by the contractor prior to construction. We do not anticipate the large storage of deicing material onsite. Typically, the plow trucks will sand and salt as they remove snow.

The SWPPP should be provided to the city prior to the preconstruction meeting.

#### V. Stormwater Management Design Standards for New Development

The design was reviewed to ensure compliance with the requirements in § 218-10.C. The following comments should be addressed by the Applicant.

1. Calculations are not provided to demonstrate that the total post-construction impervious area is treated to remove at least 80% total suspended solids and 50% removal of total phosphorus and total nitrogen, as required under § 218-10.C(1)(a). The Applicant should provide calculations that are consistent with the methods referenced in § 218-10.A(3)(a,b).

Applicant Response: The calculations are provided within the Drainage report.

The Applicant must demonstrate that the BMPs selected with achieve 50% removal of both total phosphorus and total nitrogen. The Applicant selected wet ponds. Wet ponds are only capable of removing 40% nitrogen load if designed treat 2-inches of runoff (Figure 3-18, Appendix F of MS4 Permit). The Applicant provided calculations for 0.90 inches of runoff which is sufficient for total phosphorus load. The Applicant should select a range of BMPs that are capable of achieve a 50% reduce in nitrogen.

2. Calculations are not provided to demonstrate that the stormwater treatment practices have been designed for the water quality volume or water quality flow, in accordance with Env-Wq 1504.10 and Env-Wq 1504.11, respectively, as required under § 218-10.C(1)(c).

Applicant Response: BMP worksheets demonstrating these standards are being met are included within the Drainage Report.

The Applicant has not provided a summary table indicating the total required Water Quality Volume for the site and how the proposed practices meet the proposed total volume. The Applicant should also distinguish between Analysis Points. The Applicant should provide a summary table in the Drainage Report to allow the city to easily review this information.

3. Calculations are not provided to demonstrate protection of groundwater resources by reducing the post-development stormwater runoff volume by infiltrating Groundwater Recharge Volume as required under § 218-10.C(2)(a,b).

Applicant Response: Due to the soils onsite, infiltration of stormwater is not possible, therefore we are requesting a waiver to this requirement. We will also be requesting the same waiver from the AOT regulations, which is typically granted when in Hydrologic Soil Group C or worse.

The Applicant has provided a waiver request from this section and indicates "we are unable to reduce the volume of stormwater to meet the level in pre-existing conditions". The Applicant has not included calculations demonstrating what the required Groundwater Recharge Volume is for the soil type on site and how much recharge to groundwater the Applicant is providing (if any). Further, in accordance with § 218-10.C(2)(b), if infiltration potential is limited or not practical, the Applicant must demonstrate that the stormwater volume from the site will not cause adverse impacts to downstream properties, infrastructure, aquatic habitat, or water quality degradation in downstream water bodies. The Applicant currently makes a statement that there would not be adverse impacts; however, there are no supporting calculations to demonstrate how this conclusion was made.

The Applicant should provide the calculations and supporting information before the Planning Board approves the Waiver Request.

4. Calculations are not provided to demonstrate that the post-development stormwater runoff volumes do not exceed the pre-development stormwater runoff volumes for the 2-year, 10-year, and 25-year, 24-hour design storm events, as required under § 218-10.C(3)(a).

Applicant Response: Due to the soils onsite, infiltration of stormwater is not possible, therefore we are requesting a waiver to this requirement. We will also be requesting the same waiver from the AOT regulations, which is typically granted when in Hydrologic Soil Group C or worse.

See response to comment IV.1 above.

#### VI. Stormwater Drainage System Specifications

The design was reviewed to ensure compliance with the requirements in § 218-10.F. The following comments should be addressed by the Applicant.

1. Calculations are not provided to demonstrate that the closed drainage system was sized for the 25-year, 24-hour storm event, as required under § 218-10.F(2)(a).

Applicant Response: The 25-year storm event is included within the calculations.

No further response is needed from the applicant.

2. Calculations are not provided for the 25-year, 24-hour storm to evaluate the potential for off-site effects, as if the project drainage flows to an existing roadway culvert or if a detention or retention area is proposed.

Applicant Response: We are proposing three separate Wet Ponds to mitigate peak discharge rates. The Drainage Report details the Wet Pond designs.

Similar to comment IV.1 above, the Applicant has not demonstrated that the volume discharged from the site from the proposed wet ponds during the 25-year storm will not cause adverse off-site impacts.

3. Calculations are not provided to demonstrate that the closed drainage network has a minimum velocity of 2 feet per second, as required under § 218-10.F(2)(d).

Applicant Response: These calculations are included within the Drainage Report.

Based on the information provided, multiple drainpipes from the catch basins have velocities greater than 2 feet per second.

4. Calculations are not provided to demonstration that velocities entering the proposed swales are less than 10 feet per second and that the maximum velocity within the swale

is 1 foot per second during the 25-year, 24-hour storm event, as required under § 218-10.F(2)(c).

Applicant Response: These calculations are included within the Drainage Report.

The Applicant should summarize the required velocities in a summary table or in a table on the detail sheet. The velocities entering the proposed swales are not provided within the Drainage Report, based on how the swales were modeled. The swales should be modeled as reaches. The maximum velocities within the swales modeled within the subcatchments all exceed 1 foot per second.

#### VII. Post-Construction Inspection and Maintenance Agreement

The design was reviewed to ensure compliance with the requirements in § 218-11.C. The following comments should be addressed by the Applicant.

- 1. The Inspection and Maintenance Plan should include the following:
  - a) The name of the responsible party for inspections and maintenance,

Applicant Response: The units are proposed as rental units and all maintenance will be the responsibility of the owners. Typically, AOT requires that projects of this side have annual maintenance inspection performed by a third-party inspector.

The Inspection and Maintenance Plan is applicable to the stormwater management features at the property. Based on the response from the Applicant, can additional information be provided how the rental unit occupants are supposed to know how to maintain the stormwater management features and provide sufficient funding for these features. This does not seem like a long-term Inspection and Maintenance Plan that will be successful. The Owner of the property should hold this responsibility. The Applicant should provide clarification.

b) All of the proposed stormwater practices including but not limited to bioretention ponds, drip edges, riprap inlet and outlet protection, catch basins, and the closed drainage network.

Applicant Response: The I&M document discusses these best management practices.

No further response is needed from the applicant.

c) A proposed schedule of inspection frequency,

Applicant Response: We are proposed annual inspections. A checklist is provided in the I&M manual.

No further response is needed from the applicant.

d) A plan identifying each BMP and associated details, an inspection checklist and photo documentation requirements,

Applicant Response: A BMP plan has been added to the I&M document.

The Inspection and Maintenance report should require that documentation be provided (e.g., photos) of any required maintenance. The I&M document should include a map of all BMPs with a numbering system (e.g., CB1, CB2, Wet Pond 1, Wet Pond 2, etc.) for clarity.

e) Sample log to document each inspection and maintenance activity,

Applicant Response: This has been added to the I&M document.

No further response is required from the applicant.

f) Sample deicing log to track amount and type of deicing materials applied to the site,

Applicant Response: This has been added to the I&M document.

The sample deicing log was not included in the I&M document.

g) Description of maintenance response actions, including actions to be taking if invasive species begin to grow in stormwater practices, and

Applicant Response: We have added the information provided in the Stormwater Management and Erosion Control Chapter 218 into the I&M document.

No further response is required from the applicant.

h) Documentation of how reports will be completed, submittal and retention procedures, and contingency plans if future maintenance is required.

Applicant Response: This information is provided in the I&M document and will be handled on a case by case depending on the situation and we will make reports available upon request to the DPW.

No further response is required from the applicant.

#### VIII. Other Comments

1. The Grading and Drainage Plans reference "ponds"; however, the detail sheet provides a detail for bioretention. The details or Grading and Drainage Plans should identify these features with the same terminology.

Applicant Response: The previously proposed Bioretention Ponds have been revised to be Wet Ponds. The Detail Sheets have been revised with the correct construction detail and notes have been changes within the plan set.

#### No further response is required from the applicant.

 Bioretention systems with an underdrain are not recommended as an appropriate stormwater practice for peak runoff control in accordance with Env-WQ 1507.06.
 Bioretention systems are appropriate for pollutant removal and to protect water quality. An alternative BMP should be considered for peak runoff control.

Applicant Response: The previously proposed Bioretention Ponds have been revised to be Wet Ponds. The Detail Sheets have been revised with the correct construction detail and notes have been changes within the plan set.

As currently designed the wet ponds have a 4-foot permanent pool. Wet ponds are typically considered unsuitable for residential areas due to the safety risk when they do not have a fence surrounding them. Based on review of the plans, it does not appear that any fencing is proposed around the ponds.

A 10-foot safety bench is recommended around wet ponds. Currently the design does not incorporate a safety bench on the wet ponds.

3. Proposed underdrains for the bioretention systems are not shown on the site plans.

Applicant Response: See above reply.

#### No further response is required from the applicant.

4. The Applicant should clearly mark existing trees to remain on the Landscape Plan on drawing no. L1 (Landscape Notes #14) or on an alternate plan.

Applicant Response: Additional wordage has been added to the note that tree shall be clearly marked prior to land clearing activities.

#### No further response is needed from the applicant.

Note #14 on drawing no. P1 states "All driveways to have culverts unless approved by the town road agent." However, culverts are not shown, nor are drainage calculations or culvert specifications provided.

Applicant Response: There are no driveway culverts proposed. This note has been removed.

#### No further response is required from the applicant.

6. Section 4.4 of the Drainage Analysis Sediment and Erosion Control Plan states that "Treatment is obtained through the use of deep sump hooded catch basins [...]", but does

not provide the treatment rates obtained by the catch basins. Additionally, the hood is not included on the catch basin detail on drawing no. D2.

Applicant Response: A hood has been added to the Catch Basin Detail. Treatment provided by the catch basins is included in the Drainage Report.

The hood is shown on the Catch Basin Detail drawing; however, the treatment rates provided by the catch basins are not included in the Drainage Report.

7. Snow storage areas are proposed in areas where stormwater runoff is managed (swales, inlets). This will impede the ability for stormwater to flow during rain events and cause localized flooding. Alternative locations for snow storage should be selected.

Applicant Response: We have reviewed the snow storage areas and removed any areas encroaching on inlets or swales.

No further response is needed from the applicant.

8. Details for proposed swales, including landscaping details are not provided.

Applicant Response: All swales will be grassed. A Detail has been included in the Plan Set.

No further response is needed from the applicant.

9. Outlet protection/rip-rap sizing calculations are not provided.

Applicant Response: Riprap sizing is now included in the Drainage Report.

No further response is needed from the applicant.

10. In the areas where the parking area runoff flows off of the pavement and onto vegetation prior to entering the proposed swale (near proposed buildings 103-114 and 91-102) calculations are not provided to demonstrate that the vegetation can withstand the velocities without causing erosion.

Applicant Response: A riprap apron has been added at the end of the parking lots in the areas mentioned to reduce any erosion caused by stormwater runoff.

No further response is needed from the applicant.

- 11. The following comments are specific to the HydroCAD Report and Watershed Plans:
  - i. The complete (not summary) HydroCAD outputs should be included for the 25-year, 24-hour storm, as opposed to the 10-year, 24-hour storm which was provided.

Applicant Response: The complete summary of the 25-year storm is included.

No further response is needed from the applicant.

ii. Analysis Point #5 appears to be off-site. Provide calculations to demonstrate that the existing infrastructure is sufficient to handle the additional flow from the development.

Applicant Response: There will not be any additional flow to Analysis Point #5 as the HydroCAD output shows reductions in both the peak flow and volume for all analyzed events.

The Applicant has not provided a summary table for the volume for each of the storm events. This information should be summarized in the Drainage Report, in the executive summary so the city can easily make this determination.

iii. The proposed vegetation should be modeled in the ponded area of the proposed bioretention and not treated as 100% void space to ensure that with mature vegetation these features have sufficient capacity to convey the post-development peak discharge and volume.

Applicant Response: Bioretention areas have been eliminated from the plans.

No further response is needed from the applicant.

- iv. The height of the vertical grate/orifice opening on the outlet structure for Wet Pond 1 in the HydroCAD model says 10"; however, the detail table shows a change in elevation equal to over 13". The Applicant should reconcile these values.
- v. The applicant has requested to provide the following information in the SWPPP prior to the preconstruction meeting as an alternative to providing the information in the application and response letter. The Planning Board should include this information as a condition if the application is approved.
  - a. Anticipated project start and completion dates, and duration of grading and construction activities.
  - b. Documentation on what LID site planning and design strategies were used on-site or why using LID strategies are not feasible, as required under § 218-8.B(1)(d)
  - c. Description of the procedures to control waste, such as discarded building materials, construction debris, sanitary waste, concrete washout, chemicals, and litter.
  - d. Locations of temporary sediment basins.
  - e. Location of equipment storage and staging areas and control procedures.
  - f. Location of vehicle fueling areas or equipment fueling areas and control procedures.

- g. Location of disposal facilities for solid waste, construction debris, sanitary waste, concrete washout, and plan for stump disposal and control procedures.
- h. Location and description of proposed deicing material storage areas.

Should the City or the Applicant have any questions or comments, please feel free to contact me at <a href="mailto:rbourdeau@geosyntec.com">rbourdeau@geosyntec.com</a> or at (518) 593-5406.

Sincerely,

Renee L. Bourdeau, P.E. Senior Water Resources Engineer

Reneif Bowdence

Emma Williamson, EIT Senior Staff Engineer

Emma Williamson



85 Portsmouth Avenue, PO Box 219, Stratham, NH 03885 603.772.4746 - JonesandBeach.com

April 10, 2022

Rochester Planning Board Attn. Nel Sylvian 31 Wakefield Street Rochester, NH 03867

**RE:** Response Letter

19 Old Gonic Road, Rochester, NH

Tax Map 131, Lot 1 JBE Project No. 21090

Dear Mr. Sylvian,

We are in receipt of comments from Derek Caldwell at Sebago Technics dated March 11, 2022. Review comments are listed below with our responses in bold. Stephen G. Pernaw & Company are responding to the traffic comments separately.

#### Site Plan:

6. General - The TIA makes mention that the Old Gonic Road access will be gated and limited to site departures. The submitted site plan does not appear to show any proposed gate. Has it been considered to limit the Old Gonic Road entrance to emergency access only, requiring all project traffic to use Emerson Avenue?

RESPONSE: The Old Gonic Road access will be one-way and limited to exits only. We have moved "One Way Do Not Enter" signage to the corner of Old Gonic Road and State Street to warn drivers of this condition. Additionally, the pavement along Old Gonic Road and at the Old Gonic site exit has been reduced to 18' wide to discourage two-way traffic.

- 7. General It is recommended to provide a pedestrian safety analysis of the existing surrounding roadways and potential for connections other than the proposed Emerson Avenue sidewalk. Old Gonic Road may be a walking route and does not have sidewalks currently. **RESPONSE: This will be addressed in a separate pedestrian study, currently underway.**
- 8. Sheet OFF2/3/4- The project proposes to construct a new sidewalk along the westerly side of Emerson Avenue connecting the development with existing sidewalk on Brock Street. Further detail should be provided for the proposed "handicap tipdown(s)" to ensure compliance with ADA standards and the NHDOT Sidewalk Details. Special attention should be made to how the proposed sidewalk will interface with the existing sidewalk/curb ramp at the intersection of Emerson Avenue and Brock Street.

RESPONSE: A handicap ramp detail showing concrete ramps is on Sheet D1 of the Plan Set. We plan to utilize the existing ramp at the intersection of Emerson Avenue and Brock Street. The proposed sidewalk will ramp down to the existing truncated dome area.

W:\21090 - ROCHESTER - 19 OLD GONIC RD - SITE - GREEN\WORD FILES\Response Letter 3 -Sebago.docx

9. Sheet OFF 3- We agree that rather than a full auxiliary left turn lane a widened bypass shoulder would be appropriate at the intersection of Brock Street and Emerson Street. It is recommended to increase the shoulder width to 11' to provide an additional 1' offset from curb. **RESPONSE:** The shoulder width has been increased to 11-feet on the attached plans.

10. Sheet OFF3 — It is recommended to revise the Shoulder Widening Typical Section detail to have the full depth pavement structure extend to the existing edge of travel way and both the crushed gravel and gravel extend to the existing edge of pavement.

RESPONSE: The detail has been revised as suggested.

11. Sheet OFF3 — Overall further detail is required of the design of the shoulder widening. This would include items such as any modifications to pavement markings, how the proposed widening will interface with the existing residential driveways and detail to show any required modifications to the existing closed drainage system. Full grading design with cut/fill limits will need to be understood to evaluate any impacts to adjacent properties.

RESPONSE: A 20 scale detail of the work area has been provided to show more detail on the shoulder widening. There is not change to the existing road striping.

12. Sheet OFF3 – Applicant should coordinate with Rochester DPW on the desired pavement structure for the proposed shoulder widening.

RESPONSE: We are working with City departments on all aspects of the offsite improvements.

Included with this response letter are the following:

Thank you very much for your time.

Very truly yours,

JONES & BEACH ENGINEERS, INC.

Joseph Coronati Vice President

> Green & Company (via email) John O'Neil (via email)



# Memorandum

#### 20540-02

To:

Dana Webber, P.E.

**Assistant City Engineer** 

City of Rochester, New Hampshire

From:

Derek Caldwell, P.E., PTOE

Sebago Technics, Inc

Date:

March 11, 2022

**Subject: Traffic Peer Review** 

19 Old Gonic Road - Residential Development

**Rochester, New Hampshire** 

3/11/2022

Sebago Technics, Inc. has completed a traffic peer review of the materials submitted by Green and Company for the proposed multifamily residential development at 19 Old Gonic Road in Rochester, New Hampshire Our review focused on the following documents:

- "Proposed Site Plan Bayberry Commons" by Jones and Beach Engineers, Inc dated April 29, 2021 with most recent revision date of January 18, 2022.
- "Traffic Impact Assessment Proposed Residential Development, Rochester, New Hampshire" by Stephen G. Pernaw & Company, Inc. dated December 21, 2021.
- Synchro v10 Traffic Analysis Models by Stephen G. Pernaw & Company, Inc.

The project proposes to construct twenty-seven separate residential buildings containing a total of 174 dwelling units. The site is currently undeveloped. Access to the site is proposed by way of extensions of Old Gonic Road and Emerson Avenue. The access via Old Gonic Road is proposed to limited to exiting traffic only. The access to Emerson Avenue will be full access, serving arriving and departing movements.

Our review evaluated the submitted materials for general conformance with the City of Rochester Site Plan Regulations, as they pertain to traffic, as well as general engineering practices. We offer the following comments.

#### Traffic Impact Assessment (TIA)

1. The TIA completed a trip generation calculation for the development using the Institute of Transportation Engineers Trip Generation Manual, 11th Edition. The calculation determined the development would generate a total of 1,192 trips on a Weekday, 77 trips in the AM Peak Hour of the adjacent street, and 95 Trips in the PM Peak Hour of the adjacent street. We are in agreement with this methodology and the calculated trip generation.

- 2. The TIA presents no-build traffic volumes for the analysis years of 2023 and 2033. The volumes are based on turning movement counts collected at the study intersections, a seasonal adjustment factor of 1.01, a 2% annual background growth factor and a "COVID-19" adjustment factor of 1.53 for the AM Peak Hour and 1.30 for the PM Peak Hour.
- 3. The study included a capacity and queueing analysis for the following intersections:
  - Brock Street at Emerson Avenue (unsignalized)
  - Brock Street at Old Gonic Road (unsignalized)
  - Brock Street at NH 125 (Columbus Avenue) (Signalized)

We are in agreement with the methodology and findings of the analysis for the two unsignalized intersections along Brock Street. As stated above, the applicant proposes to construct a widened bypass shoulder on Brock Street westbound at the intersection with Emerson Avenue to help mitigate the impact of left-turning vehicles generated by the development.

- 4. The analysis of the signalized intersection of Brock Street at NH 125 appears to have been completed using the Highway Capacity Manual (HCM) 2000 methodology within the Synchro 10 software environment. It is recommended to present revised results based on the latest HCM 6 methodology (as was done for the unsignalized intersections).
- 5. This intersection is also part of a coordinated signal system including the intersections along NH125 to the north including:
  - NH 125 at Old Dover Road
  - NH 125 at Charles Street
  - NH 125 at Lowell Street

The completed Synchro/HCM analysis modeled the intersection as actuated-uncoordinated. Additionally, the modeled signal timings and recall settings do not accurately depict the existing signal timings. It is requested the applicant revise the capacity analysis using the existing signal timings. These are provided on the attached spreadsheet for reference. The applicant may reach out to us directly for any clarification that may be needed.

It is recognized that using the existing signal timings with the presented analysis traffic volumes, which include a rather conservative Covid adjustment factor, may result in the intersection being over capacity under both no-build and build conditions. With that, we would request the revised analysis be completed using traffic volumes not adjusted by the stated covid factors

#### Site Plan

6. General - The TIA makes mention that the Old Gonic Road access will be gated and limited to site departures. The submitted site plan does not appear to show any proposed gate. Has it been considered to limit the Old Gonic Road entrance to emergency access only, requiring all project traffic to use Emerson Avenue?

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- 8. Sheet OFF2/3/4- The project proposes to construct a new sidewalk along the westerly side of Emerson Avenue connecting the development with existing sidewalk on Brock Street. Further detail should be provided for the proposed "handicap tipdown(s)" to ensure compliance with ADA standards and the NHDOT Sidewalk Details. Special attention should be made to how the proposed sidewalk will interface with the existing sidewalk/curb ramp at the intersection of Emerson Avenue and Brock Street.
- 9. Sheet OFF 3- We agree that rather than a full auxiliary left turn lane a widened bypass shoulder would be appropriate at the intersection of Brock Street and Emerson Street. It is recommended to increase the shoulder width to 11' to provide an additional 1' offset from curb.
- 10. Sheet OFF3 It is recommended to revise the Shoulder Widening Typical Section detail to have the full depth pavement structure extend to the existing edge of travel way and both the crushed gravel and gravel extend to the existing edge of pavement.
- 11. Sheet OFF3 Overall further detail is required of the design of the shoulder widening. This would include items such as any modifications to pavement markings, how the proposed widening will interface with the existing residential driveways and detail to show any required modifications to the existing closed drainage system. Full grading design with cut/fill limits will need to be understood to evaluate any impacts to adjacent properties.
- 12. Sheet OFF3 Applicant should coordinate with Rochester DPW on the desired pavement structure for the proposed shoulder widening.

Please let us know if you have any questions or if we can be of further assistance in the review of this project.

#### Columbus Avenue at Brock Street

| Test Operation Mode: 0 |  |
|------------------------|--|

|   |    |   |    | Schedule |    |   |    |          |
|---|----|---|----|----------|----|---|----|----------|
|   | Su | M | Tu | W        | Th | F | Sa | Day Plan |
| 1 |    | х | х  | х        | х  | х |    | 1        |
| 2 | х  |   |    |          |    |   | X  | 2        |
| - |    |   |    |          |    |   |    |          |

|   | Day Plan : | 1      |
|---|------------|--------|
|   | TOD        | Action |
| 1 | 0:00       | 54     |
| 2 | 6:30       | 1      |
| 3 | 9:00       | 2      |
| 4 | 14:00      | 3      |
| 5 | 19:00      | 54     |
| 6 | -          | -      |

|   | Day Plan 2 | 2      |
|---|------------|--------|
|   | TOD        | Action |
| 1 | 0:00       | 54     |
| 2 | 9:00       | 2      |
| 3 | 19:00      | 54     |
| 4 |            | -      |
| 5 | 7.6        |        |
| 6 | (4)        |        |

| Action | n Table |
|--------|---------|
| Action | Pattern |
| 54     | 254     |
| 1      | 1       |
| 2      | 2       |
| 3      | 3       |
|        | -       |
|        | -       |

| Pattern Table |       |        |       |     |  |  |  |  |  |  |
|---------------|-------|--------|-------|-----|--|--|--|--|--|--|
| Pattern       | Cycle | Offset | Split | Seq |  |  |  |  |  |  |
| 1             | 80    | 37     | 1     | 1   |  |  |  |  |  |  |
| 2             | 65    | 34     | 2     | 1   |  |  |  |  |  |  |
| 3             | 70    | 35     | 3     | 1   |  |  |  |  |  |  |
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|   | Sequence | T \ ung at  | iu barriei |    |  |
| 2 | 1        | 3           | 4          | 9  |  |
| 6 | 5        | 7           | 8          | 10 |  |

| Coordination Constants |          |       |         |  |  |  |  |  |  |  |
|------------------------|----------|-------|---------|--|--|--|--|--|--|--|
| Pattern                | Stragety | F.Off | Trans   |  |  |  |  |  |  |  |
| 1                      | EoG      | Fixed | Srt+Lng |  |  |  |  |  |  |  |
| 2                      | EoG      | Fixed | Srt+Lng |  |  |  |  |  |  |  |
| 3                      | EoG      | Fixed | Srt+Lng |  |  |  |  |  |  |  |
| -                      | -        | -     | -       |  |  |  |  |  |  |  |
|                        |          |       |         |  |  |  |  |  |  |  |

|           |   |          | Pha       | se Assignr    | nent     |            |     |
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|         |   |      |   | Fr   | ee/Split: 2 | 254  |   |      |    |    |
|---------|---|------|---|------|-------------|------|---|------|----|----|
| Phase   | 1 | 2 1  | 3 | 4    | 5           | 6    | 7 | 8    | 9  | 10 |
| Min Gr  | - | 10   | - | 5    | 5           | 10   | - | 5    | 7  | 7  |
| Pass*10 | - | 0.3  | - | 0.4  | -           | 0.3  | - | 0.3  | -  | -  |
| Max Gr  | - | 33.5 | - | 10.5 | 10          | 17.5 |   | 10.5 | 22 | 22 |
| Y Clr   |   | 3.5  | - | 3    | 3.5         | 3.5  | - | 3    | 3  | 3  |
| Red Clr | - | 2    | - | 2.5  | 2.5         | 2    |   | 2.5  | 1  | 1  |
| Split   | - | 39   | - | 16   | 16          | 23   | - | 16   | 26 | 26 |
| Walk    |   |      |   |      |             |      |   |      | 7  | 7  |
| Ped Clr |   |      |   |      |             |      |   |      | 15 | 15 |
| Recall  |   | Soft |   |      |             | Soft |   |      |    |    |
| D.Entry | - | X    |   | Х    |             | X    | - | X    |    |    |

|         |   |      |   |      | Split: 1 |       |     |      |    | ,  |
|---------|---|------|---|------|----------|-------|-----|------|----|----|
| Phase   | 1 | 2 1  | 3 | 4    | 5        | 6     | 7   | 8    | 9  | 10 |
| Min Gr  | - | 10   | - | 5    | 5        | 10    | -   | 5    | 5  | 5  |
| Pass*10 | - | 0.3  | - | 0.4  | -        | 0.3   | 1.7 | 0.3  | -  | -  |
| Max Gr  | - | 43.5 | - | 14.5 | 10       | 28.5  |     | 14.5 | 7  | 7  |
| Y CIF   | - | 3.5  | - | 3    | 3.5      | 3.5   |     | 3    | 3  | 3  |
| Red Clr |   | 3    | - | 2.5  | 2.5      | 2     |     | 2.5  | 1  | 1  |
| Split   | - | 50   | - | 20   | 16       | 34    | -   | 20   | 10 | 10 |
| Walk    |   |      |   |      |          |       |     |      | 7  | 7  |
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|         |   |      |   |      | Split: 2 |       |   |       |    |    |
|---------|---|------|---|------|----------|-------|---|-------|----|----|
| Phase   | 1 | 2 1  | 3 | 4    | 5        | 6     | 7 | 1 8 1 | 9  | 10 |
| Min Gr  | - | 10   | - | 5    | 5        | 10    | - | 5     | 5  | 5  |
| Pass*10 |   | 0.3  | - | 0.4  | -        | 0.3   |   | 0.3   |    |    |
| Max Gr  |   | 33.5 | - | 10.5 | 10       | 17.5  |   | 10.5  | 7  | 7  |
| Y Clr   | - | 3.5  | - | 3    | 3.5      | 3.5   |   | 3     | 3  | 3  |
| Red Clr | - | 3    | - | 2.5  | 2.5      | 2     | - | 2.5   | 1  | 1  |
| Split   | - | 39   | - | 20   | 16       | 23    | - | 16    | 6  | 6  |
| Walk    |   |      |   |      |          |       |   |       | 7  | 7  |
| Ped Cir |   |      |   |      |          |       |   |       | 15 | 15 |
| Recall  |   | Soft |   |      |          | Coord |   |       |    |    |
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|         |   |      |   |      | Split: 3 |       |               |      |    |    |
|---------|---|------|---|------|----------|-------|---------------|------|----|----|
| Phase   | 1 | 2    | 3 | 4    | 5        | 6     | 7             | 8    | 9  | 10 |
| Min Gr  |   | 10   | - | 5    | 5        | 10    | -             | 5    | 5  | 5  |
| Pass*10 | - | 0.3  | - | 0.4  | -        | 0.3   | -             | 0.3  | -  | -  |
| Max Gr  | - | 33.5 | - | 16.5 | 8        | 20.5  |               | 16.5 | 7  | 7  |
| Y Clr   | - | 3.5  | - | 3    | 3.5      | 3.5   | -             | 3    | 3  | 3  |
| Red Clr | - | 3    | - | 2.5  | 2.5      | 2     | -             | 2.5  | 1  | 1  |
| Split   | - | 40   | - | 22   | 14       | 26    | -             | 22   | 8  | 8  |
| Walk    |   |      |   |      |          |       | 4,000,000,000 |      | 7  | 7  |
| Ped Clr |   |      |   |      |          |       |               |      | 15 | 15 |
| Recall  |   | Soft |   |      |          | Coord |               |      |    |    |
| D.Entry |   | Х    | - | X    | -        | X     | -             | Х    | -  |    |

P.O. Box 1721 • Concord, NH 03302 tel: (603) 731-8500 • fax: (866) 929-6094 • sgp@ pernaw.com

Transportation: Engineering • Planning • Design

#### MEMORANDUM

Ref:

2112A

Δ

To:

Dana Webber, P.E., Assistant City Engineer, City of Rochester

Michael Green, Green and Company

From:

Stephen G. Pernaw, P.E., PTOE

Subject: Proposed Residential Development – Green and Company

Rochester, New Hampshire

Date:

April 11, 2022

On December 21, 2021 our office published the report entitled "Traffic Impact Assessment-Proposed Residential Development" for Green and Company. We are now in receipt of peer review comments from Sebago Technics dated March 11, 2022. The purpose of this memorandum is to provide responses to all applicable comments. Each comment is repeated below, for convenience:

SEBAGO COMMENT 1: "The TIA completed a trip generation calculation for the development using the Institute of Transportation Engineers Trip Generation Manual, 11th Edition. The calculation determined the development would generate a total of 1,192 trips on a Weekday, 77 trips in the AM Peak Hour of the adjacent street, and 95 Trips in the PM Peak Hour of the adjacent street. We are in agreement with this methodology and the calculated trip generation."

SGP & Co. Inc. Response: Comment acknowledged; no response necessary.

SEBAGO COMMENT 2: "The TIA presents no-build traffic volumes for the analysis years of 2023 and 2033. The volumes are based on turning movement counts collected at the study intersections, a seasonal adjustment factor of 1.01, a 2% annual background growth factor and a "COVID-19" adjustment factor of 1.53 for the AM Peak Hour and 1.30 for the PM Peak Hour."

SGP & Co. Inc. Response: Comment acknowledged; no response necessary.

SEBAGO COMMENT 3: "The study included a capacity and queueing analysis for the following intersections:

- Brock Street at Emerson Avenue (unsignalized)
- Brock Street at Old Gonic Road (unsignalized)
- Brock Street at NH 125 (Columbus Avenue) (Signalized)

We are in agreement with the methodology and findings of the analysis for the two unsignalized intersections along Brock Street. As stated above, the applicant proposes to construct a widened bypass shoulder on Brock Street westbound at the intersection with Emerson Avenue to help mitigate the impact of left-turning vehicles generated by the development."

SGP & Co. Inc. Response: Comment acknowledged; no response necessary.



SEBAGO COMMENT 4: "The analysis of the signalized intersection of Brock Street at NH 125 appears to have been completed using the Highway Capacity Manual (HCM) 2000 methodology within the Synchro 10 software environment. It is recommended to present revised results based on the latest HCM 6 methodology (as was done for the unsignalized intersections)."

**SGP & Co. Inc. Response**: Use of the HCM2000 methodology is consistent with and acceptable to the NHDOT. This methodology also provides a volume-to-capacity (v/c) ratio for the overall intersection; a helpful metric that is not available with the HCM6 methodology. Nevertheless, a supplemental capacity analysis was completed using HCM6, as requested (see Attachments 1-31).

<u>SEBAGO COMMENT 5</u>: "This intersection is also part of a coordinated signal system including the intersections along NH125 to the north including:

- NH 125 at Old Dover Road
- NH 125 at Charles Street
- NH 125 at Lowell Street

The completed Synchro/HCM analysis modeled the intersection as actuated-uncoordinated. Additionally, the modeled signal timings and recall settings do not accurately depict the existing signal timings. It is requested the applicant revise the capacity analysis using the existing signal timings. These are provided on the attached spreadsheet for reference. The applicant may reach out to us directly for any clarification that may be needed."

"It is recognized that using the existing signal timings with the presented analysis traffic volumes, which include a rather conservative Covid adjustment factor, may result in the intersection being over capacity under both no-build and build conditions. With that, we would request the revised analysis be completed using traffic volumes not adjusted by the stated covid factors."

**SGP & Co. Inc. Response**: Supplemental traffic volumes (without Covid factors) and the supplemental capacity analyses using HCM6 (and the signal timing parameters provided by Sebago Technics) are attached (see Attachments 32-35).

Other Considerations: It is our understanding that the current development proposal will be smaller than was analyzed in the traffic study. The table below demonstrates that the reduction in peak hour trips is inconsequential from a traffic impact and operations standpoint. Therefore, it is reasonable to conclude that the published study is slightly conservative on the "high side," and that the study findings and recommendations remain valid.

| Table 1         |                                   |                                     | ration Comparis<br>3 Units Townhouse:    |  |
|-----------------|-----------------------------------|-------------------------------------|--|--|
|                 |                                   | Previous<br>Proposal<br>(174 Units) | Current<br>Proposal<br>(168 Units)       | Net Change                             |
| Weekday (24 hou | urs) Entering<br>Exiting<br>Total | 596 veh<br>596 veh<br>1,192 trips   | 576 veh<br><u>576 veh</u><br>1,152 trips | -20 veh<br>-20 <u>veh</u><br>-40 trips |
| AM Peak Hour    | Entering<br>Exiting<br>Total      | 18 veh<br>59 <u>veh</u><br>77 trips | 18 veh<br><u>57 veh</u><br>75 trips      | 0 veh -2 veh -2 trips                  |
| PM Peak Hour    | Entering<br>Exiting<br>Total      | 60 veh<br>35 <u>veh</u><br>95 trips | 58 veh<br><u>35 veh</u><br>93 trips      | -2 veh<br><u>0 veh</u><br>-2 trips     |

<sup>&</sup>lt;sup>1</sup>ITE Land Use Code 220 - Multifamily Housing (Low-Rise) Trip Equation Method



## **ATTACHMENTS**

Table 6

|                             |       | 2021    | 2021 Existing | 5  |        | 2023            | 2023 No-Build |                                  |       | 2023 Build | Build  |                                  |          | 2033     | 2033 No-Build | 77                               |        | 2033      | 2033 Build |                                  |
|-----------------------------|-------|---------|---------------|--|--------|-----------------|---------------|----------------------------------|-------|------------|--------|----------------------------------|----------|----------|---------------|----------------------------------|--------|-----------|------------|----------------------------------|
|                             | V/C 1 | Delay 2 | SOT G         | Queue V/C 1) Delay 2) LOS 3) Avg/95 <sup>th 4)</sup> | V/C 1) | V/C 1) Delay 2) | LOS 31        | Queue<br>Avg/95 <sup>th 4)</sup> | V/C 1 | Delay 2)   | LOS 3) | Queue<br>Avg/95 <sup>th 4)</sup> | V/C t)   | Delay 2) | LOS 3)        | Queue<br>Avg/95 <sup>th 4)</sup> | V/C 1) | Delay 2)  | LOS 31     | Queue<br>Avg/95 <sup>th 4)</sup> |
| Weekday AM Peak Hour        |       |         |               | ********   |        |                 |               |                                  |       |            |        | *********                        |          |          |               | 1                                |        |           |            |                                  |
| Brock Street - EB LT&TH     | 0.38  | 29.8    | ပ             | 43 (81)  | 0.39   | 29.5            | ပ             | 46 (85)                          | 0.42  | 28.8       | ပ      | 51 (92)                          | 0.45     | 28.5     | O             | 56 (101)                         | 0.49   | 200       | c          | 63 (111)                         |
| Brock Street - EB RT        | 0.45  | 30.0    | ပ             | 0 (8)  | 0.41   | 29.3            | ပ             | 0 (4)                            | 0.52  | 29.1       | ပ      | 0 (24)                           | 0.39     | 27.0     | O             | 0 (13)                           | 0,51   | 27.5      | 0          | 0 (33)                           |
| Private Dwy - WB LT, TH, RT | 0.01  | 27.1    | O             | (0) 0  | 0.01   | 26.6            | ပ             | (0) 0                            | 0.01  | 25.3       | ပ      | (0) 0                            | 0.01     | 24.7     | ပ             | (0) 0                            | 0.01   | 24.0      | ပ          | (0) 0                            |
| NH125 - NB LT               | 0.39  | 32.8    | O             | 21 (52)  | 0.40   | 32.8            | ပ             | 22 (53)                          | 0.45  | 33.0       | ပ      | 26 (61)                          | 0.46     | 33.0     | ď             | 27 (62)                          | 0.50   | 20        | c          | 24 (60)                          |
| NH125 - NB TH&RT            | 0.28  | 2.7     | ∢             | 47 (77)  | 0.30   | 3.3             | ∢             | 54 (88)                          | 0.31  | 89.        | ∢      | 58 (94)                          | 0.38     | 4.6      | <             | 70 (113)                         | 0.39   | 5.0       | > <        | 70 (113)                         |
| NH125 - SB LT&TH            | 0.49  | 7.8     | ∢             | 148 (235)  | 0.54   | 9.3             | ∢             | 159 (254)                        | 0.56  | 10.6       | _      | 166 (264)                        | 0.70     | 14.1     | 60            | 219 (353)                        | 0.72   | ر.<br>بر: | α          | 210 (253)                        |
| NH125 - SB RT               | 0.08  | 4.7     | ∢             | (8)  | 0.09   | 5.4             | ∢             | (B) 0                            | 0.10  | 6.2        | ∢      | 0 (10)                           | 0.12     | 8.8      | <             | 0 (14)                           | 0.12   | 7.4       | > <        | 0 (15)                           |
| Overall                     | Ä     | 10.3    | •             | ******   | Ą      | 11.1            | •             |                                  | ¥     | 12.7       | m      | ********                         | AN<br>AN | 13.6     | m             |                                  | ¥      | 14.9      | 0          |                                  |
| Weekday PM Peak Hour        |       |         |               | *******  |        |                 |               |                                  |       |            |        | *********                        |          |          |               |                                  |        |           |            |                                  |
| Brock Street - EB LT&TH     | 0.54  | 26.2    | O             | 54 (121)   | 0.61   | 28.8            | ပ             | 57 (128)                         | 0.64  | 30.1       | O      | 61 (137)                         | 0.72     | 34.0     | C             | 73 (168)                         | 0.74   | 8         |            | (907) 666                        |
| Brock Street - EB RT        | 0.22  | 21.0    | ပ             | (O)<br>0   | 0.23   | 21.1            | O             | (0) 0                            | 0.29  | 21.5       | ပ      | (6) 0                            | 0.27     | 21.4     | O             | 0 (6)                            | 0.34   | 21.8      | ပ          | 0 (55)                           |
| Private Dwy - WB LT,TH,RT   | 90.0  | 20.4    | O             | 2 (15)   | 0.07   | 20.6            | O             | 2 (15)                           | 0.07  | 20.6       | ပ      | 2 (15)                           | 0.10     | 20.8     | O             | 3 (18)                           | 0.10   | 20.8      | O          | 8 (33)                           |
| NH125 - NB LT               | 0.57  | 29.7    | O ·           | 41 (97)  | 0.59   | 30.5            | ပ             | 43 (104)                         | 0.77  | 43.6       | ۵      | 59 (147)                         | 0.71     | 37.5     | ۵             | 53 (132)                         | 0.90   | 63.7      | ш          | 196 (358)                        |
| MAILZO - NB I MGK I         | 0.51  | 9.0     | ∢             | 106 (162)  | 0.54   | 6.9             | ∢             | 109 (175)                        | 0.54  | 6.9        | ν.     | 109 (175)                        | 0.63     | 7.5      | ∢             | 148 (247)                        | 0.63   | 7.5       | ∢          | 432 (616)                        |
| NH125 - SBLT&TH             | 0.68  | 16.1    | <b>6</b>      | 186 (292)  | 0.72   | 17.3            | 100           | 195 (317)                        | 0.72  | 17.3       |        | 195 (317)                        | 0.84     | 21.4     | O             | 271 (507)                        | 0.84   | 21.4      | O          | 846 (1165)                       |
| N 20 - 62 IN                | 0.24  | 9.7     | ∢             | 0 (25)   | 0.25   | о<br>О          | ∢             | 0 (26)                           | 0.27  | 10.0       | œ      | 0 (27)                           | 0.29     | 9.5      | ∢             | 0 (28)                           | 0.31   | 9.6       | ∢          | 29 (71)                          |
| Overall                     | ¥.    | 14.1    |               |  | NA     | 14.9            | 0             |                                  | A     | 16.5       | m      |                                  | N        | 17.5     | æ             |                                  | ¥      | 19.9      | m          |                                  |
|                             |       |         |               |  |        |                 |               | -                                |       |            |        |                                  |          |          |               |                                  |        |           |            |                                  |

1) Volume-to-capacity ratio, 2) Delay in vehicles per seconds, 3) Level of Service, 4) Queue length in feet

# HCM 6th Signalized Intersection Summary 3: NH 125 & Brock Street/Restaurant Driveway

|                              | ۶    | ->   | *    | •    | 4-           | 1    | 4    | †          | ~    | 1    | ţ    | 1    |
|------------------------------|------|------|------|------|--------------|------|------|------------|------|------|------|------|
| Movement                     | EBL  | EBT  | EBR  | WBL  | WBT          | WBR  | NBL  | NBT        | NBR  | SBL  | SBT  | SBR  |
| Lane Configurations          |      | ર્લ  | 7    |      | 4            |      | ř    | <b>1</b> > |      |      | 4    | 7    |
| Traffic Volume (veh/h)       | 92   | 0    | 67   | 1    | 0            | 1    | 47   | 364        | 0    | 0    | 547  | 79   |
| Future Volume (veh/h)        | 92   | 0    | 67   | 1    | 0            | 1    | 47   | 364        | 0    | 0    | 547  | 79   |
| Initial Q (Qb), veh          | 0    | 0    | 0    | 0    | 0            | 0    | 0    | 0          | 0    | 0    | 0    | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |      | 1.00 | 1.00 |              | 1.00 | 1.00 |            | 1.00 | 1.00 |      | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00 | 1.00 | 1.00 | 1.00         | 1.00 | 1.00 | 1.00       | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach        |      | No   |      |      | No           |      |      | No         |      |      | No   |      |
| Adj Sat Flow, veh/h/ln       | 1870 | 1900 | 1856 | 1900 | 1900         | 1900 | 1870 | 1811       | 1900 | 1900 | 1841 | 1885 |
| Adj Flow Rate, veh/h         | 111  | 0    | 81   | 1    | 0            | 1    | 51   | 391        | 0    | 0    | 588  | 85   |
| Peak Hour Factor             | 0.83 | 0.83 | 0.83 | 0.90 | 0.90         | 0.90 | 0.93 | 0.93       | 0.93 | 0.93 | 0.93 | 0.93 |
| Percent Heavy Veh, %         | 2    | 0    | 3    | 0    | 0            | 0    | 2    | 6          | 0    | 0    | 4    | 1    |
| Cap, veh/h                   | 291  | 0    | 191  | 120  | 24           | 66   | 131  | 1410       | 0    | 0    | 1193 | 1035 |
| Arrive On Green              | 0.12 | 0.00 | 0.12 | 0.12 | 0.00         | 0.12 | 0.07 | 0.78       | 0.00 | 0.00 | 0.65 | 0.65 |
| Sat Flow, veh/h              | 1554 | 0    | 1572 | 352  | 194          | 546  | 1781 | 1811       | 0    | 0    | 1841 | 1598 |
| Grp Volume(v), veh/h         | 111  | 0    | 81   | 2    | 0            | 0    | 51   | 391        | 0    | 0    | 588  | 85   |
| Grp Sat Flow(s),veh/h/ln     | 1554 | 0    | 1572 | 1092 | 0            | 0    | 1781 | 1811       | 0    | 0    | 1841 | 1598 |
| Q Serve(g_s), s              | 0.0  | 0.0  | 3.3  | 0.0  | 0.0          | 0.0  | 1.9  | 4.3        | 0.0  | 0.0  | 11.6 | 1.4  |
| Cycle Q Clear(g_c), s        | 4.4  | 0.0  | 3.3  | 4.4  | 0.0          | 0.0  | 1.9  | 4.3        | 0.0  | 0.0  | 11.6 | 1.4  |
| Prop In Lane                 | 1.00 |      | 1.00 | 0.50 |              | 0.50 | 1.00 |            | 0.00 | 0.00 |      | 1.00 |
| Lane Grp Cap(c), veh/h       | 291  | 0    | 191  | 210  | 0            | 0    | 131  | 1410       | 0    | 0    | 1193 | 1035 |
| V/C Ratio(X)                 | 0.38 | 0.00 | 0.42 | 0.01 | 0.00         | 0.00 | 0.39 | 0.28       | 0.00 | 0.00 | 0.49 | 0.08 |
| Avail Cap(c_a), veh/h        | 374  | 0    | 281  | 293  | 0            | 0    | 178  | 1410       | 0    | 0    | 1193 | 1035 |
| HCM Platoon Ratio            | 1.00 | 1.00 | 1.00 | 1.00 | 1.00         | 1.00 | 1.00 | 1.00       | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I)           | 1.00 | 0.00 | 1.00 | 1.00 | 0.00         | 0.00 | 1.00 | 1.00       | 0.00 | 0.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh     | 29.0 | 0.0  | 28.5 | 27.1 | 0.0          | 0.0  | 30.9 | 2.2        | 0.0  | 0.0  | 6.4  | 4.6  |
| Incr Delay (d2), s/veh       | 0.8  | 0.0  | 1.5  | 0.0  | 0.0          | 0.0  | 1.9  | 0.5        | 0.0  | 0.0  | 1.5  | 0.2  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0  | 0.0  | 0.0  | 0.0          | 0.0  | 0.0  | 0.0        | 0.0  | 0.0  | 0.0  | 0.0  |
| %ile BackOfQ(50%),veh/In     | 1.7  | 0.0  | 1.3  | 0.0  | 0.0          | 0.0  | 0.9  | 8.0        | 0.0  | 0.0  | 3.7  | 0.4  |
| Unsig. Movement Delay, s/veh |      |      |      |      |              |      |      |            |      |      |      |      |
| LnGrp Delay(d),s/veh         | 29.8 | 0.0  | 30.0 | 27.1 | 0.0          | 0.0  | 32.8 | 2.7        | 0.0  | 0.0  | 7.8  | 4.7  |
| LnGrp LOS                    | С    | A    | С    | С    | Α_           | Α    | C    | Α          | Α    | Α    | Α    | Α    |
| Approach Vol, veh/h          |      | 192  |      |      | 2            |      |      | 442        |      |      | 673  |      |
| Approach Delay, s/veh        |      | 29.9 |      |      | <b>27</b> .1 |      |      | 6.2        |      |      | 7.4  |      |
| Approach LOS                 |      | С    |      |      | С            |      |      | Α          |      |      | Α    |      |
| Timer - Assigned Phs         |      | 2    |      | 4    | 5            | 6    |      | 8          |      |      |      |      |
| Phs Duration (G+Y+Rc), s     |      | 58.0 |      | 12.0 | 9.1          | 48.9 |      | 12.0       |      |      |      |      |
| Change Period (Y+Rc), s      |      | 5.5  |      | 5.5  | 6.0          | 5.5  |      | 5.5        |      |      |      |      |
| Max Green Setting (Gmax), s  |      | 48.5 |      | 10.5 | 5.0          | 37.5 |      | 10.5       |      |      |      |      |
| Max Q Clear Time (g_c+l1), s |      | 6.3  |      | 6.4  | 3.9          | 13.6 |      | 6.4        |      |      |      |      |
| Green Ext Time (p_c), s      |      | 1.6  |      | 0.2  | 0.0          | 3.0  |      | 0.0        |      |      |      |      |
| Intersection Summary         |      |      |      |      |              |      |      |            |      |      |      |      |
| HCM 6th Ctrl Delay           |      |      | 10.3 |      |              |      |      |            |      |      |      |      |
| HCM 6th LOS                  |      |      | В    |      |              |      |      |            |      |      |      |      |

**Timings** 

# 3: NH 125 & Brock Street/Restaurant Driveway

|                      | *     | <b>-</b> | *     | 1     | <b>←</b> | 1     | †        | Ţ     | 1     |
|----------------------|-------|----------|-------|-------|----------|-------|----------|-------|-------|
| Lane Group           | EBL   | EBT      | EBR   | WBL   | WBT      | NBL   | NBT      | SBT   | SBR   |
| Lane Configurations  |       | न        | 7     |       | 4        | 7     | <b>1</b> | 4     | 7     |
| Traffic Volume (vph) | 92    | 0        | 67    | 1     | 0        | 47    | 364      | 547   | 79    |
| Future Volume (vph)  | 92    | 0        | 67    | 1     | 0        | 47    | 364      | 547   | 79    |
| Turn Type            | Perm  | NA       | Perm  | Perm  | NA       | Prot  | NA       | NA    | Perm  |
| Protected Phases     |       | 4        |       |       | 8        | 5     | 2        | 6     |       |
| Permitted Phases     | 4     |          | 4     | 8     |          |       |          |       | 6     |
| Detector Phase       | 4     | 4        | 4     | 8     | 8        | 5     | 2        | 6     | 6     |
| Switch Phase         |       |          |       |       |          |       |          |       |       |
| Minimum Initial (s)  | 5.0   | 5.0      | 5.0   | 5.0   | 5.0      | 5.0   | 10.0     | 10.0  | 10.0  |
| Minimum Split (s)    | 16.0  | 16.0     | 16.0  | 16.0  | 16.0     | 11.0  | 16.0     | 16.0  | 16.0  |
| Total Split (s)      | 16.0  | 16.0     | 16.0  | 16.0  | 16.0     | 11.0  | 54.0     | 43.0  | 43.0  |
| Total Split (%)      | 22.9% | 22.9%    | 22.9% | 22.9% | 22.9%    | 15.7% | 77.1%    | 61.4% | 61.4% |
| Yellow Time (s)      | 3.0   | 3.0      | 3.0   | 3.0   | 3.0      | 3.5   | 3.5      | 3.5   | 3.5   |
| All-Red Time (s)     | 2.5   | 2.5      | 2.5   | 2.5   | 2.5      | 2.5   | 2.0      | 2.0   | 2.0   |
| Lost Time Adjust (s) |       | -2.0     | -2.0  |       | -2.0     | -2.0  | -2.0     | -2.0  | -2.0  |
| Total Lost Time (s)  |       | 3.5      | 3.5   |       | 3.5      | 4.0   | 3.5      | 3.5   | 3.5   |
| Lead/Lag             |       |          |       |       |          | Lead  |          | Lag   | Lag   |
| Lead-Lag Optimize?   |       |          |       |       |          | Yes   |          | Yes   | Yes   |
| Recall Mode          | None  | None     | None  | None  | None     | None  | C-Max    | C-Max | C-Max |
| Act Effct Green (s)  |       | 11.3     | 11.3  |       | 11.2     | 7.4   | 54.7     | 48.1  | 48.1  |
| Actuated g/C Ratio   |       | 0.16     | 0.16  |       | 0.16     | 0.11  | 0.78     | 0.69  | 0.69  |
| v/c Ratio            |       | 0.49     | 0.22  |       | 0.01     | 0.27  | 0.28     | 0.47  | 0.07  |
| Control Delay        |       | 34.1     | 3.3   |       | 0.0      | 33.3  | 3.7      | 9.5   | 0.7   |
| Queue Delay          |       | 0.0      | 0.0   |       | 0.0      | 0.0   | 0.0      | 0.0   | 0.0   |
| Total Delay          |       | 34.1     | 3.3   |       | 0.0      | 33.3  | 3.7      | 9.5   | 0.7   |
| LOS                  |       | С        | Α     |       | Α        | С     | Α        | Α     | Α     |
| Approach Delay       |       | 21.1     |       |       |          |       | 7.1      | 8.4   |       |
| Approach LOS         |       | С        |       |       |          |       | Α        | Α     |       |
| Intersection Summary |       |          |       |       |          |       |          |       |       |

Cycle Length: 70

Actuated Cycle Length: 70

Offset: 0 (0%), Referenced to phase 2:NBT and 6:SBTL, Start of Yellow

Natural Cycle: 55

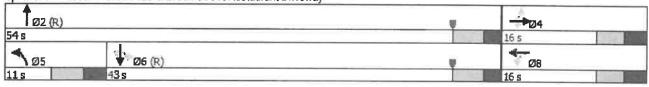
Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.49 Intersection Signal Delay: 9.8 Intersection Capacity Utilization 54.7%

Intersection LOS: A ICU Level of Service A

Analysis Period (min) 15

Splits and Phases: 3: NH 125 & Brock Street/Restaurant Driveway



## Queues

# 3: NH 125 & Brock Street/Restaurant Driveway

|                         | -    | *    | -    | 4    | <b>†</b> | <b>↓</b> | 1    |
|-------------------------|------|------|------|------|----------|----------|------|
| Lane Group              | EBT  | EBR  | WBT  | NBL  | NBT      | SBT      | SBR  |
| Lane Group Flow (vph)   | 111  | 81   | 2    | 51   | 391      | 588      | 85   |
| v/c Ratio               | 0.49 | 0.22 | 0.01 | 0.27 | 0.28     | 0.47     | 0.07 |
| Control Delay           | 34.1 | 3.3  | 0.0  | 33.3 | 3.7      | 9.5      | 0.7  |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0      | 0.0      | 0.0  |
| Total Delay             | 34.1 | 3.3  | 0.0  | 33.3 | 3.7      | 9.5      | 0.7  |
| Queue Length 50th (ft)  | 43   | 0    | 0    | 21   | 47       | 148      | 0    |
| Queue Length 95th (ft)  | 81   | 8    | 0    | 52   | 77       | 235      | 8    |
| Internal Link Dist (ft) | 204  |      | 294  |      | 1001     | 1243     |      |
| Turn Bay Length (ft)    |      |      |      | 375  |          |          |      |
| Base Capacity (vph)     | 251  | 388  | 383  | 186  | 1401     | 1256     | 1140 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0        | 0        | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0        | 0        | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0        | 0        | 0    |
| Reduced v/c Ratio       | 0.44 | 0.21 | 0.01 | 0.27 | 0.28     | 0.47     | 0.07 |
| Intersection Summary    |      |      |      |      |          |          |      |

|   | ۶    | <b>→</b>   | *    | 1     | <b>—</b>  | 1     | 4    | 1        | 1    | 1    | ļ        | 1    |
|---|------|------------|------|-------|-----------|-------|------|----------|------|------|----------|------|
| Movement  | EBL  | EBT        | EBR  | WBL   | WBT       | WBR   | NBL  | NBT      | NBR  | SBL  | SBT      | SBR  |
| Lane Configurations                                     |      | 4          | 7    |       | 4         |       | 7    | <b>1</b> |      |      | र्न      | 7    |
| Traffic Volume (veh/h)                                  | 97   | 0          | 70   | 1     | 0         | 1     | 49   | 382      | 0    | 0    | 575      | 83   |
| Future Volume (veh/h)                                   | 97   | 0          | 70   | 1     | 0         | 1     | 49   | 382      | 0    | 0    | 575      | 83   |
| Initial Q (Qb), veh                                     | 0    | 0          | 0    | 0     | 0         | 0     | 0    | 0        | 0    | 0    | 0        | 0    |
| Ped-Bike Adj(A_pbT)                                     | 1.00 |            | 1.00 | 1.00  |           | 1.00  | 1.00 |          | 1.00 | 1.00 |          | 1.00 |
| Parking Bus, Adj  | 1.00 | 1.00       | 1.00 | 1.00  | 1.00      | 1.00  | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 |
| Work Zone On Approach                                   |      | No         |      |       | No        |       |      | No       |      |      | No       |      |
| Adj Sat Flow, veh/h/ln                                  | 1870 | 1900       | 1856 | 1900  | 1900      | 1900  | 1870 | 1811     | 1900 | 1900 | 1841     | 1885 |
| Adj Flow Rate, veh/h                                    | 117  | 0          | 84   | 1     | 0         | 1     | 53   | 411      | 0    | 0    | 618      | 89   |
| Peak Hour Factor  | 0.83 | 0.83       | 0.83 | 0.90  | 0.90      | 0.90  | 0.93 | 0.93     | 0.93 | 0.93 | 0.93     | 0.93 |
| Percent Heavy Veh, %                                    | 2    | 0          | 3    | 0     | 0         | 0     | 2    | 6        | 0.00 | 0.00 | 4        | 1    |
| Cap, veh/h  | 297  | 0          | 205  | 120   | 24        | 66    | 133  | 1368     | 0    | 0    | 1148     | 996  |
| Arrive On Green   | 0.13 | 0.00       | 0.13 | 0.13  | 0.00      | 0.13  | 0.07 | 0.76     | 0.00 | 0.00 | 0.62     | 0.62 |
| Sat Flow, veh/h   | 1487 | 0.00       | 1572 | 326   | 183       | 509   | 1781 | 1811     | 0.00 | 0.00 | 1841     |      |
| Grp Volume(v), veh/h                                    | 117  | 0          | 84   | 2     | 0         | 0     |      |          |      |      |          | 1598 |
| Grp Sat Flow(s), veh/h/ln                               | 1487 | 0          | 1572 | 1018  |           |       | 53   | 411      | 0    | 0    | 618      | 89   |
|   |      |            |      | 44. 4 | 0         | 0     | 1781 | 1811     | 0    | 0    | 1841     | 1598 |
| Q Serve(g_s), s   | 0.0  | 0.0        | 3.4  | 0.0   | 0.0       | 0.0   | 2.0  | 5.0      | 0.0  | 0.0  | 13.3     | 1.6  |
| Cycle Q Clear(g_c), s                                   | 5.1  | 0.0        | 3.4  | 5.1   | 0.0       | 0.0   | 2.0  | 5.0      | 0.0  | 0.0  | 13.3     | 1.6  |
| Prop in Lane  | 1.00 |            | 1.00 | 0.50  |           | 0.50  | 1.00 |          | 0.00 | 0.00 |          | 1.00 |
| Lane Grp Cap(c), veh/h                                  | 297  | 0          | 205  | 210   | 0         | 0     | 133  | 1368     | 0    | 0    | 1148     | 996  |
| V/C Ratio(X)  | 0.39 | 0.00       | 0.41 | 0.01  | 0.00      | 0.00  | 0.40 | 0.30     | 0.00 | 0.00 | 0.54     | 0.09 |
| Avail Cap(c_a), veh/h                                   | 366  | 0          | 281  | 280   | 0         | 0     | 178  | 1368     | 0    | 0    | 1148     | 996  |
| HCM Platoon Ratio                                       | 1.00 | 1.00       | 1.00 | 1.00  | 1.00      | 1.00  | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00 |
| Upstream Filter(I)                                      | 1.00 | 0.00       | 1.00 | 1.00  | 0.00      | 0.00  | 1.00 | 1.00     | 0.00 | 0.00 | 1.00     | 1.00 |
| Uniform Delay (d), s/veh                                | 28.7 | 0.0        | 28.0 | 26.6  | 0.0       | 0.0   | 30.9 | 2.7      | 0.0  | 0.0  | 7.5      | 5.3  |
| Incr Delay (d2), s/veh                                  | 8.0  | 0.0        | 1.3  | 0.0   | 0.0       | 0.0   | 1.9  | 0.6      | 0.0  | 0.0  | 1.8      | 0.2  |
| Initial Q Delay(d3),s/veh                               | 0.0  | 0.0        | 0.0  | 0.0   | 0.0       | 0.0   | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0  |
| %ile BackOfQ(50%),veh/ln                                | 1.8  | 0.0        | 1.3  | 0.0   | 0.0       | 0.0   | 0.9  | 1.1      | 0.0  | 0.0  | 4.5      | 0.4  |
| Unsig. Movement Delay, s/veh                            |      |            |      |       |           |       |      |          |      |      | 110      | 0.1  |
| LnGrp Delay(d),s/veh                                    | 29.5 | 0.0        | 29.3 | 26.6  | 0.0       | 0.0   | 32.8 | 3.3      | 0.0  | 0.0  | 9.3      | 5.4  |
| _nGrp LOS   | С    | Α          | C    | С     | Α         | A     | C    | Α        | A    | A    | Α.       | Α.   |
| Approach Vol, veh/h                                     |      | 201        |      |       | 2         |       |      | 464      |      |      | 707      |      |
| Approach Delay, s/veh                                   |      | 29.4       |      |       | 26.6      |       |      | 6.7      |      |      |          |      |
| Approach LOS  |      | C C        |      |       | 20.0<br>C |       |      | Α.       |      |      | 8.8<br>A |      |
| Timer - Assigned Phs                                    |      | 2          |      | 4     | 5         | 6     |      | 8        |      |      | ^        |      |
| Phs Duration (G+Y+Rc), s                                |      | 57.4       |      | 12.6  | 9.2       | 48.2  |      |          |      |      |          |      |
| Change Period (Y+Rc), s                                 |      | 6.5        |      |       |           |       |      | 12.6     |      |      |          |      |
| Max Green Setting (Gmax), s                             |      |            |      | 5.5   | 6.0       | * 6.5 |      | 5.5      |      |      |          |      |
|   |      | 47.5       |      | 10.5  | 5.0       | * 38  |      | 10.5     |      |      |          |      |
| Max Q Clear Time (g_c+l1), s<br>Green Ext Time (p_c), s |      | 7.0<br>1.7 |      | 7.1   | 4.0       | 15.3  |      | 7.1      |      |      |          |      |
| " ,   |      | 1.1        |      | 0.2   | 0.0       | 3.1   |      | 0.0      |      |      |          |      |
| ntersection Summary                                     |      |            | 11 1 |       |           |       |      |          |      |      |          |      |
| HCM 6th Ctrl Delay<br>HCM 6th LOS                       |      |            | 11.1 |       |           |       |      |          |      |      |          |      |
|   |      |            | В    |       |           |       |      |          |      |      |          |      |
| Votes   |      |            |      |       |           |       |      |          |      |      |          |      |

<sup>\*</sup> HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

**Timings** 

# 3: NH 125 & Brock Street/Restaurant Driveway

|                      | *     | -     | •     | 1     | 4     | 1     | †     | ļ     | 1     |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Group           | EBL   | EBT   | EBR   | WBL   | WBT   | NBL   | NBT   | SBT   | SBR   |
| Lane Configurations  |       | લી    | 7     |       | 4     | 3     | Þ     | व     | 7     |
| Traffic Volume (vph) | 97    | 0     | 70    | 1     | 0     | 49    | 382   | 575   | 83    |
| Future Volume (vph)  | 97    | 0     | 70    | 1     | 0     | 49    | 382   | 575   | 83    |
| Turn Type            | Perm  | NA    | Perm  | Perm  | NA    | Prot  | NA    | NA    | Perm  |
| Protected Phases     |       | 4     |       |       | 8     | 5     | 2     | 6     |       |
| Permitted Phases     | 4     |       | 4     | 8     |       |       |       |       | 6     |
| Detector Phase       | 4     | 4     | 4     | 8     | 8     | 5     | 2     | 6     | 6     |
| Switch Phase         |       |       |       |       |       |       |       |       |       |
| Minimum Initial (s)  | 5.0   | 5.0   | 5.0   | 5.0   | 5.0   | 5.0   | 10.0  | 10.0  | 10.0  |
| Minimum Split (s)    | 16.0  | 16.0  | 16.0  | 16.0  | 16.0  | 11.0  | 16.5  | 16.0  | 16.0  |
| Total Split (s)      | 16.0  | 16.0  | 16.0  | 16.0  | 16.0  | 11.0  | 54.0  | 43.0  | 43.0  |
| Total Split (%)      | 22.9% | 22.9% | 22.9% | 22.9% | 22.9% | 15.7% | 77.1% | 61.4% | 61.4% |
| Yellow Time (s)      | 3.0   | 3.0   | 3.0   | 3.0   | 3.0   | 3.5   | 3.5   | 3.5   | 3.5   |
| All-Red Time (s)     | 2.5   | 2.5   | 2.5   | 2.5   | 2.5   | 2.5   | 3.0   | 2.0   | 2.0   |
| Lost Time Adjust (s) |       | -2.0  | -2.0  |       | -2.0  | -2.0  | -2.0  | -2.0  | -2.0  |
| Total Lost Time (s)  |       | 3.5   | 3.5   |       | 3.5   | 4.0   | 4.5   | 3.5   | 3.5   |
| Lead/Lag             |       |       |       |       |       | Lead  |       | Lag   | Lag   |
| Lead-Lag Optimize?   |       |       |       |       |       | Yes   |       | Yes   | Yes   |
| Recall Mode          | None  | None  | None  | None  | None  | None  | C-Max | C-Max | C-Max |
| Act Effct Green (s)  |       | 11.4  | 11.4  |       | 11.2  | 7.4   | 53.9  | 48.1  | 48,1  |
| Actuated g/C Ratio   |       | 0.16  | 0.16  |       | 0.16  | 0.11  | 0.77  | 0.69  | 0.69  |
| v/c Ratio            |       | 0.51  | 0.22  |       | 0.01  | 0.28  | 0.30  | 0.49  | 0.08  |
| Control Delay        |       | 34.8  | 2.5   |       | 0.0   | 33.5  | 4.1   | 9.8   | 0.8   |
| Queue Delay          |       | 0.0   | 0.0   |       | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| Total Delay          |       | 34.8  | 2.5   |       | 0.0   | 33.5  | 4.1   | 9.8   | 0.8   |
| LOS                  |       | С     | Α     |       | Α     | С     | Α     | Α     | Α     |
| Approach Delay       |       | 21.3  |       |       |       |       | 7.5   | 8.7   |       |
| Approach LOS         |       | С     |       |       |       |       | A     | Α     |       |
| Intersection Summary |       |       |       |       |       |       |       |       |       |

Cycle Length: 70 Actuated Cycle Length: 70

Offset: 47.5 (68%), Referenced to phase 2:NBT and 6:SBTL, Start of Yellow

Natural Cycle: 60

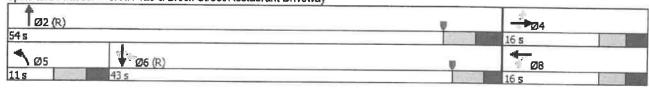
Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.51 Intersection Signal Delay: 10.1 Intersection Capacity Utilization 57.3%

Intersection LOS: B ICU Level of Service B

Analysis Period (min) 15

Splits and Phases: 3: NH 125 & Brock Street/Restaurant Driveway



|                         | -    | *    | 4    | 1    | <b>†</b> | 1    | 1    |
|-------------------------|------|------|------|------|----------|------|------|
| Lane Group              | EBT  | EBR  | WBT  | NBL  | NBT      | SBT  | SBR  |
| Lane Group Flow (vph)   | 117  | 84   | 2    | 53   | 411      | 618  | 89   |
| v/c Ratio               | 0.51 | 0.22 | 0.01 | 0.28 | 0.30     | 0.49 | 0.08 |
| Control Delay           | 34.8 | 2.5  | 0.0  | 33.5 | 4.1      | 9.8  | 0.8  |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0      | 0.0  | 0.0  |
| Total Delay             | 34.8 | 2.5  | 0.0  | 33.5 | 4.1      | 9.8  | 0.8  |
| Queue Length 50th (ft)  | 46   | 0    | 0    | 22   | 54       | 159  | 0    |
| Queue Length 95th (ft)  | 85   | 4    | 0    | 53   | 88       | 254  | 8    |
| Internal Link Dist (ft) | 204  |      | 294  |      | 1001     | 1243 |      |
| Turn Bay Length (ft)    |      |      |      | 375  |          |      |      |
| Base Capacity (vph)     | 251  | 401  | 396  | 186  | 1379     | 1254 | 1139 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0        | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0        | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0        | 0    | 0    |
| Reduced v/c Ratio       | 0.47 | 0.21 | 0.01 | 0.28 | 0.30     | 0.49 | 0.08 |
| Intersection Summary    |      |      |      |      |          |      |      |

# HCM 6th Signalized Intersection Summary 3: NH 125 & Brock Street/Restaurant Driveway

|                              | ۶         | -    | *    | 1    | +    | 1     | 4    | †    | -    | 1         | <b></b> | 1    |
|------------------------------|-----------|------|------|------|------|-------|------|------|------|-----------|---------|------|
| Movement                     | EBL       | EBT  | EBR  | WBL  | WBT  | WBR   | NBL  | NBT  | NBR  | SBL       | SBT     | SBR  |
| Lane Configurations          |           | र्न  | 7    |      | 4    |       | Ť    | 7-   |      |           | र्स     | 7    |
| Traffic Volume (veh/h)       | 118       | 0    | 85   | 1    | 0    | 1     | 60   | 466  | 0    | 0         | 701     | 101  |
| Future Volume (veh/h)        | 118       | 0    | 85   | 1    | 0    | 1     | 60   | 466  | 0    | 0         | 701     | 101  |
| Initial Q (Qb), veh          | 0         | 0    | 0    | 0    | 0    | 0     | 0    | 0    | 0    | 0         | 0       | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00      |      | 1.00 | 1.00 |      | 1.00  | 1.00 |      | 1.00 | 1.00      |         | 1.00 |
| Parking Bus, Adj             | 1.00      | 1.00 | 1.00 | 1.00 | 1.00 | 1.00  | 1.00 | 1.00 | 1.00 | 1.00      | 1.00    | 1.00 |
| Work Zone On Approach        |           | No   |      |      | No   |       |      | No   |      |           | No      |      |
| Adj Sat Flow, veh/h/ln       | 1870      | 1900 | 1856 | 1900 | 1900 | 1900  | 1870 | 1811 | 1900 | 1900      | 1841    | 1885 |
| Adj Flow Rate, veh/h         | 142       | 0    | 102  | 1    | 0    | 1     | 65   | 501  | 0    | 0         | 754     | 109  |
| Peak Hour Factor             | 0.83      | 0.83 | 0.83 | 0.90 | 0.90 | 0.90  | 0.93 | 0.93 | 0.93 | 0.93      | 0.93    | 0.93 |
| Percent Heavy Veh, %         | 2         | 0    | 3    | 0    | 0    | 0     | 2    | 6    | 0    | 0         | 4       | 1    |
| Cap, veh/h                   | 319       | 0    | 260  | 119  | 24   | 66    | 142  | 1304 | 0    | 0         | 1074    | 932  |
| Arrive On Green              | 0.17      | 0.00 | 0.17 | 0.17 | 0.00 | 0.17  | 0.08 | 0.72 | 0.00 | 0.00      | 0.58    | 0.58 |
| Sat Flow, veh/h              | 1307      | 0    | 1572 | 250  | 148  | 398   | 1781 | 1811 | 0    | 0         | 1841    | 1598 |
| Grp Volume(v), veh/h         | 142       | 0    | 102  | 2    | 0    | 0     | 65   | 501  | 0    | 0         | 754     | 109  |
| Grp Sat Flow(s),veh/h/ln     | 1307      | Ö    | 1572 | 796  | Ö    | 0     | 1781 | 1811 | Ö    | 0         | 1841    | 1598 |
| Q Serve(g_s), s              | 0.0       | 0.0  | 4.1  | 0.0  | 0.0  | 0.0   | 2.4  | 7.5  | 0.0  | 0.0       | 20.2    | 2.1  |
| Cycle Q Clear(g_c), s        | 7.6       | 0.0  | 4.1  | 7.6  | 0.0  | 0.0   | 2.4  | 7.5  | 0.0  | 0.0       | 20.2    | 2.1  |
| Prop In Lane                 | 1.00      | 0.0  | 1.00 | 0.50 | 0.0  | 0.50  | 1.00 | 1.0  | 0.00 | 0.00      | 20.2    |      |
| Lane Grp Cap(c), veh/h       | 319       | 0    | 260  | 209  | 0    | 0.00  | 142  | 1304 | 0.00 | 0.00      | 1074    | 1.00 |
| V/C Ratio(X)                 | 0.45      | 0.00 | 0.39 | 0.01 | 0.00 | 0.00  | 0.46 | 0.38 | 0.00 |           |         | 932  |
| Avail Cap(c_a), veh/h        | 338       | 0.00 | 281  | 228  | 0.00 | 0.00  | 178  | 1304 | 0.00 | 0.00<br>0 | 0.70    | 0.12 |
| HCM Platoon Ratio            | 1.00      | 1.00 | 1.00 | 1.00 | 1.00 | 1.00  | 1.00 | 1.00 | 1.00 | 1.00      | 1074    | 932  |
| Upstream Filter(I)           | 1.00      | 0.00 | 1.00 | 1.00 | 0.00 | 0.00  | 1.00 | 1.00 | 0.00 |           | 1.00    | 1.00 |
| Uniform Delay (d), s/veh     | 27.5      | 0.0  | 26.1 | 24.6 | 0.0  | 0.00  | 30.8 | 3.8  | 0.00 | 0.00      | 1.00    | 1.00 |
| incr Delay (d2), s/veh       | 1.0       | 0.0  | 1.0  | 0.0  | 0.0  | 0.0   | 2.3  | 0.9  | 0.0  | 0.0       | 10.3    | 6.5  |
| Initial Q Delay(d3),s/veh    | 0.0       | 0.0  | 0.0  | 0.0  | 0.0  | 0.0   | 0.0  |      |      | 0.0       | 3.8     | 0.3  |
| %ile BackOfQ(50%),veh/ln     | 2.2       | 0.0  | 1.5  | 0.0  | 0.0  | 0.0   |      | 0.0  | 0.0  | 0.0       | 0.0     | 0.0  |
| Unsig. Movement Delay, s/veh | 2.2       | 0.0  | 1.5  | 0.0  | 0.0  | 0.0   | 1.1  | 1.9  | 0.0  | 0.0       | 7.5     | 0.7  |
| LnGrp Delay(d),s/veh         | 28.5      | 0.0  | 27.0 | 24.7 | 0.0  | 0.0   | 00.0 | 4.0  |      |           |         |      |
| LnGrp LOS                    | 20.5<br>C | 0.0  | 27.0 | 24.7 | 0.0  | 0.0   | 33.0 | 4.6  | 0.0  | 0.0       | 14.1    | 6.8  |
|                              |           | A    | C    | C    | A    | Α     | C    | A    | A    | A         | В       | A    |
| Approach Vol, veh/h          |           | 244  |      |      | 2    |       |      | 566  |      |           | 863     |      |
| Approach Delay, s/veh        |           | 27.9 |      |      | 24.7 |       |      | 7.9  |      |           | 13.2    |      |
| Approach LOS                 |           | С    |      |      | С    |       |      | Α    |      |           | В       |      |
| Timer - Assigned Phs         |           | 2    |      | 4    | 5    | 6     |      | 8    |      |           |         |      |
| Phs Duration (G+Y+Rc), s     |           | 54.9 |      | 15.1 | 9.6  | 45.3  |      | 15.1 |      |           |         |      |
| Change Period (Y+Rc), s      |           | 6.5  |      | 5.5  | 6.0  | * 6.5 |      | 5.5  |      |           |         |      |
| Max Green Setting (Gmax), s  |           | 47.5 |      | 10.5 | 5.0  | * 38  |      | 10.5 |      |           |         |      |
| Max Q Clear Time (g_c+l1), s |           | 9.5  |      | 9.6  | 4.4  | 22.2  |      | 9.6  |      |           |         |      |
| Green Ext Time (p_c), s      |           | 2.2  |      | 0.1  | 0.0  | 3.7   |      | 0.0  |      |           |         |      |
| Intersection Summary         |           |      |      |      |      |       |      |      |      |           |         |      |
| HCM 6th Ctrl Delay           |           |      | 13.6 |      |      |       |      |      |      |           |         |      |
| HCM 6th LOS                  |           |      | В    |      |      |       |      |      |      |           |         |      |
| Notes                        |           |      |      |      |      |       |      |      |      |           |         |      |

<sup>\*</sup> HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

**Timings** 

|                      | 1     | $\rightarrow$ | •     | 1     | 4     | 4     | 1     | 1     | 1     |
|----------------------|-------|---------------|-------|-------|-------|-------|-------|-------|-------|
| Lane Group           | EBL   | EBT           | EBR   | WBL   | WBT   | NBL   | NBT   | SBT   | SBR   |
| Lane Configurations  |       | 4             | 7     |       | 4     | 7     | f)    | सी    | 78    |
| Traffic Volume (vph) | 118   | 0             | 85    | 1     | 0     | 60    | 466   | 701   | 101   |
| Future Volume (vph)  | 118   | 0             | 85    | 1     | 0     | 60    | 466   | 701   | 101   |
| Turn Type            | Perm  | NA            | Perm  | Perm  | NA    | Prot  | NA    | NA    | Perm  |
| Protected Phases     |       | 4             |       |       | 8     | 5     | 2     | 6     |       |
| Permitted Phases     | 4     |               | 4     | 8     |       |       |       | ·     | 6     |
| Detector Phase       | 4     | 4             | 4     | 8     | 8     | 5     | 2     | 6     | 6     |
| Switch Phase         |       |               |       |       |       |       | _     |       | •     |
| Minimum Initial (s)  | 5.0   | 5.0           | 5.0   | 5.0   | 5.0   | 5.0   | 10.0  | 10.0  | 10.0  |
| Minimum Split (s)    | 16.0  | 16.0          | 16.0  | 16.0  | 16.0  | 11.0  | 16.5  | 16.0  | 16.0  |
| Total Split (s)      | 16.0  | 16.0          | 16.0  | 16.0  | 16.0  | 11.0  | 54.0  | 43.0  | 43.0  |
| Total Split (%)      | 22.9% | 22.9%         | 22.9% | 22.9% | 22.9% | 15.7% | 77.1% | 61.4% | 61.4% |
| Yellow Time (s)      | 3.0   | 3.0           | 3.0   | 3.0   | 3.0   | 3.5   | 3.5   | 3.5   | 3.5   |
| All-Red Time (s)     | 2.5   | 2.5           | 2.5   | 2.5   | 2.5   | 2.5   | 3.0   | 2.0   | 2.0   |
| Lost Time Adjust (s) |       | -2.0          | -2.0  |       | -2.0  | -2.0  | -2.0  | -2.0  | -2.0  |
| Total Lost Time (s)  |       | 3.5           | 3.5   |       | 3.5   | 4.0   | 4.5   | 3.5   | 3.5   |
| Lead/Lag             |       |               |       |       |       | Lead  |       | Lag   | Lag   |
| Lead-Lag Optimize?   |       |               |       |       |       | Yes   |       | Yes   | Yes   |
| Recall Mode          | None  | None          | None  | None  | None  | None  | C-Max | C-Max | C-Max |
| Act Effct Green (s)  |       | 11.7          | 11.7  |       | 11.7  | 7.2   | 50.3  | 44.7  | 44.7  |
| Actuated g/C Ratio   |       | 0.17          | 0.17  |       | 0.17  | 0.10  | 0.72  | 0.64  | 0.64  |
| v/c Ratio            |       | 0.60          | 0.26  |       | 0.01  | 0.36  | 0.39  | 0.65  | 0.10  |
| Control Delay        |       | 38.3          | 3.9   |       | 0.0   | 35.5  | 5.1   | 12.9  | 1.3   |
| Queue Delay          |       | 0.0           | 0.0   |       | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| Total Delay          |       | 38.3          | 3.9   |       | 0.0   | 35.5  | 5.1   | 12.9  | 1.3   |
| LOS                  |       | D             | Α     |       | Α     | D     | Α     | В     | A     |
| Approach Delay       |       | 23.9          |       |       |       |       | 8.6   | 11.4  |       |
| Approach LOS         |       | С             |       |       |       |       | Α     | В     |       |
| Intersection Summary |       |               |       |       |       |       |       |       |       |

Cycle Length: 70

Actuated Cycle Length: 70

Offset: 47.5 (68%), Referenced to phase 2:NBT and 6:SBTL, Start of Yellow

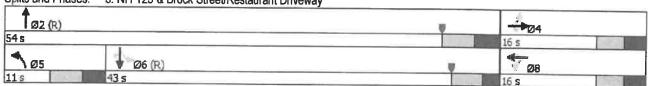
Natural Cycle: 60

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.65 Intersection Signal Delay: 12.3 Intersection Capacity Utilization 68.5%

Intersection LOS: B ICU Level of Service C

Analysis Period (min) 15



|                         | -    | *    | -    | 1    | <b>†</b> | 1    | 1    |
|-------------------------|------|------|------|------|----------|------|------|
| Lane Group              | EBT  | EBR  | WBT  | NBL  | NBT      | SBT  | SBR  |
| Lane Group Flow (vph)   | 142  | 102  | 2    | 65   | 501      | 754  | 109  |
| v/c Ratio               | 0.60 | 0.26 | 0.01 | 0.36 | 0.39     | 0.65 | 0.10 |
| Control Delay           | 38.3 | 3.9  | 0.0  | 35.5 | 5.1      | 12.9 | 1.3  |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0      | 0.0  | 0.0  |
| Total Delay             | 38.3 | 3.9  | 0.0  | 35.5 | 5.1      | 12.9 | 1.3  |
| Queue Length 50th (ft)  | 56   | 0    | 0    | 27   | 70       | 219  | 0    |
| Queue Length 95th (ft)  | 101  | 13   | 0    | 62   | 113      | 353  | 14   |
| Internal Link Dist (ft) | 204  |      | 294  |      | 1001     | 1243 | , ,  |
| Turn Bay Length (ft)    |      |      |      | 375  |          |      |      |
| Base Capacity (vph)     | 251  | 401  | 399  | 181  | 1287     | 1165 | 1068 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0        | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0        | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0        | 0    | 0    |
| Reduced v/c Ratio       | 0.57 | 0.25 | 0.01 | 0.36 | 0.39     | 0.65 | 0.10 |
| Intersection Summary    |      |      |      |      |          |      |      |

|                              | *    |      | $\rightarrow$ | 1    | +    | •     | 4        | 1    | 1    | 1    | Į.   | 1    |
|------------------------------|------|------|---------------|------|------|-------|----------|------|------|------|------|------|
| Movement                     | EBL  | EBT  | EBR           | WBL  | WBT  | WBR   | NBL      | NBT  | NBR  | SBL  | SBT  | SBR  |
| Lane Configurations          |      | 4    | 7             |      | 4    |       | T.       | 1>   |      |      | 4    | 7    |
| Traffic Volume (veh/h)       | 109  | 0    | 104           | 1    | 0    | 1     | 59       | 382  | 0    | 0    | 575  | 87   |
| Future Volume (veh/h)        | 109  | 0    | 104           | 1    | 0    | 1     | 59       | 382  | 0    | 0    | 575  | 87   |
| Initial Q (Qb), veh          | 0    | 0    | 0             | 0    | 0    | 0     | 0        | 0    | 0    | 0    | 0    | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |      | 1.00          | 1.00 |      | 1.00  | 1.00     |      | 1.00 | 1.00 |      | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00 | 1.00          | 1.00 | 1.00 | 1.00  | 1.00     | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach        |      | No   |               |      | No   |       |          | No   |      |      | No   |      |
| Adj Sat Flow, veh/h/ln       | 1870 | 1900 | 1856          | 1900 | 1900 | 1900  | 1870     | 1811 | 1900 | 1900 | 1841 | 1885 |
| Adj Flow Rate, veh/h         | 131  | 0    | 125           | 1    | 0    | 1     | 63       | 411  | 0    | 0    | 618  | 94   |
| Peak Hour Factor             | 0.83 | 0.83 | 0.83          | 0.90 | 0.90 | 0.90  | 0.93     | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Percent Heavy Veh, %         | 2    | 0    | 3             | 0    | 0    | 0     | 2        | 6    | 0    | 0    | 4    | 1    |
| Cap, veh/h                   | 313  | 0    | 240           | 120  | 24   | 67    | 141      | 1328 | 0    | ō    | 1099 | 954  |
| Arrive On Green              | 0.15 | 0.00 | 0.15          | 0.15 | 0.00 | 0.15  | 0.08     | 0.73 | 0.00 | 0.00 | 0.60 | 0.60 |
| Sat Flow, veh/h              | 1375 | 0    | 1572          | 283  | 159  | 442   | 1781     | 1811 | 0.00 | 0.00 | 1841 | 1598 |
| Grp Volume(v), veh/h         | 131  | 0    | 125           | 2    | 0    | 0     | 63       | 411  | 0    | 0    | 618  | 94   |
| Grp Sat Flow(s), veh/h/in    | 1375 | ő    | 1572          | 884  | 0    | 0     | 1781     | 1811 | 0    | 0    | 1841 | 1598 |
| Q Serve(g_s), s              | 0.0  | 0.0  | 5.1           | 0.0  | 0.0  | 0.0   | 2,4      | 5.5  | 0.0  | 0.0  | 14.3 |      |
| Cycle Q Clear(g_c), s        | 6.5  | 0.0  | 5.1           | 6.5  | 0.0  | 0.0   | 2.4      | 5.5  | 0.0  | 0.0  | 14.3 | 1.8  |
| Prop In Lane                 | 1.00 | 0.0  | 1.00          | 0.50 | 0.0  | 0.50  | 1.00     | 5.5  | 0.00 | 0.00 | 14.3 | 1.8  |
| Lane Grp Cap(c), veh/h       | 313  | 0    | 240           | 212  | 0    | 0.50  | 141      | 1328 |      |      | 4000 | 1.00 |
| V/C Ratio(X)                 | 0.42 | 0.00 | 0.52          | 0.01 | 0.00 | 0.00  | 0.45     | 0.31 | 0.00 | 0    | 1099 | 954  |
| Avail Cap(c_a), veh/h        | 371  | 0.00 | 303           | 270  | 0.00 | 0.00  | 178      | 1328 |      | 0.00 | 0.56 | 0.10 |
| HCM Platoon Ratio            | 1.00 | 1.00 | 1.00          | 1.00 | 1.00 | 1.00  | 1.00     | 1.00 | 1.00 | 0    | 1099 | 954  |
| Upstream Filter(I)           | 1.00 | 0.00 | 1.00          | 1.00 | 0.00 | 0.00  | 1.00     | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh     | 27.9 | 0.0  | 27.3          | 25.3 | 0.00 | 0.00  | 30.8     | 3.2  | 0.00 | 0.00 | 1.00 | 1.00 |
| Incr Delay (d2), s/veh       | 0.9  | 0.0  | 1.7           | 0.0  | 0.0  | 0.0   | 2.2      |      | 0.0  | 0.0  | 8.6  | 6.0  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0  | 0.0           | 0.0  | 0.0  | 0.0   |          | 0.6  | 0.0  | 0.0  | 2.1  | 0.2  |
| %ile BackOfQ(50%),veh/ln     | 2.0  | 0.0  | 1.9           | 0.0  | 0.0  |       | 0.0      | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| Unsig. Movement Delay, s/veh | 2.0  | 0.0  | 1.9           | 0.0  | 0.0  | 0.0   | 1.1      | 1.3  | 0.0  | 0.0  | 5.0  | 0.5  |
|                              | 20.0 | 0.0  | 00.4          | 05.0 |      | 0.0   | 00.0     |      |      |      |      |      |
| LnGrp Delay(d),s/veh         | 28.8 | 0.0  | 29.1          | 25.3 | 0.0  | 0.0   | 33.0     | 3.8  | 0.0  | 0.0  | 10.6 | 6.2  |
| LnGrp LOS                    | C    | A    | C             | С    | A    | A     | <u>C</u> | A    | A    | A    | B    | A    |
| Approach Vol, veh/h          |      | 256  |               |      | 2    |       |          | 474  |      |      | 712  |      |
| Approach Delay, s/veh        |      | 28.9 |               |      | 25.3 |       |          | 7.7  |      |      | 10.1 |      |
| Approach LOS                 |      | С    |               |      | С    |       |          | Α    |      |      | В    |      |
| Timer - Assigned Phs         |      | 2    |               | 4    | 5    | 6     |          | 8    |      |      |      |      |
| Phs Duration (G+Y+Rc), s     |      | 55.8 |               | 14.2 | 9.5  | 46.3  |          | 14.2 |      |      |      |      |
| Change Period (Y+Rc), s      |      | 6.5  |               | 5.5  | 6.0  | * 6.5 |          | 5.5  |      |      |      |      |
| Max Green Setting (Gmax), s  |      | 46.5 |               | 11.5 | 5.0  | * 37  |          | 11.5 |      |      |      |      |
| Max Q Clear Time (g_c+i1), s |      | 7.5  |               | 8.5  | 4.4  | 16.3  |          | 8.5  |      |      |      |      |
| Green Ext Time (p_c), s      |      | 1.7  |               | 0.3  | 0.0  | 3.1   |          | 0.0  |      |      |      |      |
| Intersection Summary         |      |      |               |      |      |       |          |      |      |      |      |      |
| HCM 6th Ctrl Delay           |      |      | 12.7          |      |      |       |          |      |      |      |      |      |
| HCM 6th LOS                  |      |      | В             |      |      |       |          |      |      |      |      |      |
| Notes                        |      |      |               |      |      |       |          |      |      |      |      |      |

<sup>\*</sup> HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

**Timings** 

|                      | 1     |       | >     | •     | 4     | 4     | <b>†</b> | 1     | 4     |
|----------------------|-------|-------|-------|-------|-------|-------|----------|-------|-------|
| Lane Group           | EBL   | EBT   | EBR   | WBL   | WBT   | NBL   | NBT      | SBT   | SBR   |
| Lane Configurations  |       | र्ब   | 7     |       | 4     | , j   | 1>       | स     | 7     |
| Traffic Volume (vph) | 109   | 0     | 104   | 1     | 0     | 59    | 382      | 575   | 87    |
| Future Volume (vph)  | 109   | 0     | 104   | 1     | 0     | 59    | 382      | 575   | 87    |
| Turn Type            | Perm  | NA    | Perm  | Perm  | NA    | Prot  | NA       | NA    | Perm  |
| Protected Phases     |       | 4     |       |       | 8     | 5     | 2        | 6     |       |
| Permitted Phases     | 4     |       | 4     | 8     |       | -     | _        | •     | 6     |
| Detector Phase       | 4     | 4     | 4     | 8     | 8     | 5     | 2        | 6     | 6     |
| Switch Phase         |       |       |       |       |       | •     | _        | ·     | Ū     |
| Minimum Initial (s)  | 5.0   | 5.0   | 5.0   | 5.0   | 5.0   | 5.0   | 10.0     | 10.0  | 10.0  |
| Minimum Split (s)    | 16.0  | 16.0  | 16.0  | 16.0  | 16.0  | 11.0  | 16.5     | 16.0  | 16.0  |
| Total Split (s)      | 17.0  | 17.0  | 17.0  | 17.0  | 17.0  | 11.0  | 53.0     | 42.0  | 42.0  |
| Total Split (%)      | 24.3% | 24.3% | 24.3% | 24.3% | 24.3% | 15.7% | 75.7%    | 60.0% | 60.0% |
| Yellow Time (s)      | 3.0   | 3.0   | 3.0   | 3.0   | 3.0   | 3.5   | 3.5      | 3.5   | 3.5   |
| All-Red Time (s)     | 2.5   | 2.5   | 2.5   | 2.5   | 2.5   | 2.5   | 3.0      | 2.0   | 2.0   |
| Lost Time Adjust (s) |       | -2.0  | -2.0  |       | -2.0  | -2.0  | -2.0     | -2.0  | -2.0  |
| Total Lost Time (s)  |       | 3.5   | 3.5   |       | 3.5   | 4.0   | 4.5      | 3.5   | 3.5   |
| Lead/Lag             |       |       |       |       |       | Lead  |          | Lag   | Lag   |
| Lead-Lag Optimize?   |       |       |       |       |       | Yes   |          | Yes   | Yes   |
| Recall Mode          | None  | None  | None  | None  | None  | None  | C-Max    | C-Max | C-Max |
| Act Effct Green (s)  |       | 12.2  | 12.2  |       | 12.2  | 7.4   | 49.8     | 44.2  | 44.2  |
| Actuated g/C Ratio   |       | 0.17  | 0.17  |       | 0.17  | 0.11  | 0.71     | 0.63  | 0.63  |
| v/c Ratio            |       | 0.54  | 0.32  |       | 0.01  | 0.34  | 0.32     | 0.54  | 0.09  |
| Control Delay        |       | 34.6  | 5.9   |       | 0.0   | 34.6  | 4.8      | 11.1  | 1.0   |
| Queue Delay          |       | 0.0   | 0.0   |       | 0.0   | 0.0   | 0.0      | 0.0   | 0.0   |
| Total Delay          |       | 34.6  | 5.9   |       | 0.0   | 34.6  | 4.8      | 11.1  | 1.0   |
| LOS                  |       | С     | Α     |       | Α     | C     | Α        | В     | Α     |
| Approach Delay       |       | 20.6  |       |       | •     | _     | 8.8      | 9.8   | , ,   |
| Approach LOS         |       | С     |       |       |       |       | A        | A     |       |
| Intersection Summary |       |       |       |       |       |       |          |       |       |

Cycle Length: 70

Actuated Cycle Length: 70

Offset: 0 (0%), Referenced to phase 2:NBT and 6:SBTL, Start of Yellow

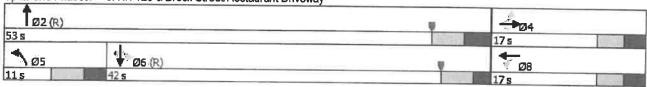
Natural Cycle: 60

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.54 Intersection Signal Delay: 11.3 Intersection Capacity Utilization 66.8%

Intersection LOS: B
ICU Level of Service C

Analysis Period (min) 15



|                         |      | *    | 4    | 4    | <b>†</b> | 1    | 1    |
|-------------------------|------|------|------|------|----------|------|------|
| Lane Group              | EBT  | EBR  | WBT  | NBL  | NBT      | SBT  | SBR  |
| Lane Group Flow (vph)   | 131  | 125  | 2    | 63   | 411      | 618  | 94   |
| v/c Ratio               | 0.54 | 0.32 | 0.01 | 0.34 | 0.32     | 0.54 | 0.09 |
| Control Delay           | 34.6 | 5.9  | 0.0  | 34.6 | 4.8      | 11.1 | 1.0  |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0      | 0.0  | 0.0  |
| Total Delay             | 34.6 | 5.9  | 0.0  | 34.6 | 4.8      | 11.1 | 1.0  |
| Queue Length 50th (ft)  | 51   | 0    | 0    | 26   | 58       | 166  | 0    |
| Queue Length 95th (ft)  | 92   | 24   | 0    | 61   | 94       | 264  | 10   |
| Internal Link Dist (ft) | 204  |      | 294  |      | 1001     | 1243 |      |
| Turn Bay Length (ft)    |      |      |      | 375  |          |      |      |
| Base Capacity (vph)     | 271  | 421  | 421  | 188  | 1275     | 1154 | 1058 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0        | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0        | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0        | 0    | 0    |
| Reduced v/c Ratio       | 0.48 | 0.30 | 0.00 | 0.34 | 0.32     | 0.54 | 0.09 |
| Intersection Summary    |      |      |      |      |          |      |      |

|                              | ۶    | $\rightarrow$ | *    | 1        | <b>←</b> | *     | 4    | <b>†</b>   | -    | 1    | 1    | 1    |
|------------------------------|------|---------------|------|----------|----------|-------|------|------------|------|------|------|------|
| Movement                     | EBL  | EBT           | EBR  | WBL      | WBT      | WBR   | NBL  | NBT        | NBR  | SBL  | SBT  | SBR  |
| Lane Configurations          |      | बी            | 7    |          | 4        |       | ħ    | 7>         |      |      | 4    | 7    |
| Traffic Volume (veh/h)       | 130  | Ō             | 119  | 1        | ō        | 1     | 70   | 466        | 0    | 0    | 701  | 105  |
| Future Volume (veh/h)        | 130  | 0             | 119  | 1        | 0        | 1     | 70   | 466        | Ō    | ő    | 701  | 105  |
| Initial Q (Qb), veh          | 0    | 0             | 0    | 0        | 0        | 0     | 0    | 0          | ŏ    | ő    | 0    | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |               | 1.00 | 1.00     |          | 1.00  | 1.00 | •          | 1.00 | 1.00 | v    | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00          | 1.00 | 1.00     | 1.00     | 1.00  | 1.00 | 1.00       | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach        |      | No            |      |          | No       |       |      | No         |      | 1.00 | No   | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1870 | 1900          | 1856 | 1900     | 1900     | 1900  | 1870 | 1811       | 1900 | 1900 | 1841 | 1885 |
| Adj Flow Rate, veh/h         | 157  | 0             | 143  | 1        | 0        | 1     | 75   | 501        | 0    | 0    | 754  | 113  |
| Peak Hour Factor             | 0.83 | 0.83          | 0.83 | 0.90     | 0.90     | 0.90  | 0.93 | 0.93       | 0.93 | 0.93 | 0.93 | 0.93 |
| Percent Heavy Veh, %         | 2    | 0             | 3    | 0        | 0        | 0     | 2    | 6          | 0.00 | 0.00 | 4    | 1    |
| Cap, veh/h                   | 322  | 0             | 281  | 112      | 25       | 59    | 149  | 1281       | ő    | 0    | 1043 | 905  |
| Arrive On Green              | 0.18 | 0.00          | 0.18 | 0.18     | 0.00     | 0.18  | 0.08 | 0.71       | 0.00 | 0.00 | 0.57 | 0.57 |
| Sat Flow, veh/h              | 1228 | 0             | 1572 | 193      | 138      | 331   | 1781 | 1811       | 0.00 | 0.00 | 1841 | 1598 |
| Grp Volume(v), veh/h         | 157  | 0             | 143  | 2        | 0        | 0     | 75   | 501        | 0    |      |      |      |
| Grp Sat Flow(s), veh/h/ln    | 1228 | 0             | 1572 | 662      | 0        | 0     | 1781 | 1811       |      | 0    | 754  | 113  |
| Q Serve(g_s), s              | 0.0  | 0.0           | 5.8  | 0.0      | 0.0      | 0.0   | 2.8  | 7.8        | 0    | 0    | 1841 | 1598 |
| Cycle Q Clear(g_c), s        | 9.1  | 0.0           | 5.8  | 9.1      | 0.0      | 0.0   | 2.8  | 7.0<br>7.8 | 0.0  | 0.0  | 21.0 | 2.3  |
| Prop In Lane                 | 1.00 | 0.0           | 1.00 | 0.50     | 0.0      | 0.50  | 1.00 | 1.0        | 0.0  | 0.0  | 21.0 | 2.3  |
| Lane Grp Cap(c), veh/h       | 322  | 0             | 281  | 195      | 0        |       | 1.00 | 4004       | 0.00 | 0.00 |      | 1.00 |
| V/C Ratio(X)                 | 0.49 | 0.00          | 0.51 | 0.01     | 0.00     | 0.00  |      | 1281       | 0    | 0    | 1043 | 905  |
| Avail Cap(c_a), veh/h        | 322  | 0.00          | 281  | 195      |          |       | 0.50 | 0.39       | 0.00 | 0.00 | 0.72 | 0.12 |
| HCM Platoon Ratio            | 1.00 | 1.00          | 1.00 | 1.00     | 1.00     | 1.00  | 178  | 1281       | 0    | 0    | 1043 | 905  |
| Upstream Filter(I)           | 1.00 | 0.00          | 1.00 | 1.00     | 1.00     | 1.00  | 1.00 | 1.00       | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh     | 27.4 | 0.00          | 26.0 |          | 0.00     | 0.00  | 1.00 | 1.00       | 0.00 | 0.00 | 1.00 | 1.00 |
| Incr Delay (d2), s/veh       | 1.1  | 0.0           |      | 24.0     | 0.0      | 0.0   | 30.7 | 4.1        | 0.0  | 0.0  | 11.1 | 7.1  |
| Initial Q Delay(d3),s/veh    | 0.0  |               | 1.5  | 0.0      | 0.0      | 0.0   | 2.6  | 0.9        | 0.0  | 0.0  | 4.4  | 0.3  |
|                              |      | 0.0           | 0.0  | 0.0      | 0.0      | 0.0   | 0.0  | 0.0        | 0.0  | 0.0  | 0.0  | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 2.4  | 0.0           | 2.1  | 0.0      | 0.0      | 0.0   | 1.3  | 2.1        | 0.0  | 0.0  | 8.1  | 0.7  |
| Unsig. Movement Delay, s/veh | 00.5 |               |      |          |          |       |      |            |      |      |      |      |
| LnGrp Delay(d),s/veh         | 28.5 | 0.0           | 27.5 | 24.0     | 0.0      | 0.0   | 33.3 | 5.0        | 0.0  | 0.0  | 15.5 | 7.4  |
| LnGrp LOS                    | C    | Α             | C    | <u>C</u> | A        | A     | C_   | A          | A    | A    | В    | A    |
| Approach Vol, veh/h          |      | 300           |      |          | 2        |       |      | 576        |      |      | 867  |      |
| Approach Delay, s/veh        |      | 28.0          |      |          | 24.0     |       |      | 8.7        |      |      | 14.4 |      |
| Approach LOS                 |      | С             |      |          | С        |       |      | Α          |      |      | В    |      |
| Timer - Assigned Phs         |      | 2             |      | 4        | 5        | 6     |      | 8          |      |      |      |      |
| Phs Duration (G+Y+Rc), s     |      | 54.0          |      | 16.0     | 9.8      | 44.2  |      | 16.0       |      |      |      |      |
| Change Period (Y+Rc), s      |      | 6.5           |      | 5.5      | 6.0      | * 6.5 |      | 5.5        |      |      |      |      |
| Max Green Setting (Gmax), s  |      | 47.5          |      | 10.5     | 5.0      | * 38  |      | 10.5       |      |      |      |      |
| Max Q Clear Time (g_c+l1), s |      | 9.8           |      | 11.1     | 4.8      | 23.0  |      | 11.1       |      |      |      |      |
| Green Ext Time (p_c), s      |      | 2.2           |      | 0.0      | 0.0      | 3.6   |      | 0.0        |      |      |      |      |
| ntersection Summary          |      |               |      |          |          |       |      |            |      |      |      |      |
| HCM 6th Ctrl Delay           |      |               | 14.9 |          |          |       |      |            |      |      |      |      |
| HCM 6th LOS                  |      |               | В    |          |          |       |      |            |      |      |      |      |
| Notes                        |      |               |      |          |          |       |      |            |      |      |      |      |

<sup>\*</sup> HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

**Timings** 

|                      | *     | <b>→</b> | *     | 1     | -     | 4     | †     | ļ     | 1     |
|----------------------|-------|----------|-------|-------|-------|-------|-------|-------|-------|
| Lane Group           | EBL.  | EBT      | EBR   | WBL   | WBT   | NBL   | NBT   | SBT   | SBR   |
| Lane Configurations  |       | 4        | 7     |       | 4     | 7     | P     | र्स   | 7     |
| Traffic Volume (vph) | 130   | 0        | 119   | 1     | Ō     | 70    | 466   | 701   | 105   |
| Future Volume (vph)  | 130   | 0        | 119   | 1     | 0     | 70    | 466   | 701   | 105   |
| Turn Type            | Perm  | NA       | Perm  | Perm  | NA    | Prot  | NA    | NA    | Perm  |
| Protected Phases     |       | 4        |       |       | 8     | 5     | 2     | 6     |       |
| Permitted Phases     | 4     |          | 4     | 8     |       |       |       | _     | 6     |
| Detector Phase       | 4     | 4        | 4     | 8     | 8     | 5     | 2     | 6     | 6     |
| Switch Phase         |       |          |       |       |       |       |       |       | •     |
| Minimum Initial (s)  | 5,0   | 5.0      | 5.0   | 5.0   | 5.0   | 5.0   | 10.0  | 10.0  | 10.0  |
| Minimum Split (s)    | 16.0  | 16.0     | 16.0  | 16.0  | 16.0  | 11.0  | 16.5  | 16.0  | 16.0  |
| Total Split (s)      | 16.0  | 16.0     | 16.0  | 16.0  | 16.0  | 11.0  | 54.0  | 43.0  | 43.0  |
| Total Split (%)      | 22.9% | 22.9%    | 22.9% | 22.9% | 22.9% | 15.7% | 77.1% | 61.4% | 61.4% |
| Yellow Time (s)      | 3.0   | 3.0      | 3.0   | 3.0   | 3.0   | 3.5   | 3.5   | 3.5   | 3.5   |
| All-Red Time (s)     | 2.5   | 2.5      | 2.5   | 2.5   | 2.5   | 2.5   | 3.0   | 2.0   | 2.0   |
| Lost Time Adjust (s) |       | -2.0     | -2.0  |       | -2.0  | -2.0  | -2.0  | -2.0  | -2.0  |
| Total Lost Time (s)  |       | 3.5      | 3.5   |       | 3.5   | 4.0   | 4.5   | 3.5   | 3.5   |
| Lead/Lag             |       |          |       |       |       | Lead  |       | Lag   | Lag   |
| Lead-Lag Optimize?   |       |          |       |       |       | Yes   |       | Yes   | Yes   |
| Recall Mode          | None  | None     | None  | None  | None  | None  | C-Max | C-Max | C-Max |
| Act Effct Green (s)  |       | 11.9     | 11.9  |       | 11.9  | 7.1   | 50.1  | 42.3  | 42.3  |
| Actuated g/C Ratio   |       | 0.17     | 0.17  |       | 0.17  | 0.10  | 0.72  | 0.60  | 0.60  |
| v/c Ratio            |       | 0.65     | 0.37  |       | 0.01  | 0.42  | 0.39  | 0.68  | 0.11  |
| Control Delay        |       | 41.4     | 7.8   |       | 0.0   | 37.3  | 5.1   | 14.6  | 1.4   |
| Queue Delay          |       | 0.0      | 0.0   |       | 0.0   | 0.0   | 0.0   | 0.0   | 0.0   |
| Total Delay          |       | 41.4     | 7.8   |       | 0.0   | 37.3  | 5.1   | 14.6  | 1.4   |
| LOS                  |       | D        | Α     |       | Α     | D     | Α     | В     | Α     |
| Approach Delay       |       | 25.4     |       |       |       |       | 9.3   | 12.9  |       |
| Approach LOS         |       | С        |       |       |       |       | Α     | В     |       |
| Intersection Summary |       |          |       |       |       |       |       |       |       |

Cycle Length: 70

Actuated Cycle Length: 70

Offset: 0 (0%), Referenced to phase 2:NBT and 6:SBTL, Start of Yellow

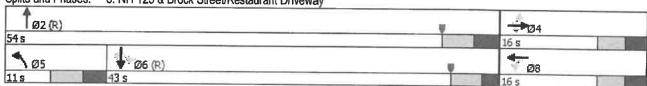
Natural Cycle: 60

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.68 Intersection Signal Delay: 13.9 Intersection Capacity Utilization 78.0%

Intersection LOS: B
ICU Level of Service D

Analysis Period (min) 15



|                         |      | 7    | <b>←</b> | 1    | 1    | Ţ    | 1    |
|-------------------------|------|------|----------|------|------|------|------|
| Lane Group              | EBT  | EBR  | WBT      | NBL  | NBT  | SBT  | SBR  |
| Lane Group Flow (vph)   | 157  | 143  | 2        | 75   | 501  | 754  | 113  |
| v/c Ratio               | 0.65 | 0.37 | 0.01     | 0.42 | 0.39 | 0.68 | 0.11 |
| Control Delay           | 41.4 | 7.8  | 0.0      | 37.3 | 5.1  | 14.6 | 1.4  |
| Queue Delay             | 0.0  | 0.0  | 0.0      | 0.0  | 0.0  | 0.0  | 0.0  |
| Total Delay             | 41.4 | 7.8  | 0.0      | 37.3 | 5.1  | 14.6 | 1.4  |
| Queue Length 50th (ft)  | 63   | 0    | 0        | 31   | 70   | 219  | 0    |
| Queue Length 95th (ft)  | #111 | 33   | 0        | 69   | 113  | 353  | 15   |
| Internal Link Dist (ft) | 204  |      | 294      |      | 1001 | 1243 |      |
| Turn Bay Length (ft)    |      |      |          | 375  |      |      |      |
| Base Capacity (vph)     | 251  | 401  | 398      | 179  | 1281 | 1102 | 1017 |
| Starvation Cap Reductn  | 0    | 0    | 0        | 0    | 0    | 0    | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0        | 0    | 0    | 0    | 0    |
| Storage Cap Reductn     | 0    | 0    | 0        | 0    | 0    | 0    | 0    |
| Reduced v/c Ratio       | 0.63 | 0.36 | 0.01     | 0.42 | 0.39 | 0.68 | 0.11 |
| Intersection Summary    |      |      |          |      |      |      |      |

<sup># 95</sup>th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

|                              | ۶    | -    | *        | 1    | 4-   | *          | 1    | <b>†</b> | -    | 1    | <b></b>      | 1    |
|------------------------------|------|------|----------|------|------|------------|------|----------|------|------|--------------|------|
| Movement                     | EBL  | EBT  | EBR      | WBL  | WBT  | WBR        | NBL  | NBT      | NBR  | SBL  | SBT          | SBR  |
| Lane Configurations          |      | र्न  | 7        |      | 4    |            | 7    | 7>       |      |      | 4            | 7    |
| Traffic Volume (veh/h)       | 148  | 5    | 67       | 4    | 3    | 6          | 102  | 579      | 0    | 2    | 650          | 180  |
| Future Volume (veh/h)        | 148  | 5    | 67       | 4    | 3    | 6          | 102  | 579      | Õ    | 2    | 650          | 180  |
| Initial Q (Qb), veh          | 0    | 0    | 0        | 0    | 0    | 0          | 0    | 0        | Ö    | ō    | 0            | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |      | 1.00     | 1.00 |      | 1.00       | 1.00 | _        | 1.00 | 1.00 | Ŭ            | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00 | 1.00     | 1.00 | 1.00 | 1.00       | 1.00 | 1.00     | 1.00 | 1.00 | 1.00         | 1.00 |
| Work Zone On Approach        |      | No   |          |      | No   |            |      | No       |      | 1.00 | No           | 1.00 |
| Adj Sat Flow, veh/h/ln       | 1900 | 1900 | 1900     | 1900 | 1900 | 1900       | 1885 | 1885     | 1900 | 1900 | 1885         | 1870 |
| Adj Flow Rate, veh/h         | 156  | 5    | 71       | 4    | 3    | 7          | 113  | 643      | 0    | 2    | 670          | 186  |
| Peak Hour Factor             | 0.95 | 0.95 | 0.95     | 0.90 | 0.90 | 0.90       | 0.90 | 0.90     | 0.90 | 0.97 | 0.97         | 0.97 |
| Percent Heavy Veh, %         | 0    | 0    | 0        | 0    | 0.00 | 0.00       | 1    | 1        | 0.30 | 0.37 | 0. <i>51</i> | 0.97 |
| Cap, veh/h                   | 295  | 6    | 325      | 84   | 69   | 79         | 199  | 1262     | 0    | 59   | 929          |      |
| Arrive On Green              | 0.20 | 0.20 | 0.20     | 0.20 | 0.20 | 0.20       | 0.11 | 0.67     | 0.00 | 0.49 | 0.49         | 783  |
| Sat Flow, veh/h              | 894  | 29   | 1610     | 48   | 342  | 390        | 1795 | 1885     | 0.00 |      |              | 0.49 |
| Grp Volume(v), veh/h         | 161  | 0    | 71       | 14   | 0    | 0          | 113  | 643      |      | 1    | 1883         | 1585 |
| Grp Sat Flow(s), veh/h/in    | 922  | 0    | 1610     | 781  | 0    |            |      |          | 0    | 672  | 0            | 186  |
| Q Serve(g_s), s              | 0.2  | 0.0  | 2.3      | 0.1  | 0.0  | 0          | 1795 | 1885     | 0    | 1884 | 0            | 1585 |
| Cycle Q Clear(g_c), s        | 11.3 | 0.0  | 2.3      | 11.2 | 0.0  | 0.0<br>0.0 | 3.7  | 10.6     | 0.0  | 0.0  | 0.0          | 4.2  |
| Prop in Lane                 | 0.97 | 0.0  | 1.00     | 0.29 | 0.0  |            | 3.7  | 10.6     | 0.0  | 17.4 | 0.0          | 4.2  |
| Lane Grp Cap(c), veh/h       | 300  | 0    | 325      | 232  | 0    | 0.50       | 1.00 | 4000     | 0.00 | 0.00 | _            | 1.00 |
| V/C Ratio(X)                 | 0.54 | 0.00 | 0.22     |      | 0    | 0          | 199  | 1262     | 0    | 988  | 0            | 783  |
| Avail Cap(c_a), veh/h        | 300  | 0.00 | 325      | 0.06 | 0.00 | 0.00       | 0.57 | 0.51     | 0.00 | 0.68 | 0.00         | 0.24 |
| HCM Platoon Ratio            | 1.00 | 1.00 |          | 232  | 0    | 0          | 203  | 1262     | 0    | 1015 | 0            | 805  |
| Upstream Filter(I)           | 1.00 |      | 1.00     | 1.00 | 1,00 | 1.00       | 1.00 | 1.00     | 1.00 | 1.00 | 1.00         | 1.00 |
| Uniform Delay (d), s/veh     | 24.3 | 0.00 | 1.00     | 1.00 | 0.00 | 0.00       | 1.00 | 1.00     | 0.00 | 1.00 | 0.00         | 1.00 |
|                              |      | 0.0  | 20.7     | 20.3 | 0.0  | 0.0        | 26.1 | 5.1      | 0.0  | 12.3 | 0.0          | 9.0  |
| Incr Delay (d2), s/veh       | 1.9  | 0.0  | 0.3      | 0.1  | 0.0  | 0.0        | 3.5  | 1.5      | 0.0  | 3.8  | 0.0          | 0.7  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0  | 0.0      | 0.0  | 0.0  | 0.0        | 0.0  | 0.0      | 0.0  | 0.0  | 0.0          | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 2.3  | 0.0  | 8.0      | 0.2  | 0.0  | 0.0        | 1.7  | 3.0      | 0.0  | 6.9  | 0.0          | 1.3  |
| Unsig. Movement Delay, s/veh |      |      |          |      |      |            |      |          |      |      |              |      |
| LnGrp Delay(d),s/veh         | 26.2 | 0.0  | 21.0     | 20.4 | 0.0  | 0.0        | 29.7 | 6.6      | 0.0  | 16.1 | 0.0          | 9.7  |
| LnGrp LOS                    | С    | A    | <u>C</u> | C    | A    | A          | С    | A        | A    | В    | Α            | A    |
| Approach Vol, veh/h          |      | 232  |          |      | 14   |            |      | 756      |      |      | 858          |      |
| Approach Delay, s/veh        |      | 24.6 |          |      | 20.4 |            |      | 10.1     |      |      | 14.7         |      |
| Approach LOS                 |      | С    |          |      | C    |            |      | В        |      |      | В            |      |
| Timer - Assigned Phs         |      | 2    |          | 4    | 5    | 6          |      | 8        |      |      |              |      |
| Phs Duration (G+Y+Rc), s     |      | 46.0 |          | 16.0 | 10.9 | 35.1       |      | 16.0     |      |      |              |      |
| Change Period (Y+Rc), s      |      | 6.5  |          | 5.5  | 6.0  | * 6.5      |      | 5.5      |      |      |              |      |
| Max Green Setting (Gmax), s  |      | 39.5 |          | 10.5 | 5.0  | * 30       |      | 10.5     |      |      |              |      |
| Max Q Clear Time (g_c+I1), s |      | 12.6 |          | 13.3 | 5.7  | 19.4       |      | 13.2     |      |      |              |      |
| Green Ext Time (p_c), s      |      | 2.9  |          | 0.0  | 0.0  | 2.9        |      | 0.0      |      |      |              |      |
| ntersection Summary          |      |      |          |      |      |            |      |          |      |      |              |      |
| HCM 6th Ctrl Delay           |      |      | 14.1     |      |      |            |      |          |      |      |              |      |
| HCM 6th LOS                  |      |      | В        |      |      |            |      |          |      |      |              |      |
| Notes                        |      |      |          |      |      |            |      |          |      |      |              |      |

<sup>\*</sup> HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

**Timings** 

|                      | 1     | <b>→</b> | 7     | •     | -     | 4     | †     | 1     | <b>+</b> | 4     |  |
|----------------------|-------|----------|-------|-------|-------|-------|-------|-------|----------|-------|--|
| Lane Group           | EBL   | EBT      | EBR   | WBL   | WBT   | NBL   | NBT   | SBL   | SBT      | SBR   |  |
| Lane Configurations  |       | र्न      | 7     |       | 4     | 7     | 4     |       | र्स      | 77    |  |
| Traffic Volume (vph) | 148   | 5        | 67    | 4     | 3     | 102   | 579   | 2     | 650      | 180   |  |
| Future Volume (vph)  | 148   | 5        | 67    | 4     | 3     | 102   | 579   | 2     | 650      | 180   |  |
| Turn Type            | Perm  | NA       | Perm  | Perm  | NA    | Prot  | NA    | Perm  | NA       | Perm  |  |
| Protected Phases     |       | 4        |       |       | 8     | 5     | 2     |       | 6        |       |  |
| Permitted Phases     | 4     |          | 4     | 8     |       |       |       | 6     |          | 6     |  |
| Detector Phase       | 4     | 4        | 4     | 8     | 8     | 5     | 2     | 6     | 6        | 6     |  |
| Switch Phase         |       |          |       |       |       |       |       |       | _        | _     |  |
| Minimum Initial (s)  | 5.0   | 5.0      | 5.0   | 5.0   | 5.0   | 5.0   | 10.0  | 10.0  | 10.0     | 10.0  |  |
| Minimum Split (s)    | 16.0  | 16.0     | 16.0  | 16.0  | 16.0  | 11.0  | 16.5  | 16.0  | 16.0     | 16.0  |  |
| Total Split (s)      | 16.0  | 16.0     | 16.0  | 16.0  | 16.0  | 11.0  | 46.0  | 35.0  | 35.0     | 35.0  |  |
| Total Split (%)      | 25.8% | 25.8%    | 25.8% | 25.8% | 25.8% | 17.7% | 74.2% | 56.5% | 56.5%    | 56.5% |  |
| Yellow Time (s)      | 3.0   | 3.0      | 3.0   | 3.0   | 3.0   | 3.5   | 3.5   | 3.5   | 3.5      | 3.5   |  |
| All-Red Time (s)     | 2.5   | 2.5      | 2.5   | 2.5   | 2.5   | 2.5   | 3.0   | 2.0   | 2.0      | 2.0   |  |
| Lost Time Adjust (s) |       | -2.0     | -2.0  |       | -2.0  | -2.0  | -2.0  |       | -2.0     | -2.0  |  |
| Total Lost Time (s)  |       | 3.5      | 3.5   |       | 3.5   | 4.0   | 4.5   |       | 3.5      | 3.5   |  |
| Lead/Lag             |       |          |       |       |       | Lead  |       | Lag   | Lag      | Lag   |  |
| Lead-Lag Optimize?   |       |          |       |       |       | Yes   |       | Yes   | Yes      | Yes   |  |
| Recall Mode          | None  | None     | None  | None  | None  | None  | C-Min | C-Min | C-Min    | C-Min |  |
| Act Effct Green (s)  |       | 12.0     | 12.0  |       | 11.7  | 7.8   | 45.4  |       | 36.8     | 36.8  |  |
| Actuated g/C Ratio   |       | 0.19     | 0.19  |       | 0.19  | 0.13  | 0.73  |       | 0.59     | 0.59  |  |
| v/c Ratio            |       | 0.61     | 0.16  |       | 0.05  | 0.51  | 0.47  |       | 0.60     | 0.18  |  |
| Control Delay        |       | 33.4     | 0.8   |       | 15.9  | 35.2  | 6.1   |       | 14.1     | 2.0   |  |
| Queue Delay          |       | 0.0      | 0.0   |       | 0.0   | 0.0   | 0.0   |       | 0.0      | 0.0   |  |
| Total Delay          |       | 33.4     | 0.8   |       | 15.9  | 35.2  | 6.1   |       | 14.1     | 2.0   |  |
| LOS                  |       | С        | Α     |       | В     | D     | Α     |       | В        | A     |  |
| Approach Delay       |       | 23.4     |       |       | 15.9  |       | 10.5  |       | 11.5     | •••   |  |
| Approach LOS         |       | С        |       |       | В     |       | В     |       | В        |       |  |
| Intersection Summary |       |          |       |       |       |       |       |       |          |       |  |

Cycle Length: 62

Actuated Cycle Length: 62

Offset: 0 (0%), Referenced to phase 2:NBT and 6:SBTL, Start of Yellow

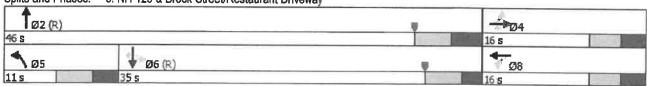
Natural Cycle: 60

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.61 Intersection Signal Delay: 12.6 Intersection Capacity Utilization 90.3%

Intersection LOS: B
ICU Level of Service E

Analysis Period (min) 15



|                         | -    | *    | -    | 1    | †    | <b>↓</b> | 1    |
|-------------------------|------|------|------|------|------|----------|------|
| Lane Group              | EBT  | EBR  | WBT  | NBL  | NBT  | SBT      | SBR  |
| Lane Group Flow (vph)   | 161  | 71   | 14   | 113  | 643  | 672      | 186  |
| v/c Ratio               | 0.61 | 0.16 | 0.05 | 0.51 | 0.47 | 0.60     | 0.18 |
| Control Delay           | 33.4 | 8.0  | 15.9 | 35.2 | 6.1  | 14.1     | 2.0  |
| Queue Delay             | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0      | 0.0  |
| Total Delay             | 33.4 | 8.0  | 15.9 | 35.2 | 6.1  | 14.1     | 2.0  |
| Queue Length 50th (ft)  | 54   | 0    | 2    | 41   | 106  | 186      | 0    |
| Queue Length 95th (ft)  | #121 | 0    | 15   | #97  | 162  | 292      | 25   |
| Internal Link Dist (ft) | 204  |      | 294  |      | 1001 | 1243     |      |
| Turn Bay Length (ft)    |      |      |      | 375  |      |          |      |
| Base Capacity (vph)     | 282  | 463  | 333  | 223  | 1385 | 1139     | 1033 |
| Starvation Cap Reductn  | 0    | 0    | 0    | 0    | 0    | 0        | 0    |
| Spillback Cap Reductn   | 0    | 0    | 0    | 0    | 0    | 0        | 0    |
| Storage Cap Reductn     | 0    | 0    | 0    | 0    | 0    | 0        | 0    |
| Reduced v/c Ratio       | 0.57 | 0.15 | 0.04 | 0.51 | 0.46 | 0.59     | 0.18 |
| Intersection Summary    |      |      |      |      |      |          |      |

<sup># 95</sup>th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

|                                   | ۶         | $\rightarrow$ | *         | 1    | 4-   | 4     | 1    | †    | 1         | 1    | Ţ    | 1    |
|-----------------------------------|-----------|---------------|-----------|------|------|-------|------|------|-----------|------|------|------|
| Movement                          | EBL       | EBT           | EBR       | WBL  | WBT  | WBR   | NBL  | NBT  | NBR       | SBL  | SBT  | SBR  |
| Lane Configurations               |           | ની            | ř         |      | 4    |       | ሻ    | 1>   |           |      | र्स  | 7    |
| Traffic Volume (veh/h)            | 155       | 5             | 70        | 4    | 3    | 6     | 107  | 608  | 0         | 2    | 683  | 189  |
| Future Volume (veh/h)             | 155       | 5             | 70        | 4    | 3    | 6     | 107  | 608  | 0         | 2    | 683  | 189  |
| Initial Q (Qb), veh               | 0         | 0             | 0         | 0    | 0    | 0     | 0    | 0    | 0         | 0    | 0    | 0    |
| Ped-Bike Adj(A_pbT)               | 1.00      |               | 1.00      | 1.00 |      | 1.00  | 1.00 |      | 1.00      | 1.00 |      | 1.00 |
| Parking Bus, Adj                  | 1.00      | 1.00          | 1.00      | 1.00 | 1.00 | 1.00  | 1.00 | 1.00 | 1.00      | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach             |           | No            |           |      | No   |       |      | No   |           |      | No   |      |
| Adj Sat Flow, veh/h/in            | 1900      | 1900          | 1900      | 1900 | 1900 | 1900  | 1885 | 1885 | 1900      | 1900 | 1885 | 1870 |
| Adj Flow Rate, veh/h              | 163       | 5             | 74        | 4    | 3    | 7     | 119  | 676  | 0         | 2    | 704  | 195  |
| Peak Hour Factor                  | 0.95      | 0.95          | 0.95      | 0.90 | 0.90 | 0.90  | 0.90 | 0.90 | 0.90      | 0.97 | 0.97 | 0.97 |
| Percent Heavy Veh, %              | 0         | 0             | 0         | 0    | 0    | 0     | 1    | 1    | 0         | 0    | 1    | 2    |
| Cap, veh/h                        | 272       | 5             | 325       | 75   | 62   | 62    | 203  | 1262 | 0         | 59   | 926  | 780  |
| Arrive On Green                   | 0.20      | 0.20          | 0.20      | 0.20 | 0.20 | 0.20  | 0.11 | 0.67 | 0.00      | 0.49 | 0.49 | 0.49 |
| Sat Flow, veh/h                   | 780       | 24            | 1610      | 0    | 306  | 307   | 1795 | 1885 | 0.00      | 1    | 1883 | 1585 |
| Grp Volume(v), veh/h              | 168       | 0             | 74        | 14   | 0    | 0     | 119  | 676  | 0         | 706  | 0    | 195  |
| Grp Sat Flow(s), veh/h/ln         | 804       | Ö             | 1610      | 613  | ő    | ő     | 1795 | 1885 | 0         | 1884 | 0    |      |
| Q Serve(g_s), s                   | 0.0       | 0.0           | 2.4       | 0.0  | 0.0  | 0.0   | 3.9  | 11.5 | 0.0       | 0.0  | 0.0  | 1585 |
| Cycle Q Clear(g_c), s             | 12.5      | 0.0           | 2.4       | 12.5 | 0.0  | 0.0   | 3.9  | 11.5 | 0.0       | 18.9 | 0.0  | 4.4  |
| Prop in Lane                      | 0.97      | 0.0           | 1.00      | 0.29 | 0.0  | 0.50  | 1.00 | 11.5 | 0.00      | 0.00 | 0.0  | 4.4  |
| Lane Grp Cap(c), veh/h            | 277       | 0             | 325       | 198  | 0    | 0.50  | 203  | 1262 | 0.00      | 985  | 0    | 1.00 |
| V/C Ratio(X)                      | 0.61      | 0.00          | 0.23      | 0.07 | 0.00 | 0.00  | 0.59 | 0.54 | 0.00      | 0.72 | 0    | 780  |
| Avail Cap(c_a), veh/h             | 277       | 0.00          | 325       | 198  | 0.00 | 0.00  | 203  | 1262 |           |      | 0.00 | 0.25 |
| HCM Platoon Ratio                 | 1.00      | 1.00          | 1.00      | 1.00 | 1.00 | 1.00  | 1.00 | 1.00 | 0<br>1.00 | 1015 | 0    | 805  |
| Upstream Filter(I)                | 1.00      | 0.00          | 1.00      | 1.00 | 0.00 | 0.00  | 1.00 | 1.00 | 0.00      | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh          | 25.0      | 0.0           | 20.7      | 20.5 | 0.0  | 0.0   | 26.1 | 5.3  | 0.0       | 1.00 | 0.00 | 1.00 |
| Incr Delay (d2), s/veh            | 3.8       | 0.0           | 0.4       | 0.1  | 0.0  | 0.0   | 4.3  | 1.6  |           | 12.8 | 0.0  | 9.1  |
| Initial Q Delay(d3),s/veh         | 0.0       | 0.0           | 0.0       | 0.0  | 0.0  | 0.0   | 0.0  |      | 0.0       | 4.5  | 0.0  | 0.8  |
| %ile BackOfQ(50%),veh/ln          | 2.6       | 0.0           | 0.0       | 0.0  | 0.0  | 0.0   | 1.8  | 0.0  | 0.0       | 0.0  | 0.0  | 0.0  |
| Unsig. Movement Delay, s/veh      | 2.0       | 0.0           | 0.9       | 0.2  | 0.0  | 0.0   | 1.0  | 3.3  | 0.0       | 7.6  | 0.0  | 1.4  |
|                                   | 20.0      | 0.0           | 24.4      | 00.0 | 0.0  | 0.0   | 00.5 |      |           |      |      |      |
| LnGrp Delay(d),s/veh<br>LnGrp LOS | 28.8<br>C | 0.0           | 21.1<br>C | 20.6 | 0.0  | 0.0   | 30.5 | 6.9  | 0.0       | 17.3 | 0.0  | 9.9  |
|                                   | U         | Α             | <u> </u>  | C    | A    | A     | С    | A    | A         | B    | Α    | A    |
| Approach Vol, veh/h               |           | 242           |           |      | 14   |       |      | 795  |           |      | 901  |      |
| Approach Delay, s/veh             |           | 26.4          |           |      | 20.6 |       |      | 10.4 |           |      | 15.7 |      |
| Approach LOS                      |           | С             |           |      | C    |       |      | В    |           |      | В    |      |
| Timer - Assigned Phs              |           | 2             |           | 4    | 5    | 6     |      | 8    |           |      |      |      |
| Phs Duration (G+Y+Rc), s          |           | 46.0          |           | 16.0 | 11.0 | 35.0  |      | 16.0 |           |      |      |      |
| Change Period (Y+Rc), s           |           | 6.5           |           | 5.5  | 6.0  | * 6.5 |      | 5.5  |           |      |      |      |
| Max Green Setting (Gmax), s       |           | 39.5          |           | 10.5 | 5.0  | * 30  |      | 10.5 |           |      |      |      |
| Max Q Clear Time (g_c+l1), s      |           | 13.5          |           | 14.5 | 5.9  | 20.9  |      | 14.5 |           |      |      |      |
| Green Ext Time (p_c), s           |           | 3,1           |           | 0.0  | 0.0  | 2.8   |      | 0.0  |           |      |      |      |
| ntersection Summary               |           |               |           |      |      |       |      |      |           |      |      |      |
| HCM 6th Ctrl Delay                |           |               | 14.9      |      |      |       |      |      |           |      |      |      |
| HCM 6th LOS                       |           |               | В         |      |      |       |      |      |           |      |      |      |
| Notes                             |           |               |           |      |      |       |      |      |           |      |      |      |

<sup>\*</sup> HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

#### **Timings**

#### 3: NH 125 & Brock Street/Restaurant Driveway

|                      | ۶     | <b>-</b> | *     | 1     | -     | 4     | †     | 6     | 1     | 4     |  |
|----------------------|-------|----------|-------|-------|-------|-------|-------|-------|-------|-------|--|
| Lane Group           | EBL   | EBT      | EBR   | WBL   | WBT   | NBL   | NBT   | SBL   | SBT   | SBR   |  |
| Lane Configurations  |       | सी       | 7     |       | 4     | 76    | 1>    |       | न     | 7     |  |
| Traffic Volume (vph) | 155   | 5        | 70    | 4     | 3     | 107   | 608   | 2     | 683   | 189   |  |
| Future Volume (vph)  | 155   | 5        | 70    | 4     | 3     | 107   | 608   | 2     | 683   | 189   |  |
| Turn Type            | Perm  | NA       | Perm  | Perm  | NA    | Prot  | NA    | Perm  | NA    | Perm  |  |
| Protected Phases     |       | 4        |       |       | 8     | 5     | 2     |       | 6     |       |  |
| Permitted Phases     | 4     |          | 4     | 8     |       |       |       | 6     |       | 6     |  |
| Detector Phase       | 4     | 4        | 4     | 8     | 8     | 5     | 2     | 6     | 6     | 6     |  |
| Switch Phase         |       |          |       |       |       |       |       |       |       | _     |  |
| Minimum Initial (s)  | 5.0   | 5.0      | 5.0   | 5.0   | 5.0   | 5.0   | 10.0  | 10.0  | 10.0  | 10.0  |  |
| Minimum Split (s)    | 16.0  | 16.0     | 16.0  | 16.0  | 16.0  | 11.0  | 16.5  | 16.0  | 16.0  | 16.0  |  |
| Total Split (s)      | 16.0  | 16.0     | 16.0  | 16.0  | 16.0  | 11.0  | 46.0  | 35.0  | 35.0  | 35.0  |  |
| Total Split (%)      | 25.8% | 25.8%    | 25.8% | 25.8% | 25.8% | 17.7% | 74.2% | 56.5% | 56.5% | 56.5% |  |
| Yellow Time (s)      | 3.0   | 3.0      | 3.0   | 3.0   | 3.0   | 3.5   | 3.5   | 3.5   | 3.5   | 3.5   |  |
| All-Red Time (s)     | 2.5   | 2.5      | 2.5   | 2.5   | 2.5   | 2.5   | 3.0   | 2.0   | 2.0   | 2.0   |  |
| Lost Time Adjust (s) |       | -2.0     | -2.0  |       | -2.0  | -2.0  | -2.0  |       | -2.0  | -2.0  |  |
| Total Lost Time (s)  |       | 3.5      | 3.5   |       | 3.5   | 4.0   | 4.5   |       | 3.5   | 3.5   |  |
| Lead/Lag             |       |          |       |       |       | Lead  |       | Lag   | Lag   | Lag   |  |
| Lead-Lag Optimize?   |       |          |       |       |       | Yes   |       | Yes   | Yes   | Yes   |  |
| Recall Mode          | None  | None     | None  | None  | None  | None  | C-Min | C-Min | C-Min | C-Min |  |
| Act Effct Green (s)  |       | 12.0     | 12.0  |       | 12.0  | 7.8   | 42.0  |       | 33.6  | 33.6  |  |
| Actuated g/C Ratio   |       | 0.19     | 0.19  |       | 0.19  | 0.13  | 0.68  |       | 0.54  | 0.54  |  |
| v/c Ratio            |       | 0.63     | 0.17  |       | 0.04  | 0.53  | 0.53  |       | 0.69  | 0.21  |  |
| Control Delay        |       | 35.2     | 8.0   |       | 15.9  | 36.3  | 7.1   |       | 16.4  | 2.1   |  |
| Queue Delay          |       | 0.0      | 0.0   |       | 0.0   | 0.0   | 0.0   |       | 0.0   | 0.0   |  |
| Total Delay          |       | 35.2     | 0.8   |       | 15.9  | 36.3  | 7.1   |       | 16.4  | 2.1   |  |
| LOS                  |       | D        | Α     |       | В     | D     | Α     |       | В     | Α     |  |
| Approach Delay       |       | 24.7     |       |       | 15.9  |       | 11.5  |       | 13.3  |       |  |
| Approach LOS         |       | С        |       |       | В     |       | В     |       | В     |       |  |
| Intersection Summary |       |          |       |       |       |       |       |       |       |       |  |

Cycle Length: 62 Actuated Cycle Length: 62

Offset: 0 (0%), Referenced to phase 2:NBT and 6:SBTL, Start of Yellow

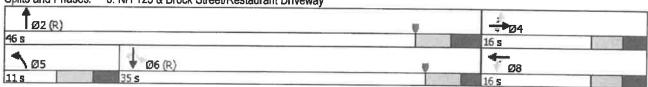
Natural Cycle: 60

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.69
Intersection Signal Delay: 14.0
Intersection Capacity Utilization 94.0%

Intersection LOS: B ICU Level of Service F

Analysis Period (min) 15



|                         | <b>→</b> | *    | -    | 4    | <b>†</b> | Ţ    | 1    |
|-------------------------|----------|------|------|------|----------|------|------|
| Lane Group              | EBT      | EBR  | WBT  | NBL  | NBT      | SBT  | SBR  |
| Lane Group Flow (vph)   | 168      | 74   | 14   | 119  | 676      | 706  | 195  |
| v/c Ratio               | 0.63     | 0.17 | 0.04 | 0.53 | 0.53     | 0.69 | 0.21 |
| Control Delay           | 35.2     | 8.0  | 15.9 | 36.3 | 7.1      | 16.4 | 2.1  |
| Queue Delay             | 0.0      | 0.0  | 0.0  | 0.0  | 0.0      | 0.0  | 0.0  |
| Total Delay             | 35.2     | 0.8  | 15.9 | 36.3 | 7.1      | 16.4 | 2.1  |
| Queue Length 50th (ft)  | 57       | 0    | 2    | 43   | 109      | 195  | 0    |
| Queue Length 95th (ft)  | #128     | 0    | 15   | #104 | 175      | 317  | 26   |
| Internal Link Dist (ft) | 204      |      | 294  |      | 1001     | 1243 |      |
| Turn Bay Length (ft)    |          |      |      | 375  |          |      |      |
| Base Capacity (vph)     | 278      | 460  | 333  | 225  | 1278     | 1039 | 963  |
| Starvation Cap Reductn  | 0        | 0    | 0    | 0    | 0        | 0    | 0    |
| Spillback Cap Reductn   | 0        | 0    | 0    | 0    | 0        | 0    | 0    |
| Storage Cap Reductn     | 0        | 0    | 0    | 0    | 0        | 0    | 0    |
| Reduced v/c Ratio       | 0.60     | 0.16 | 0.04 | 0.53 | 0.53     | 0.68 | 0.20 |
| Intersection Summary    |          |      |      |      |          |      |      |

<sup># 95</sup>th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

|                              | *    | <b>→</b> | *    | 1    | 4    | 1     | 1    | 1    | -    | 1    | +    | 1    |
|------------------------------|------|----------|------|------|------|-------|------|------|------|------|------|------|
| Movement                     | EBL  | EBT      | EBR  | WBL  | WBT  | WBR   | NBL  | NBT  | NBR  | SBL  | SBT  | SBR  |
| Lane Configurations          |      | 4        | 7    |      | 4    |       | 7    | 1    |      |      | ની   | 7    |
| Traffic Volume (veh/h)       | 189  | 6        | 85   | 5    | 4    | 7     | 130  | 741  | 0    | 2    | 833  | 230  |
| Future Volume (veh/h)        | 189  | 6        | 85   | 5    | 4    | 7     | 130  | 741  | 0    | 2    | 833  | 230  |
| Initial Q (Qb), veh          | 0    | 0        | 0    | 0    | 0    | 0     | 0    | 0    | 0    | 0    | 0    | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |          | 1.00 | 1.00 |      | 1.00  | 1.00 |      | 1.00 | 1.00 |      | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00     | 1.00 | 1.00 | 1.00 | 1.00  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach        |      | No       |      |      | No   |       |      | No   |      |      | No   |      |
| Adj Sat Flow, veh/h/ln       | 1900 | 1900     | 1900 | 1900 | 1900 | 1900  | 1885 | 1885 | 1900 | 1900 | 1885 | 1870 |
| Adj Flow Rate, veh/h         | 199  | 6        | 89   | 6    | 4    | 8     | 144  | 823  | 0    | 2    | 859  | 237  |
| Peak Hour Factor             | 0.95 | 0.95     | 0.95 | 0.90 | 0.90 | 0.90  | 0.90 | 0.90 | 0.90 | 0.97 | 0.97 | 0.97 |
| Percent Heavy Veh, %         | 0    | 0        | 0    | 0    | 0    | 0     | 1    | 1    | 0    | 0    | 1    | 2    |
| Cap, veh/h                   | 281  | 5        | 325  | 77   | 58   | 46    | 203  | 1306 | 0    | 59   | 971  | 817  |
| Arrive On Green              | 0.20 | 0.20     | 0.20 | 0.20 | 0.20 | 0.20  | 0.11 | 0.69 | 0.00 | 0.52 | 0.52 | 0.52 |
| Sat Flow, veh/h              | 827  | 25       | 1610 | 0    | 288  | 230   | 1795 | 1885 | 0    | 1    | 1883 | 1585 |
| Grp Volume(v), veh/h         | 205  | 0        | 89   | 18   | 0    | 0     | 144  | 823  | 0    | 861  | 0    | 237  |
| Grp Sat Flow(s), veh/h/ln    | 852  | Ŏ        | 1610 | 518  | ő    | ŏ     | 1795 | 1885 | 0    | 1884 | 0    | 1585 |
| Q Serve(g_s), s              | 0.0  | 0.0      | 2.9  | 0.0  | 0.0  | 0.0   | 4.8  | 14.7 | 0.0  | 0.0  | 0.0  | 5.3  |
| Cycle Q Clear(g_c), s        | 12.5 | 0.0      | 2.9  | 12.5 | 0.0  | 0.0   | 4.8  | 14.7 | 0.0  | 25.2 | 0.0  | 5.3  |
| Prop In Lane                 | 0.97 | 0.0      | 1.00 | 0.33 | 0.0  | 0.44  | 1.00 | 17.1 | 0.00 | 0.00 | 0.0  | 1.00 |
| Lane Grp Cap(c), veh/h       | 286  | 0        | 325  | 182  | 0    | 0.44  | 203  | 1306 | 0.00 | 1029 | 0    | 817  |
| V/C Ratio(X)                 | 0.72 | 0.00     | 0.27 | 0.10 | 0.00 | 0.00  | 0.71 | 0.63 | 0.00 | 0.84 | 0.00 | 0.29 |
| Avail Cap(c_a), veh/h        | 286  | 0.00     | 325  | 182  | 0.00 | 0.00  | 203  | 1306 | 0.00 | 1029 | 0.00 | 817  |
| HCM Platoon Ratio            | 1.00 | 1.00     | 1.00 | 1.00 | 1.00 | 1.00  | 1.00 | 1.00 | 1.00 | 1.00 | -    |      |
| Upstream Filter(I)           | 1.00 | 0.00     | 1.00 | 1.00 | 0.00 | 0.00  | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh     | 25.8 | 0.0      | 20.9 | 20.6 | 0.0  | 0.0   | 26.5 | 5.2  | 0.00 | 13.4 | 0.00 | 1.00 |
| Incr Delay (d2), s/veh       | 8.3  | 0.0      | 0.5  | 0.2  | 0.0  | 0.0   | 11.0 | 2.3  | 0.0  |      | 0.0  | 8.6  |
| Initial Q Delay(d3),s/veh    | 0.0  | 0.0      | 0.0  | 0.2  | 0.0  | 0.0   | 0.0  |      |      | 8.1  | 0.0  | 0.9  |
| %ile BackOfQ(50%),veh/ln     | 3.5  | 0.0      | 1.0  | 0.0  | 0.0  |       | 2.5  | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
|                              | 3.3  | 0.0      | 1.0  | 0.2  | 0.0  | 0.0   | 2.0  | 4.0  | 0.0  | 10.6 | 0.0  | 1.7  |
| Unsig. Movement Delay, s/veh | 24.0 | 0.0      | 04.4 | 00.0 |      |       | 07.5 | ~ -  |      |      |      |      |
| LnGrp Delay(d),s/veh         | 34.0 | 0.0      | 21.4 | 20.8 | 0.0  | 0.0   | 37.5 | 7.5  | 0.0  | 21.4 | 0.0  | 9.5  |
| LnGrp LOS                    | C    | A        | C    | C    | A    | A     | D    | A    | A    | C    | A    | A    |
| Approach Vol, veh/h          |      | 294      |      |      | 18   |       |      | 967  |      |      | 1098 |      |
| Approach Delay, s/veh        |      | 30.2     |      |      | 20.8 |       |      | 12.0 |      |      | 18.9 |      |
| Approach LOS                 |      | С        |      |      | C    |       |      | В    |      |      | В    |      |
| Timer - Assigned Phs         |      | 2        |      | 4    | 5    | 6     |      | 8    |      |      |      |      |
| Phs Duration (G+Y+Rc), s     |      | 47.5     |      | 16.0 | 11.0 | 36.5  |      | 16.0 |      |      |      |      |
| Change Period (Y+Rc), s      |      | 6.5      |      | 5.5  | 6.0  | * 6.5 |      | 5.5  |      |      |      |      |
| Max Green Setting (Gmax), s  |      | 39.5     |      | 10.5 | 5.0  | * 30  |      | 10.5 |      |      |      |      |
| Max Q Clear Time (g_c+l1), s |      | 16.7     |      | 14.5 | 6.8  | 27.2  |      | 14.5 |      |      |      |      |
| Green Ext Time (p_c), s      |      | 4.1      |      | 0.0  | 0.0  | 1.3   |      | 0.0  |      |      |      |      |
| Intersection Summary         |      |          |      |      |      |       |      |      |      |      |      |      |
| HCM 6th Ctrl Delay           |      |          | 17.5 |      |      |       |      |      |      |      |      |      |
| HCM 6th LOS                  |      |          | В    |      |      |       |      |      |      |      |      |      |
| Notes                        |      |          |      |      |      |       |      |      |      |      |      |      |

<sup>\*</sup> HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

|                      | 1     | $\rightarrow$ | -     | 1     | -     | 4     | †     | -     | <b>↓</b> | 1     |
|----------------------|-------|---------------|-------|-------|-------|-------|-------|-------|----------|-------|
| Lane Group           | EBL   | EBT           | EBR   | WBL   | WBT   | NBL   | NBT   | SBL   | SBT      | SBR   |
| Lane Configurations  |       | र्ब           | 7     |       | 4     | 3     | B     |       | 4        | 7     |
| Traffic Volume (vph) | 189   | 6             | 85    | 5     | 4     | 130   | 741   | 2     | 833      | 230   |
| Future Volume (vph)  | 189   | 6             | 85    | 5     | 4     | 130   | 741   | 2     | 833      | 230   |
| Turn Type            | Perm  | NA            | Perm  | Perm  | NA    | Prot  | NA    | Perm  | NA       | Perm  |
| Protected Phases     |       | 4             |       |       | 8     | 5     | 2     |       | 6        |       |
| Permitted Phases     | 4     |               | 4     | 8     |       |       |       | 6     |          | 6     |
| Detector Phase       | 4     | 4             | 4     | 8     | 8     | 5     | 2     | 6     | 6        | 6     |
| Switch Phase         |       |               |       |       |       |       |       |       | -        | ·     |
| Minimum Initial (s)  | 5.0   | 5.0           | 5.0   | 5.0   | 5.0   | 5.0   | 10.0  | 10.0  | 10.0     | 10.0  |
| Minimum Split (s)    | 16.0  | 16.0          | 16.0  | 16.0  | 16.0  | 11.0  | 16.5  | 16.0  | 16.0     | 16.0  |
| Total Split (s)      | 16.0  | 16.0          | 16.0  | 16.0  | 16.0  | 11.0  | 46.0  | 35.0  | 35.0     | 35.0  |
| Total Split (%)      | 25.8% | 25.8%         | 25.8% | 25.8% | 25.8% | 17.7% | 74.2% | 56.5% | 56.5%    | 56.5% |
| Yellow Time (s)      | 3.0   | 3.0           | 3.0   | 3.0   | 3.0   | 3.5   | 3.5   | 3.5   | 3.5      | 3.5   |
| All-Red Time (s)     | 2.5   | 2.5           | 2.5   | 2.5   | 2.5   | 2.5   | 3.0   | 2.0   | 2.0      | 2.0   |
| Lost Time Adjust (s) |       | -2.0          | -2.0  |       | -2.0  | -2.0  | -2.0  |       | -2.0     | -2.0  |
| Total Lost Time (s)  |       | 3.5           | 3.5   |       | 3.5   | 4.0   | 4.5   |       | 3.5      | 3.5   |
| Lead/Lag             |       |               |       |       |       | Lead  |       | Lag   | Lag      | Lag   |
| Lead-Lag Optimize?   |       |               |       |       |       | Yes   |       | Yes   | Yes      | Yes   |
| Recall Mode          | None  | None          | None  | None  | None  | None  | C-Min | C-Min | C-Min    | C-Min |
| Act Effct Green (s)  |       | 12.2          | 12.2  |       | 12.2  | 7.4   | 41.8  |       | 31.4     | 31.4  |
| Actuated g/C Ratio   |       | 0.20          | 0.20  |       | 0.20  | 0.12  | 0.67  |       | 0.51     | 0.51  |
| v/c Ratio            |       | 0.76          | 0.20  |       | 0.06  | 0.68  | 0.65  |       | 0.91     | 0.26  |
| Control Delay        |       | 44.6          | 1.6   |       | 16.1  | 45.7  | 9.0   |       | 29.9     | 2.2   |
| Queue Delay          |       | 0.0           | 0.0   |       | 0.0   | 0.0   | 0.0   |       | 0.0      | 0.0   |
| Total Delay          |       | 44.6          | 1.6   |       | 16.1  | 45.7  | 9.0   |       | 29.9     | 2.2   |
| LOS                  |       | D             | Α     |       | В     | D     | Α     |       | С        | Α     |
| Approach Delay       |       | 31.6          |       |       | 16.1  |       | 14.5  |       | 23.9     |       |
| Approach LOS         |       | С             |       |       | В     |       | В     |       | С        |       |
| Intersection Summary |       |               |       |       |       |       |       |       |          |       |

Cycle Length: 62 Actuated Cycle Length: 62

Offset: 0 (0%), Referenced to phase 2:NBT and 6:SBTL, Start of Yellow

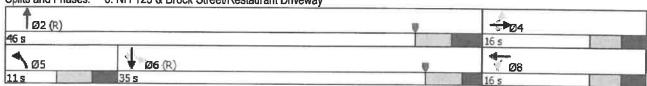
Natural Cycle: 60

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.91 Intersection Signal Delay: 21.0 Intersection Capacity Utilization 110.8%

Intersection LOS: C
ICU Level of Service H

Analysis Period (min) 15



|                         | <b>→</b> | *    | <b>—</b> | 4    | 1    | <b>↓</b> | 1    |
|-------------------------|----------|------|----------|------|------|----------|------|
| Lane Group              | EBT      | EBR  | WBT      | NBL  | NBT  | SBT      | SBR  |
| Lane Group Flow (vph)   | 205      | 89   | 18       | 144  | 823  | 861      | 237  |
| v/c Ratio               | 0.76     | 0.20 | 0.06     | 0.68 | 0.65 | 0.91     | 0.26 |
| Control Delay           | 44.6     | 1.6  | 16.1     | 45.7 | 9.0  | 29.9     | 2.2  |
| Queue Delay             | 0.0      | 0.0  | 0.0      | 0.0  | 0.0  | 0.0      | 0.0  |
| Total Delay             | 44.6     | 1.6  | 16.1     | 45.7 | 9.0  | 29.9     | 2.2  |
| Queue Length 50th (ft)  | 73       | 0    | 3        | 53   | 148  | 271      | 0    |
| Queue Length 95th (ft)  | #168     | 6    | 18       | #132 | 247  | #507     | 28   |
| Internal Link Dist (ft) | 204      |      | 294      |      | 1001 | 1243     |      |
| Turn Bay Length (ft)    |          |      |          | 375  |      |          |      |
| Base Capacity (vph)     | 275      | 458  | 324      | 212  | 1267 | 954      | 920  |
| Starvation Cap Reductn  | 0        | 0    | 0        | 0    | 0    | 0        | 0    |
| Spillback Cap Reductn   | 0        | 0    | 0        | 0    | 0    | 0        | 0    |
| Storage Cap Reductn     | 0        | 0    | 0        | 0    | 0    | 0        | 0    |
| Reduced v/c Ratio       | 0.75     | 0.19 | 0.06     | 0.68 | 0.65 | 0.90     | 0.26 |
| Intersection Summary    |          |      |          |      |      |          |      |

<sup># 95</sup>th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

|                              | ۶    | $\rightarrow$ | 7    | 1    | +    | 1     | 1    | <b>†</b> | 1    | 1    | 1    | 1    |
|------------------------------|------|---------------|------|------|------|-------|------|----------|------|------|------|------|
| Movement                     | EBL  | EBT           | EBR  | WBL  | WBT  | WBR   | NBL  | NBT      | NBR  | SBL  | SBT  | SBR  |
| Lane Configurations          |      | र्स           | 7    |      | 4    |       | ሻ    | 1>       |      |      | 4    | 7    |
| Traffic Volume (veh/h)       | 162  | 5             | 90   | 4    | 3    | 6     | 141  | 608      | 0    | 2    | 683  | 202  |
| Future Volume (veh/h)        | 162  | 5             | 90   | 4    | 3    | 6     | 141  | 608      | 0    | 2    | 683  | 202  |
| Initial Q (Qb), veh          | 0    | 0             | 0    | 0    | 0    | 0     | 0    | 0        | 0    | 0    | 0    | 0    |
| Ped-Bike Adj(A_pbT)          | 1.00 |               | 1.00 | 1.00 |      | 1.00  | 1.00 |          | 1.00 | 1.00 |      | 1.00 |
| Parking Bus, Adj             | 1.00 | 1.00          | 1.00 | 1.00 | 1.00 | 1.00  | 1.00 | 1.00     | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach        |      | No            |      |      | No   |       |      | No       |      |      | No   |      |
| Adj Sat Flow, veh/h/ln       | 1900 | 1900          | 1900 | 1900 | 1900 | 1900  | 1885 | 1885     | 1900 | 1900 | 1885 | 1870 |
| Adj Flow Rate, veh/h         | 171  | 5             | 95   | 4    | 3    | 7     | 157  | 676      | 0    | 2    | 704  | 208  |
| Peak Hour Factor             | 0.95 | 0.95          | 0.95 | 0.90 | 0.90 | 0.90  | 0.90 | 0.90     | 0.90 | 0.97 | 0.97 | 0.97 |
| Percent Heavy Veh, %         | 0    | 0             | 0    | 0    | 0    | 0     | 1    | 1        | 0    | 0    | 1    | 2    |
| Cap, veh/h                   | 271  | 5             | 325  | 75   | 62   | 62    | 203  | 1262     | 0    | 59   | 926  | 780  |
| Arrive On Green              | 0.20 | 0.20          | 0.20 | 0.20 | 0.20 | 0.20  | 0.11 | 0.67     | 0.00 | 0.49 | 0.49 | 0.49 |
| Sat Flow, veh/h              | 778  | 23            | 1610 | 0    | 306  | 306   | 1795 | 1885     | 0.00 | 1    | 1883 | 1585 |
| Grp Volume(v), veh/h         | 176  | 0             | 95   | 14   | 0    | 0     | 157  | 676      | 0    | 706  | 0    | 208  |
| Grp Sat Flow(s), veh/h/ln    | 801  | ŏ             | 1610 | 612  | ő    | ő     | 1795 | 1885     | 0    | 1884 | 0    |      |
| Q Serve(g_s), s              | 0.0  | 0.0           | 3.1  | 0.0  | 0.0  | 0.0   | 5.3  | 11.5     | 0.0  | 0.0  | •    | 1585 |
| Cycle Q Clear(g_c), s        | 12.5 | 0.0           | 3.1  | 12.5 | 0.0  | 0.0   | 5.3  | 11.5     | 0.0  | 18.9 | 0.0  | 4.8  |
| Prop In Lane                 | 0.97 | 0.0           | 1.00 | 0.29 | 0.0  | 0.50  | 1.00 | 11.5     | 0.00 | 0.00 | 0.0  | 4.8  |
| Lane Grp Cap(c), veh/h       | 276  | 0             | 325  | 198  | 0    | 0.30  | 203  | 1262     |      |      | •    | 1.00 |
| V/C Ratio(X)                 | 0.64 | 0.00          | 0.29 | 0.07 | 0.00 | 0.00  | 0.77 | 0.54     | 0    | 985  | 0    | 780  |
| Avail Cap(c_a), veh/h        | 276  | 0.00          | 325  | 198  | 0.00 | 0.00  | 203  | 1262     | 0.00 | 0.72 | 0.00 | 0.27 |
| HCM Platoon Ratio            | 1.00 | 1.00          | 1.00 | 1.00 | 1.00 | 1.00  | 1.00 |          | 0    | 1015 | 0    | 805  |
| Upstream Filter(I)           | 1.00 | 0.00          | 1.00 | 1.00 | 0.00 | 0.00  |      | 1.00     | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh     | 25.3 | 0.00          | 21.0 | 20.5 | 0.00 |       | 1.00 | 1.00     | 0.00 | 1.00 | 0.00 | 1.00 |
| Incr Delay (d2), s/veh       | 4.8  | 0.0           |      |      |      | 0.0   | 26.7 | 5.3      | 0.0  | 12.8 | 0.0  | 9.2  |
|                              | 0.0  |               | 0.5  | 0.1  | 0.0  | 0.0   | 16.9 | 1.6      | 0.0  | 4.5  | 0.0  | 0.8  |
| Initial Q Delay(d3),s/veh    |      | 0.0           | 0.0  | 0.0  | 0.0  | 0.0   | 0.0  | 0.0      | 0.0  | 0.0  | 0.0  | 0.0  |
| %ile BackOfQ(50%),veh/ln     | 2.8  | 0.0           | 1.1  | 0.2  | 0.0  | 0.0   | 3.0  | 3.3      | 0.0  | 7.6  | 0.0  | 1.5  |
| Unsig. Movement Delay, s/veh | 00.4 | 0.0           | 04 = |      |      |       |      |          |      |      |      |      |
| LnGrp Delay(d),s/veh         | 30.1 | 0.0           | 21.5 | 20.6 | 0.0  | 0.0   | 43.6 | 6.9      | 0.0  | 17.3 | 0.0  | 10.0 |
| LnGrp LOS                    | C    | A             | С    | C    | A    | A     | D    | Α        | A    | B    | A    | B    |
| Approach Vol, veh/h          |      | 271           |      |      | 14   |       |      | 833      |      |      | 914  |      |
| Approach Delay, s/veh        |      | 27.1          |      |      | 20.6 |       |      | 13.8     |      |      | 15.6 |      |
| Approach LOS                 |      | С             |      |      | С    |       |      | В        |      |      | В    |      |
| Timer - Assigned Phs         |      | 2             |      | 4    | 5    | 6     |      | 8        |      |      |      |      |
| Phs Duration (G+Y+Rc), s     |      | 46.0          |      | 16.0 | 11.0 | 35.0  |      | 16.0     |      |      |      |      |
| Change Period (Y+Rc), s      |      | 6.5           |      | 5.5  | 6.0  | * 6.5 |      | 5.5      |      |      |      |      |
| Max Green Setting (Gmax), s  |      | 39.5          |      | 10.5 | 5.0  | * 30  |      | 10.5     |      |      |      |      |
| Max Q Clear Time (g_c+l1), s |      | 13.5          |      | 14.5 | 7.3  | 20.9  |      | 14.5     |      |      |      |      |
| Green Ext Time (p_c), s      |      | 3.1           |      | 0.0  | 0.0  | 2.9   |      | 0.0      |      |      |      |      |
| ntersection Summary          |      |               |      |      |      |       |      |          |      |      |      |      |
| HCM 6th Ctrl Delay           |      |               | 16.5 |      |      |       |      |          |      |      |      |      |
| HCM 6th LOS                  |      |               | В    |      |      |       |      |          |      |      |      |      |
| Notes                        |      |               |      |      |      |       |      |          |      |      |      |      |

<sup>\*</sup> HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

**Timings** 

|                      | 1     | <b>→</b> | *     | •     | 4     | 4     | †     | 1     | <b>+</b> | 4     |  |
|----------------------|-------|----------|-------|-------|-------|-------|-------|-------|----------|-------|--|
| Lane Group           | EBL   | EBT      | EBR   | WBL   | WBT   | NBL   | NBT   | SBL   | SBT      | SBR   |  |
| Lane Configurations  |       | 4        | 7     |       | 4     | ħ     | 1>    |       | 4        | 7     |  |
| Traffic Volume (vph) | 162   | 5        | 90    | 4     | 3     | 141   | 608   | 2     | 683      | 202   |  |
| Future Volume (vph)  | 162   | 5        | 90    | 4     | 3     | 141   | 608   | 2     | 683      | 202   |  |
| Turn Type            | Perm  | NA       | Perm  | Perm  | NA    | Prot  | NA    | Perm  | NA       | Perm  |  |
| Protected Phases     |       | 4        |       |       | 8     | 5     | 2     |       | 6        |       |  |
| Permitted Phases     | 4     |          | 4     | 8     |       |       |       | 6     |          | 6     |  |
| Detector Phase       | 4     | 4        | 4     | 8     | 8     | 5     | 2     | 6     | 6        | 6     |  |
| Switch Phase         |       |          |       |       |       |       |       |       | _        | •     |  |
| Minimum Initial (s)  | 5.0   | 5.0      | 5.0   | 5.0   | 5.0   | 5.0   | 10.0  | 10.0  | 10.0     | 10.0  |  |
| Minimum Split (s)    | 16.0  | 16.0     | 16.0  | 16.0  | 16.0  | 11.0  | 16.5  | 16.0  | 16.0     | 16.0  |  |
| Total Split (s)      | 16.0  | 16.0     | 16.0  | 16.0  | 16.0  | 11.0  | 46.0  | 35.0  | 35.0     | 35.0  |  |
| Total Split (%)      | 25.8% | 25.8%    | 25.8% | 25.8% | 25.8% | 17.7% | 74.2% | 56.5% | 56.5%    | 56.5% |  |
| Yellow Time (s)      | 3.0   | 3.0      | 3.0   | 3.0   | 3.0   | 3.5   | 3.5   | 3.5   | 3.5      | 3.5   |  |
| All-Red Time (s)     | 2.5   | 2.5      | 2.5   | 2.5   | 2.5   | 2.5   | 3.0   | 2.0   | 2.0      | 2.0   |  |
| Lost Time Adjust (s) |       | -2.0     | -2.0  |       | -2.0  | -2.0  | -2.0  |       | -2.0     | -2.0  |  |
| Total Lost Time (s)  |       | 3.5      | 3.5   |       | 3.5   | 4.0   | 4.5   |       | 3.5      | 3.5   |  |
| Lead/Lag             |       |          |       |       |       | Lead  |       | Lag   | Lag      | Lag   |  |
| Lead-Lag Optimize?   |       |          |       |       |       | Yes   |       | Yes   | Yes      | Yes   |  |
| Recall Mode          | None  | None     | None  | None  | None  | None  | C-Min | C-Min | C-Min    | C-Min |  |
| Act Effct Green (s)  |       | 12.1     | 12.1  |       | 12.1  | 8.1   | 41.9  |       | 30.7     | 30.7  |  |
| Actuated g/C Ratio   |       | 0.20     | 0.20  |       | 0.20  | 0.13  | 0.68  |       | 0.50     | 0.50  |  |
| v/c Ratio            |       | 0.66     | 0.21  |       | 0.04  | 0.67  | 0.53  |       | 0.76     | 0.23  |  |
| Control Delay        |       | 36.5     | 2.0   |       | 15.8  | 44.3  | 7.2   |       | 19.2     | 2.2   |  |
| Queue Delay          |       | 0.0      | 0.0   |       | 0.0   | 0.0   | 0.0   |       | 0.0      | 0.0   |  |
| Total Delay          |       | 36.5     | 2.0   |       | 15.8  | 44.3  | 7.2   |       | 19.2     | 2.2   |  |
| LOS                  |       | D        | Α     |       | В     | D     | Α     |       | В        | A     |  |
| Approach Delay       |       | 24.4     |       |       | 15.8  |       | 14.1  |       | 15.3     | • •   |  |
| Approach LOS         |       | С        |       |       | В     |       | В     |       | В        |       |  |
| Intersection Summary |       |          |       |       |       |       |       |       |          |       |  |

Cycle Length: 62 Actuated Cycle Length: 62

Offset: 0 (0%), Referenced to phase 2:NBT and 6:SBTL, Start of Yellow

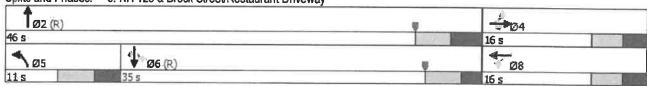
Natural Cycle: 60

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.76 Intersection Signal Delay: 16.1 Intersection Capacity Utilization 94.4%

Intersection LOS: B
ICU Level of Service F

Analysis Period (min) 15



|                         | $\rightarrow$ | *    | 4    | 4          | <b>†</b> | <b>↓</b> | 1    |
|-------------------------|---------------|------|------|------------|----------|----------|------|
| Lane Group              | EBT           | EBR  | WBT  | NBL        | NBT      | SBT      | SBR  |
| Lane Group Flow (vph)   | 176           | 95   | 14   | 157        | 676      | 706      | 208  |
| v/c Ratio               | 0.66          | 0.21 | 0.04 | 0.67       | 0.53     | 0.76     | 0.23 |
| Control Delay           | 36.5          | 2.0  | 15.8 | 44.3       | 7.2      | 19.2     | 2.2  |
| Queue Delay             | 0.0           | 0.0  | 0.0  | 0.0        | 0.0      | 0.0      | 0.0  |
| Total Delay             | 36.5          | 2.0  | 15.8 | 44.3       | 7.2      | 19.2     | 2.2  |
| Queue Length 50th (ft)  | 61            | 0    | 2    | <b>5</b> 9 | 109      | 195      | 0    |
| Queue Length 95th (ft)  | #137          | 9    | 15   | #147       | 175      | 317      | 27   |
| Internal Link Dist (ft) | 204           |      | 294  |            | 1001     | 1243     |      |
| Turn Bay Length (ft)    |               |      |      | 375        |          |          |      |
| Base Capacity (vph)     | 280           | 462  | 334  | 234        | 1275     | 955      | 906  |
| Starvation Cap Reductn  | 0             | 0    | 0    | 0          | 0        | 0        | 0    |
| Spillback Cap Reductn   | 0             | 0    | 0    | 0          | 0        | 0        | 0    |
| Storage Cap Reductn     | 0             | 0    | 0    | 0          | 0        | 0        | 0    |
| Reduced v/c Ratio       | 0.63          | 0.21 | 0.04 | 0.67       | 0.53     | 0.74     | 0.23 |
| Intersection Summary    |               |      |      |            |          |          |      |

<sup># 95</sup>th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

|                                   | ۶         | $\rightarrow$ | $\rightarrow$ | 1    | 4    | 1     | 4    | <b>†</b> | 1    | 1    | <b>‡</b> | 1            |
|-----------------------------------|-----------|---------------|---------------|------|------|-------|------|----------|------|------|----------|--------------|
| Movement                          | EBL       | EBT           | EBR           | WBL  | WBT  | WBR   | NBL  | NBT      | NBR  | SBL  | SBT      | SBR          |
| Lane Configurations               |           | स             | 7             |      | 4    |       | ሻ    | ĵ»       |      |      | सी       | 7            |
| Traffic Volume (veh/h)            | 196       | 6             | 105           | 5    | 4    | 7     | 164  | 741      | 0    | 2    | 833      | 243          |
| Future Volume (veh/h)             | 196       | 6             | 105           | 5    | 4    | 7     | 164  | 741      | 0    | 2    | 833      | 243          |
| Initial Q (Qb), veh               | 0         | 0             | 0             | 0    | 0    | 0     | 0    | 0        | 0    | 0    | 0        | 0            |
| Ped-Bike Adj(A_pbT)               | 1.00      |               | 1.00          | 1.00 |      | 1.00  | 1.00 |          | 1.00 | 1.00 |          | 1.00         |
| Parking Bus, Adj                  | 1.00      | 1.00          | 1.00          | 1.00 | 1.00 | 1.00  | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     | 1.00         |
| Work Zone On Approach             |           | No            |               |      | No   |       |      | No       |      |      | No       |              |
| Adj Sat Flow, veh/h/ln            | 1900      | 1900          | 1900          | 1900 | 1900 | 1900  | 1885 | 1885     | 1900 | 1900 | 1885     | 1870         |
| Adj Flow Rate, veh/h              | 206       | 6             | 111           | 6    | 4    | 8     | 182  | 823      | 0    | 2    | 859      | 251          |
| Peak Hour Factor                  | 0.95      | 0.95          | 0.95          | 0.90 | 0.90 | 0.90  | 0.90 | 0.90     | 0.90 | 0.97 | 0.97     | 0.97         |
| Percent Heavy Veh, %              | 0         | 0             | 0             | 0    | 0    | 0     | 1    | 1        | 0    | 0    | 1        | 2            |
| Cap, veh/h                        | 281       | 5             | 325           | 77   | 58   | 46    | 203  | 1307     | 0    | 59   | 972      | 818          |
| Arrive On Green                   | 0.20      | 0.20          | 0.20          | 0.20 | 0.20 | 0.20  | 0.11 | 0.69     | 0.00 | 0.52 | 0.52     | 0.52         |
| Sat Flow, veh/h                   | 828       | 24            | 1610          | 0    | 288  | 230   | 1795 | 1885     | 0    | 1    | 1883     | 1585         |
| Grp Volume(v), veh/h              | 212       | 0             | 111           | 18   | 0    | 0     | 182  | 823      | 0    | 861  | 0        | 251          |
| Grp Sat Flow(s),veh/h/ln          | 852       | Õ             | 1610          | 518  | Ŏ    | ő     | 1795 | 1885     | 0    | 1884 | 0        | 1585         |
| Q Serve(g_s), s                   | 0.0       | 0.0           | 3.7           | 0.0  | 0.0  | 0.0   | 6.2  | 14.7     | 0.0  | 0.0  | 0.0      | 5.6          |
| Cycle Q Clear(g_c), s             | 12.5      | 0.0           | 3.7           | 12.5 | 0.0  | 0.0   | 6.2  | 14.7     | 0.0  | 25.2 | 0.0      | 5.6          |
| Prop In Lane                      | 0.97      | 0.0           | 1.00          | 0.33 | 0.0  | 0.44  | 1.00 | 17,7     | 0.00 | 0.00 | 0.0      | 1.00         |
| Lane Grp Cap(c), veh/h            | 286       | 0             | 325           | 182  | 0    | 0.44  | 203  | 1307     | 0.00 | 1030 | 0        | 818          |
| V/C Ratio(X)                      | 0.74      | 0.00          | 0.34          | 0.10 | 0.00 | 0.00  | 0.90 | 0.63     | 0.00 | 0.84 | 0.00     | 0.31         |
| Avail Cap(c_a), veh/h             | 286       | 0.00          | 325           | 182  | 0.00 | 0.00  | 203  | 1307     | 0.00 | 1030 | 0.00     | 818          |
| HCM Platoon Ratio                 | 1.00      | 1.00          | 1.00          | 1.00 | 1.00 | 1.00  | 1.00 | 1.00     | 1.00 | 1.00 | 1.00     |              |
| Upstream Filter(I)                | 1.00      | 0.00          | 1.00          | 1.00 | 0.00 | 0.00  | 1.00 | 1.00     | 0.00 | 1.00 | 0.00     | 1.00<br>1.00 |
| Uniform Delay (d), s/veh          | 25.9      | 0.0           | 21.2          | 20.6 | 0.0  | 0.0   | 27.1 | 5.2      | 0.0  | 13.4 |          |              |
| Incr Delay (d2), s/veh            | 9.8       | 0.0           | 0.6           | 0.2  | 0.0  | 0.0   | 36.5 | 2.3      | 0.0  | 8.0  | 0.0      | 8.6          |
| Initial Q Delay(d3),s/veh         | 0.0       | 0.0           | 0.0           | 0.2  | 0.0  | 0.0   | 0.0  | 0.0      |      |      | 0.0      | 1.0          |
| %ile BackOfQ(50%),veh/ln          | 3.8       | 0.0           | 1.3           | 0.0  | 0.0  | 0.0   | 4.5  | 4.0      | 0.0  | 0.0  | 0.0      | 0.0          |
| Unsig. Movement Delay, s/veh      | 3.0       | 0.0           | 1.0           | 0.2  | 0.0  | 0.0   | 4.0  | 4.0      | 0.0  | 10.6 | 0.0      | 1.8          |
|                                   | 25.0      | 0.0           | 04.0          | 00.0 | 0.0  | 0.0   | 00.7 | 7.5      |      |      |          |              |
| LnGrp Delay(d),s/veh<br>LnGrp LOS | 35.8<br>D | 0.0           | 21.8          | 20.8 | 0.0  | 0.0   | 63.7 | 7.5      | 0.0  | 21.4 | 0.0      | 9.6          |
|                                   | U         | A             | С             | C    | A    | Α     | E    | A        | A    | C    | Α        | A            |
| Approach Vol, veh/h               |           | 323           |               |      | 18   |       |      | 1005     |      |      | 1112     |              |
| Approach Delay, s/veh             |           | 31.0          |               |      | 20.8 |       |      | 17.7     |      |      | 18.7     |              |
| Approach LOS                      |           | C             |               |      | С    |       |      | В        |      |      | В        |              |
| Timer - Assigned Phs              |           | 2             |               | 4    | 5    | 6     |      | 88       |      |      |          |              |
| Phs Duration (G+Y+Rc), s          |           | 47.5          |               | 16.0 | 11.0 | 36.5  |      | 16.0     |      |      |          |              |
| Change Period (Y+Rc), s           |           | 6.5           |               | 5.5  | 6.0  | * 6.5 |      | 5.5      |      |      |          |              |
| Max Green Setting (Gmax), s       |           | 39.5          |               | 10.5 | 5.0  | * 30  |      | 10.5     |      |      |          |              |
| Max Q Clear Time (g_c+l1), s      |           | 16.7          |               | 14.5 | 8.2  | 27.2  |      | 14.5     |      |      |          |              |
| Green Ext Time (p_c), s           |           | 4.1           |               | 0.0  | 0.0  | 1.3   |      | 0.0      |      |      |          |              |
| Intersection Summary              |           |               |               |      |      |       |      |          |      |      |          |              |
| HCM 6th Ctrl Delay                |           |               | 19.9          |      |      |       |      |          |      |      |          |              |
| HCM 6th LOS                       |           |               | В             |      |      |       |      |          |      |      |          |              |
| Notes                             |           |               |               |      |      |       |      |          |      |      |          |              |

<sup>\*</sup> HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

**Timings** 

|                      | •     | $\rightarrow$ | 7     | 1     | +     | 1     | <b>†</b> | 1     | Į.    | 1     |
|----------------------|-------|---------------|-------|-------|-------|-------|----------|-------|-------|-------|
| Lane Group           | EBL   | EBT           | EBR   | WBL   | WBT   | NBL   | NBT      | SBL   | SBT   | SBR   |
| Lane Configurations  |       | 4             | 7     |       | 4     | ħ     | 1        |       | र्न   | 7     |
| Traffic Volume (vph) | 196   | 6             | 105   | 5     | 4     | 164   | 741      | 2     | 833   | 243   |
| Future Volume (vph)  | 196   | 6             | 105   | 5     | 4     | 164   | 741      | 2     | 833   | 243   |
| Turn Type            | Perm  | NA            | Perm  | Perm  | NA    | Prot  | NA       | Perm  | NA    | Perm  |
| Protected Phases     |       | 4             |       |       | 8     | 5     | 2        |       | 6     |       |
| Permitted Phases     | 4     |               | 4     | 8     |       |       |          | 6     |       | 6     |
| Detector Phase       | 4     | 4             | 4     | 8     | 8     | 5     | 2        | 6     | 6     | 6     |
| Switch Phase         |       |               |       |       |       |       |          |       |       |       |
| Minimum Initial (s)  | 5.0   | 5.0           | 5.0   | 5.0   | 5.0   | 5.0   | 10.0     | 10.0  | 10.0  | 10.0  |
| Minimum Split (s)    | 16.0  | 16.0          | 16.0  | 16.0  | 16.0  | 11.0  | 16.5     | 16.0  | 16.0  | 16.0  |
| Total Split (s)      | 16.0  | 16.0          | 16.0  | 16.0  | 16.0  | 11.0  | 46.0     | 35.0  | 35.0  | 35.0  |
| Total Split (%)      | 25.8% | 25.8%         | 25.8% | 25.8% | 25.8% | 17.7% | 74.2%    | 56.5% | 56.5% | 56.5% |
| Yellow Time (s)      | 3.0   | 3.0           | 3.0   | 3.0   | 3.0   | 3.5   | 3.5      | 3.5   | 3.5   | 3.5   |
| All-Red Time (s)     | 2.5   | 2,5           | 2.5   | 2.5   | 2.5   | 2.5   | 3.0      | 2.0   | 2.0   | 2.0   |
| Lost Time Adjust (s) |       | -2.0          | -2.0  |       | -2.0  | -2.0  | -2.0     |       | -2.0  | -2.0  |
| Total Lost Time (s)  |       | 3.5           | 3.5   |       | 3.5   | 4.0   | 4.5      |       | 3.5   | 3.5   |
| Lead/Lag             |       |               |       |       |       | Lead  |          | Lag   | Lag   | Lag   |
| _ead-Lag Optimize?   |       |               |       |       |       | Yes   |          | Yes   | Yes   | Yes   |
| Recall Mode          | None  | None          | None  | None  | None  | None  | C-Min    | C-Min | C-Min | C-Min |
| Act Effct Green (s)  |       | 12.3          | 12.3  |       | 12.3  | 7.7   | 41.7     |       | 31.0  | 31.0  |
| Actuated g/C Ratio   |       | 0.20          | 0.20  |       | 0.20  | 0.12  | 0.67     |       | 0.50  | 0.50  |
| v/c Ratio            |       | 0.78          | 0.24  |       | 0.06  | 0.82  | 0.65     |       | 0.92  | 0.27  |
| Control Delay        |       | 46.3          | 3.0   |       | 16.1  | 59.9  | 9.1      |       | 31.7  | 2.2   |
| Queue Delay          |       | 0.0           | 0.0   |       | 0.0   | 0.0   | 0.0      |       | 0.0   | 0.0   |
| Total Delay          |       | 46.3          | 3.0   |       | 16.1  | 59.9  | 9.1      |       | 31.7  | 2.2   |
| LOS                  |       | D             | Α     |       | В     | Ε     | Α        |       | С     | Α     |
| Approach Delay       |       | 31.4          |       |       | 16.1  |       | 18.3     |       | 25.0  |       |
| Approach LOS         |       | С             |       |       | В     |       | В        |       | С     |       |
| ntersection Summary  |       |               |       |       |       |       |          |       |       |       |

Cycle Length: 62

Actuated Cycle Length: 62

Offset: 0 (0%), Referenced to phase 2:NBT and 6:SBTL, Start of Yellow

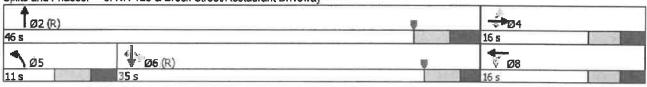
Natural Cycle: 75

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.92 Intersection Signal Delay: 23.0 Intersection Capacity Utilization 111.2%

Intersection LOS: C
ICU Level of Service H

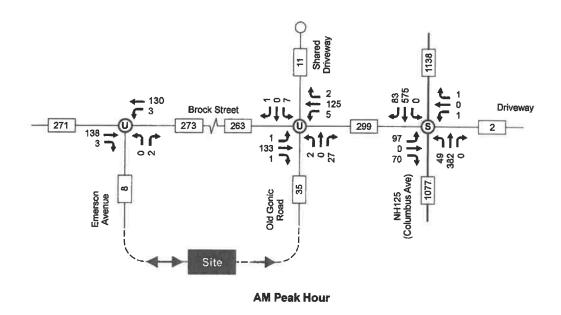
Analysis Period (min) 15

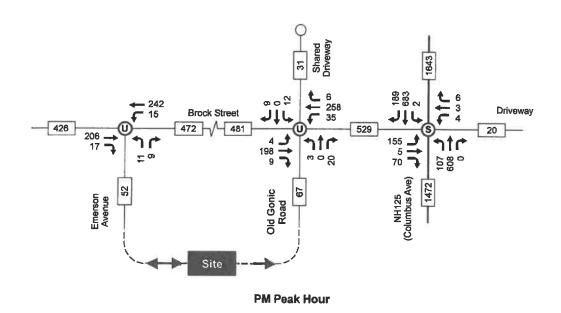


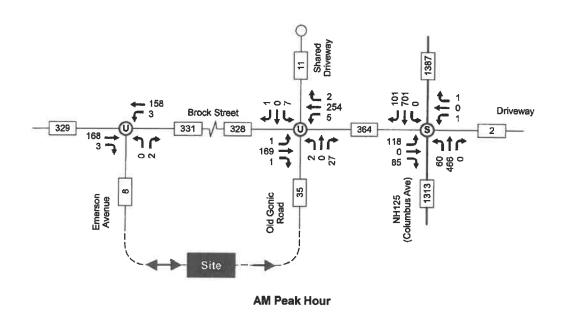
|                         | -    | *    | <del>-</del> | 4    | 1    | 1    | 1    |  |
|-------------------------|------|------|--------------|------|------|------|------|--|
| Lane Group              | EBT  | EBR  | WBT          | NBL  | NBT  | SBT  | SBR  |  |
| Lane Group Flow (vph)   | 212  | 111  | 18           | 182  | 823  | 861  | 251  |  |
| v/c Ratio               | 0.78 | 0.24 | 0.06         | 0.82 | 0.65 | 0.92 | 0.27 |  |
| Control Delay           | 46.3 | 3.0  | 16.1         | 59.9 | 9.1  | 31.7 | 2.2  |  |
| Queue Delay             | 0.0  | 0.0  | 0.0          | 0.0  | 0.0  | 0.0  | 0.0  |  |
| Total Delay             | 46.3 | 3.0  | 16.1         | 59.9 | 9.1  | 31.7 | 2.2  |  |
| Queue Length 50th (ft)  | 76   | 0    | 3            | 69   | 148  | 271  | 0    |  |
| Queue Length 95th (ft)  | #176 | 16   | 18           | #174 | 247  | #507 | 29   |  |
| Internal Link Dist (ft) | 204  |      | 294          |      | 1001 | 1243 |      |  |
| Turn Bay Length (ft)    |      |      |              | 375  |      |      |      |  |
| Base Capacity (vph)     | 275  | 458  | 324          | 222  | 1264 | 954  | 927  |  |
| Starvation Cap Reductn  | 0    | 0    | 0            | 0    | 0    | 0    | 0    |  |
| Spillback Cap Reductn   | 0    | 0    | 0            | 0    | 0    | 0    | 0    |  |
| Storage Cap Reductn     | 0    | 0    | 0            | 0    | 0    | 0    | 0    |  |
| Reduced v/c Ratio       | 0.77 | 0.24 | 0.06         | 0.82 | 0.65 | 0.90 | 0.27 |  |
| Intersection Summary    |      |      |              |      |      |      |      |  |

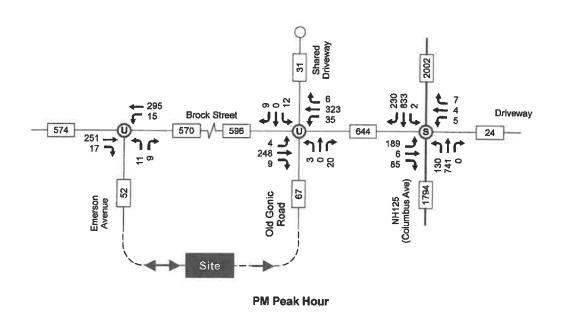
<sup># 95</sup>th percentile volume exceeds capacity, queue may be longer.

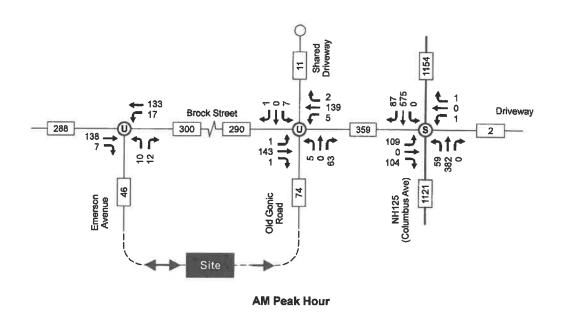
Queue shown is maximum after two cycles.

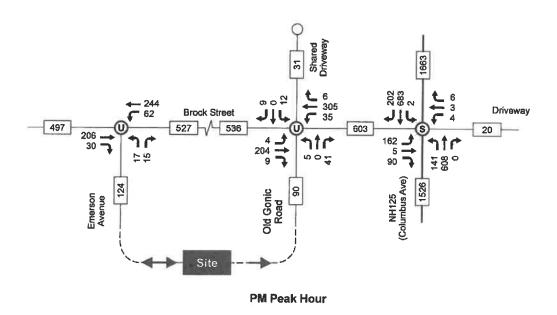


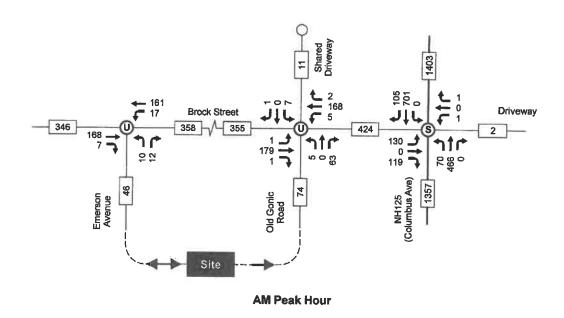


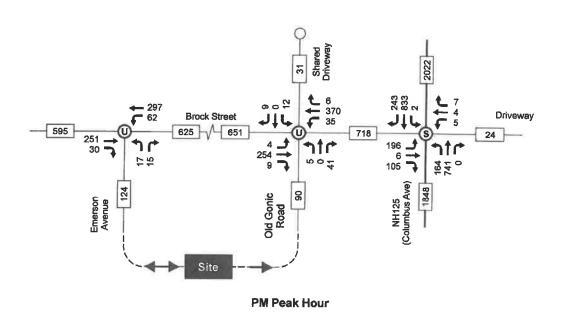


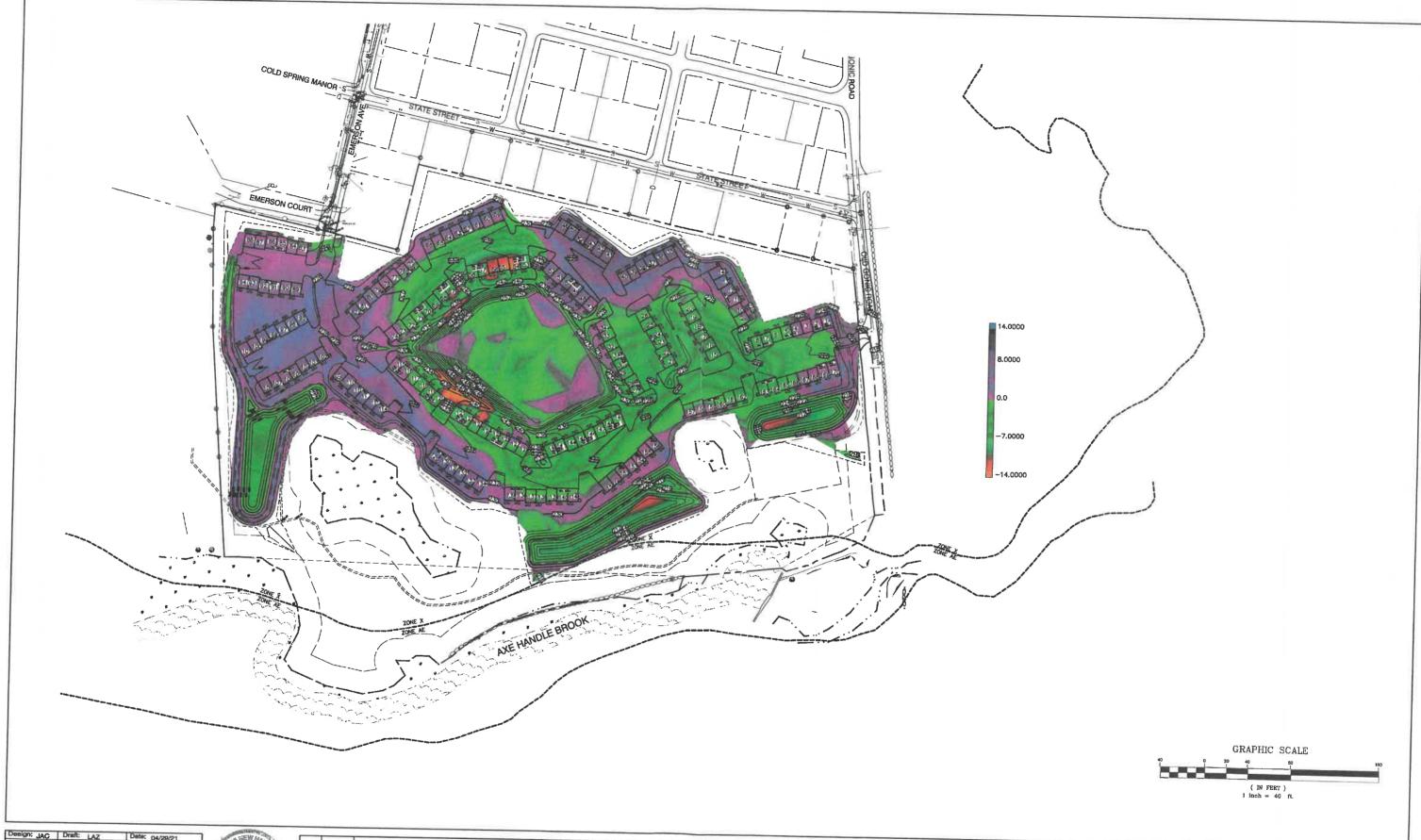












Design: JAC Draft: LAZ Date: 04/28/21
Checked: JAC Scale: AS NOTED Project No.: 21090
Drawing Name: 21090-PLAN.dwg
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| 2    | 4/11/22  | OFMOVED POAR                           |     |
|------|----------|--|-----|
| 1    | 1/18/22  | REMOVED ROAD REVISED PER CITY COMMENTS | LAZ |
| 0    | 11/23/21 | ISSUED FOR REVIEW                      | LAZ |
| REV. | DATE     | REVISION                               | BY  |

Jones & Beach Engineers, Inc.

85 Portsmouth Ave. Civil Engineering Somicon 609-172-4746

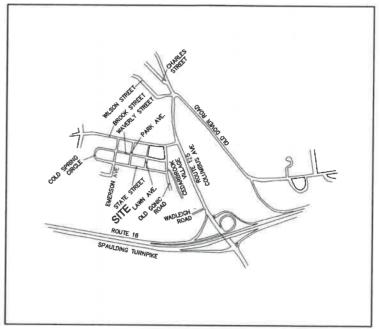
85 Portsmouth Ave. Civil Engineering Services 603-772-4746
PO Box 219 FAX: 603-772-0227
Stratham, NH 03885 E-MAIL: JBE@JONESANDBEACH.COM

| CUT/FILL PLAN  |
|--|
| BAYBERRY COMMONS<br>19 OLD GONIC ROAD, ROCHESTER, NH   |
| LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE<br>19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148 |
|  |



# GENERAL LEGEND × 100.00 99.50 TREES AND BUSHES 4K SEPTIC AREA WETLAND IMPACT XXXXX VEGETATED FILTER STRIP 350505 **●** \* ● FRESHWATER WETLANDS TIDAL WETLANDS SNOW STORAGE

# PROPOSED SITE PLAN "BAYBERRY COMMONS" **TAX MAP 131, LOT 10** 19 OLD GONIC ROAD, ROCHESTER, NH



LOCUS MAP SCALE 1" = 2000'

CIVIL ENGINEER / SURVEYOR JONES & BEACH ENGINEERS, INC. 85 PORTSMOUTH AVENUE PO BOX 219 STRATHAM, NH 03885 (603) 772-4746 CONTACT: JOSEPH CORONATI EMAIL: JCORONATI@JONESANDBEACH,COM

TRAFFIC ENGINEER STEPHEN G. PERNAW & COMPANY, INC. P.O. BOX 1821 CONCORD, NH 03302 (603) 731-8500 CONTACT: STEPHEN G. PERNAW EMAIL: SGP@PERNAW.COM

WETLAND CONSULTANT GOVE ENVIRONMENTAL SERVICES, INC. 8 CONTINENTAL DR., BUILDING 2, UNIT H EXETER, NH 03833-7526 (603) 778-0644 CONTACT: JAMES GOVE EMAIL: JGOVE@GESINC, BIZ

LANDSCAPE DESIGNER LM LAND DESIGN, LLC 11 SOUTH ROAD BRENTWOOD, NH 03833 (603) 770-7728 CONTACT: LISE McNAUGHTON LMLANDDESIGN@GMAIL.COM

WATER AND SEWER ROCHESTER DEPARTMENT OF PUBLIC WORKS 45 OLD DOVER ROAD ROCHESTER, NH 03867 (603) 332-4096 CONTACT: MICHAEL BEZANSON, P.E.

**ELECTRIC EVERSOURCE ENERGY** 74 OLD DOVER ROAD ROCHESTER, NH 03867 (603) 555-5334 CONTACT: MARK BOUCHER TELEPHONE CONSOLIDATED COMMUNICATIONS 1575 GREENLAND ROAD GREENLAND, NH 03840 (603) 427-5525 CONTACT: JOE CONSIDINE

CABLE TV COMCAST COMMUNICATION CORPORATION 334-B CALEF HIGHWAY EPPING, NH 03042-2325 (603) 679-5695

NATURAL GAS UNITIL SERVICE CORP. 325 WEST ROAD PORTSMOUTH, NH 03801 (603) 294-5261 MACLEAND@UNITIL.COM

#### SHEET INDEX

**COVER SHEET** 

EXISTING CONDITINS OVERVIEW PLAN

EXISTING CONDITIONS PLAN

DEMOLITION PLAN

OVERVIEW SITE PLAN

SITE PLANS

OVRG OVERVIEW GRADING PLAN

C9-C11 GRADING AND DRAINAGE PLAN

OVERVIEW UTILITY PLAN

UTILITY PLAN

LANDSCAPE PLAN L1-L2

LIGHTING PLAN

ROAD PLAN AND PROFILE

SEWER PROFILE

OFF-1-5 OFFSITE IMPROVEMENT PLANS

DETAIL SHEETS

**EROSION AND SEDIMENT CONTROL DETAILS** 

PHASING PLAN

PROJECT PARCEL CITY OF ROCHESTER TAX MAP 131, LOT 10

APPLICANT GREEN AND COMPAN

TOTAL LOT AREA

APPROVED - ROCHESTER, NH PLANNING BOARD

DATE:

| Checked: JAC     | Scale:   | AS NOTED      | Project No.: 21090   |
|------------------|----------|---------------|----------------------|
| Drawing Name:    | 21090-   | PLAN.dwg      |                      |
| THIS PLAN SHALL  | NOT BE   | MODIFIED WIT  | HOUT WRITTEN         |
| PERMISSION FRO   | M JONES  | & BEACH ENG   | GINEERS, INC. (JBE). |
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| AT THE USER'S SO | OLE RISK | AND WITHOUT   | LIABILITY TO JBE.    |

Design: JAC | Draft: LAZ | Date: 04/29/21



| 4    | 4/10/22  | REMOVED ROAD                          | LAZ |
|------|----------|---------------------------------------|-----|
| 3    | 3/11/22  | REVISED PER CITY COMMENTS             | LAZ |
| 2    | 2/14/22  | REVISED PER CITY ENGINEERING COMMENTS | LAZ |
| 1    | 1/18/22  | REVISED PER CITY COMMENTS             | LAZ |
| 0    | 11/23/21 | ISSUED FOR REVIEW                     | LAZ |
| REV. | DATE     | REVISION                              | BY  |

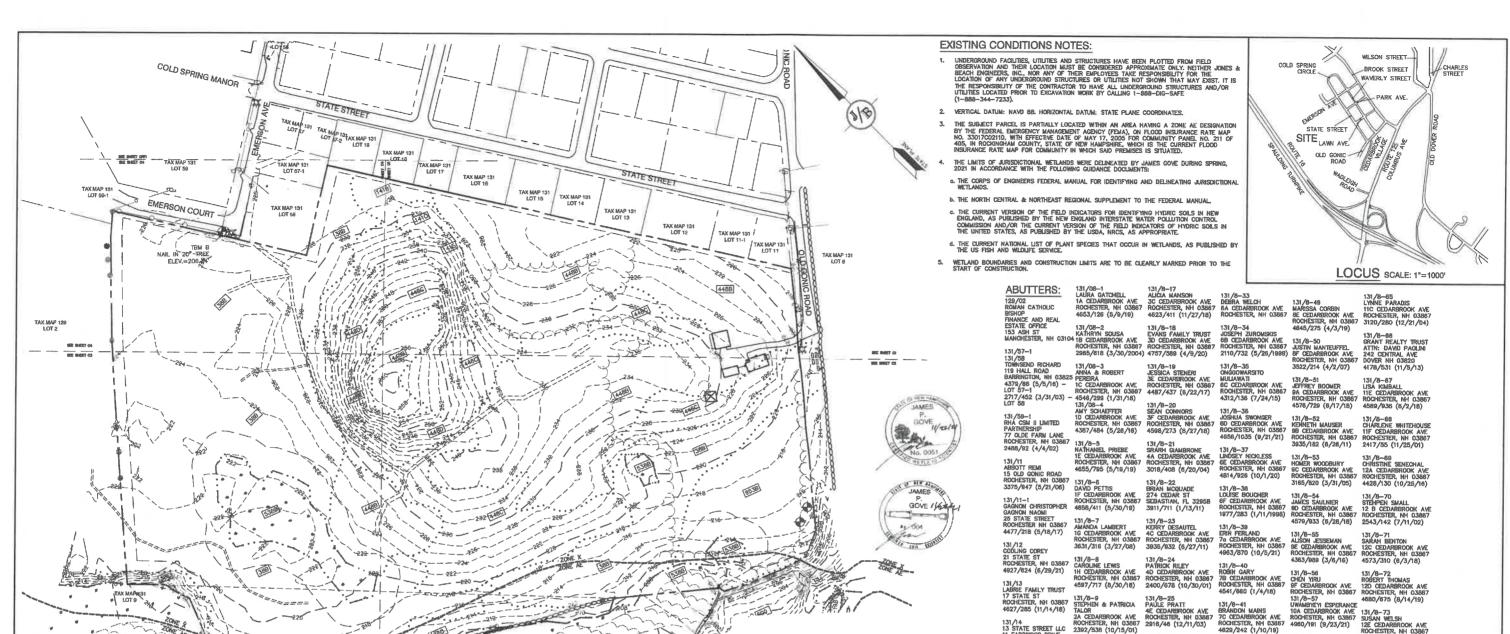
B Jones & Beach Engineers, Inc. 85 Portsmouth Ave. Civil Engineering Services

E-MAIL: JBE@JONESANDBEACH.COM

Plan Name **COVER SHEET** BAYBERRY COMMONS 19 OLD GONIC ROAD, ROCHESTER, NH Project:

LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4083 PG 148

CS SHEET 1 OF 45 JBE PROJECT NO. 21090



SOIL NOTES:

**PLAN REFERENCES:** 

"CEDARBROOK VILLAGE CONDOMINIUM DEVELOPMENT BOUNDARY SURVEY FOR ROUNDHOUSE REALTY TRUST

. "PLAN OF LAND PARCEL NO. 5 TAX ASSESSOR'S MAP 59 AND PARCEL NO. 2 TAX ASSESSOR'S MAP NO 8 NEW HAMPSHIER ROUTE 125 PREPARED FOR JEN-SCOT REALTY, INC"; PREPARED BY CIVILWORKS ENGINEERS AND SURVEYORS; DATED NOVEMBER 8, 1888 RECORDED AT THE STRAFFORD COUNTY REGISTRY OF DEEDS AS PLAN P37A—2028.

"PROPOSED SUBDIVISION AND LOT LINE REVISION FOR ROCHESTER HOUSING AUTHORITY COLD SPRING MANOR BROOK STREET ROCHESTER, NH"; PREPARED BY BERRY SUNEVING & ENGINEERING DATED FEBRUARY 13, 2001; RECORDED AT THE STRAFFORD COUNTY REGISTRY OF DEEDS AS PLAN P81–058.

. "PROPOSED SUBDIVISION LAND OF THOMAS & JODI REMINISTON 15 OLD GONIC ROAD ROCHESTER, NH"; PREPARED BY BERRY SURVEYING & ENGINEERING; DATED AUGUST 17, 2005; RECORDED AT THE STRAFFORD COUNTY REGISTRY OF DEEDS AS PLAN P81-0036.

CERTIFICATION:

THIS SURVEY CONFORMS TO A CATEGORY 1 CONDITION 1 SURVEY AS DEFINED IN SECTION 4.1 OF THE N.H.L.S.A. ETHICS AND STANDARDS.

DATE:

DAVID M. COLLIER, LLS 892 ON BEHALF OF JONES & BEACH ENGINEERS, INC. THIS MAP PRODUCT IS WITHIN THE TECHNICAL STANDARDS OF THE NATIONAL COOPERATIVE SOIL SURVEY. IT IS A SPECIAL PURPOSE PRODUCT, INTERDED FOR INFILTRATION REQUIREMENTS BY THE NH DES ALTERATION OF TERRAIN BUREAU. IT WAS PRODUCED BY A PROPESSIONAL SOIL SCIENTIST, AND IS NOT A PRODUCT OF THE USDA NATURAL RESOURCES CONSERVATION SERVICE. THERE IS A REPORT THAT ACCOMPANIES THIS MAP. THE STIE SPECIFIC SOIL SURVEY (SSSS) WAS PRODUCED JULY 21, 2021, AND WAS PREPARED BY JAMES P. GOVE, CSS # 004, GOVE ENVIRONMENTAL SERVICES, INC. THE SURVEY AREA IS LOCATED AT 18 DLD GROÜG ROAD, ROCHESTER, NH. SOLS WERE IDENTIFIED WITH THE NEW HAMPSHIRE STATE—MIDE NUMERICAL SOLS LEGEND, USDA NRCS, DURHAM, NH. ISSUE # 10, JANUARY 2011. THE NUMERIC LEGEND WAS AMENDED TO IDENTIFY THE CORRECT SOL COMPONENTS OF THE COMPLEX.

HYDROLOGIC SCIL GROUP FROM KSAT VALUES FOR NEW HAMPSHIRE SCILS, SOCIETY OF SCIL SCIENTISTS OF NEW ENGLAND, SPECIAL PUBLICATION NO. 5, SEPTEMBER, 2009. SSSS MAP NAME HISS SYM. HYDRO, SOIL GRP

BOXFORD (SOMEWHAT POORLY DRAINED) ELDRIDGE LOAMY SAND 228 323 SCITUATE FINE SANDY LOAM COUDORTHENTS, LOAMY

0-8% 8 8-15% C GRAPHIC SCALE

( IN FEET )

131/08 CEDARBROOK VILLAGE CONDO ASSOCIATION 14A CEDARBROOK VILL ROCHESTER, NH 03867 1161/202 (2/27/1985)

## EXISTING CONDITIONS PLAN

131/8-15 SEAN JACKSON 3A CEDARBROOK AVE ROCHESTER, NH 03867 4581/644 (6/28/18)

131/8-9 STEPHEN & PATRICIA TALOR 2A CEDARBROOK AVE ROCHESTER, NH 03867 2392/538 (10/15/01)

131/15
PENA DOMINIC RAFAEL
11 STATE STREET
ROCHESTER, NH 03867
3567/428 (8/23/07)
131/8-11

TOTAL ST ROCHESTER, NH 03887 137/8—12 4847/802 (12/13/20) 20 CORDE GATCOMB 20 COMPRENOW AVE ROCHESTER, NH 03887 7 STATE ST ROCHESTER NH 03887 20 COMPRENOW AVE ROCHESTER NH 03887 20 COMPRENOW AVE ROCHESTER NH 03887

4702/788 (10/23/19)

131/16 FRISBEE TRACEY 64 BROCK ST ROCHESTER, NH 03867

7 STATE ST ROCHESTER, NH 03867 3158/178 (2/14/05)

131/18 DAY ARRON 5 WSTATE STREET ROCHESTER, NH 03867 4769/475 (6/2/20)

131/19 GELINAS BRYAN GELINAS PAMELA 3 STATE ST ROCHESTER, NH 03867 4789/762 (8/25/20)

131/8-26 TIMES CAN

**BAYBERRY COMMONS** 19 OLD GONIC ROAD, ROCHESTER, NH

131/8-44 ALEXANDRA WCKMAN JOSEPH WARREN 7F CEDARBROOK AVE ROCHESTER, NH 03867 4765/958 (5/28/20)

131/8-45 7 KAREN BAILEY 8A CEDARBROOK AVE ROCHESTER, NH 03867 3876/380 (10/27/10)

4715/120 (12/2/19)

131/8-48 ROBIN LORD 8D CEDARBROOK AVE ROCHESTER, NH 03867 4923/182 (8/22/21)

131/8-62 JOHN COLECCHIA 10 F CEDARBROOK A ROCHESTER, NH 0386 4792/125 (5/7/20)

131/8-63 TARA CANFIELD 11A CEDARBROOK AVE ROCHESTER, NH 03867

2443/74 (1/10/02)

131/8-84 MOORE FAMILY REV.

Owner of Record:

3032/39 (7/2/04)

4304/153 (6/25/15) 4525/479 (10/26/17)

131/8-60 DENISE SELFE 10D CEDARBROOK AVE ROCHESTER, NH 03887 2215/260 (4/18/2000)

131/8-61 RICHARD DUSETT 33 ALEXANDRA LANE ROCHESTER NH 03867 1304/258 (4/15/1887)

PROJECT PARCEL TAX MAP 131, LOT 10

APPLICANT GREEN AND COMPANY 11 LAFAYETTE ROAD NORTH HAMPTON, NH 03862

TOTAL LOT AREA 1.309,695 SQ. FT, ± 30,07 ACRES ±

> DRAWING No. **OVR**

> > SHEET 2 OF 45

JBE PROJECT NO. 21090

Design: JAC Draft: LAZ
Checked: JAC Scale: AS NOTE
Drawing Name: 21090-PLAN.dwg

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"SUBDIVISION PLAN TAX MAP 131, LOT 57 STATE STREET & ENERSON COURT ROCHESTER NH FOR RUNNING WITH HAMMERS, LOT: PREPARED BY NORWAY PLANS ASSOCIATES, INC.: DATED OCTOBES 17, 2007: RECORDED AT THE STRAFFORD COUNTY REGISTRY OF DEEDS AS PLAN P82—014.

"ROCHESTER HEIGHTS ROCHESTER, NH A.H. CHAPMAI LAND CO"; PREPARED BY E.H. SHEFFIELD; DATED JULY 1920; RECORDED AT THE STRAFFORD COUNTY REGISTRY OF DEEDS AS PLAN #19 POCKET #10 FOLDER #3.

LAZ REMOVED ROAD 3/11/22 LAZ REVISED PER CITY COMMENTS LAZ REVISED PER CITY ENGINEERING COMMENTS 1/18/22 LAZ REVISED PER CITY COMMENTS 0 11/23/21 ISSUED FOR REVIEW LAŻ REV. DATE BY

Designed and Produced in NH B Jones & Beach Engineers, Inc.

85 Portsmouth Ave. PO Box 219
Stratham, NH 03885

85 Portsmouth Ave. Civil Engineering Services
E-MAIL: JBE©

E-MAIL: JBE@JONESANDBEACH,COM

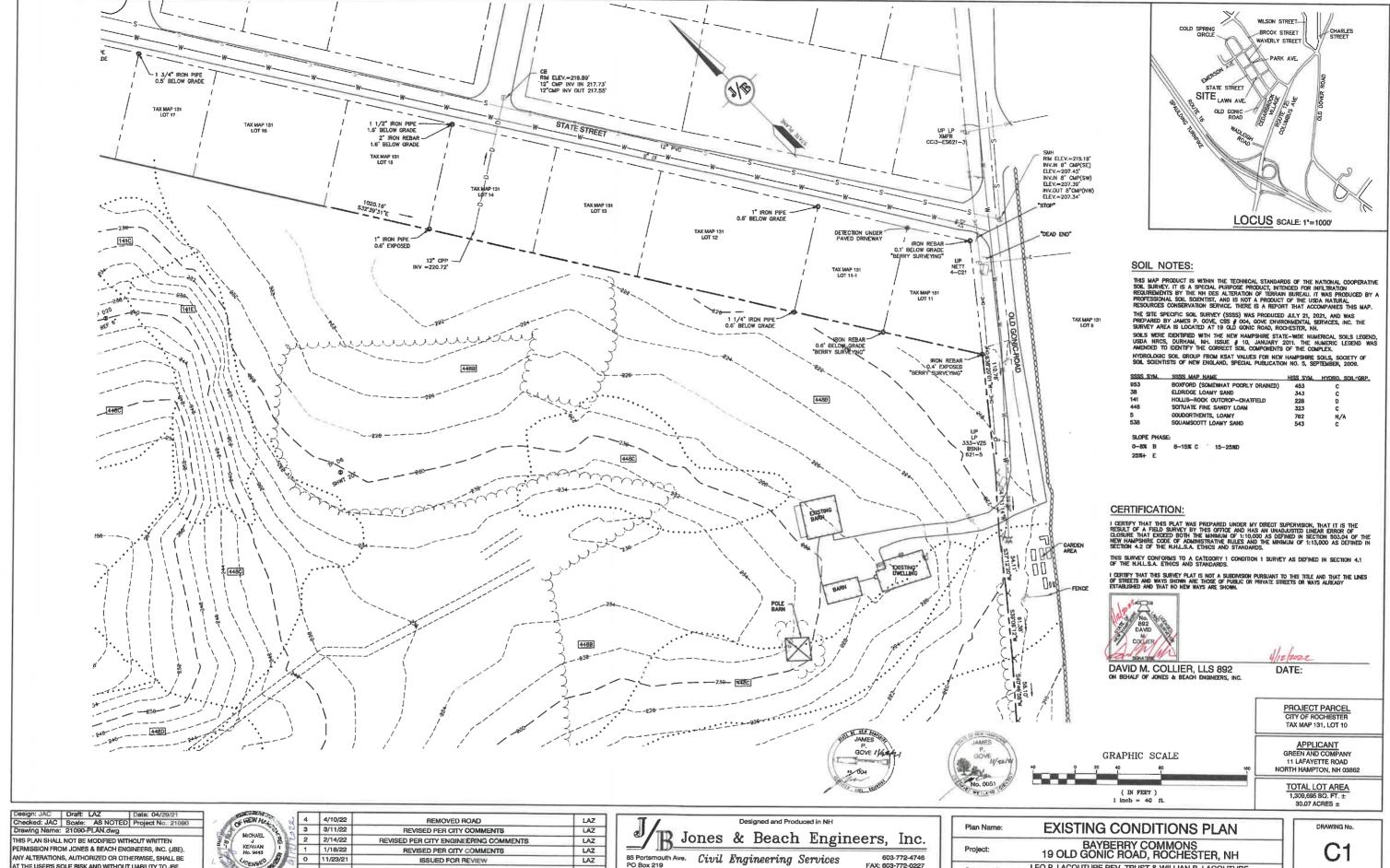
131/8–30
131/8–30
131/8–30
SAMDRA FOURNIER
OAK BILUFF REALTY LLC SO CEDARBROOK AVE
242 CENTRAL AVE
00VER NH 03820
2942/181 (2/11/04)
3953/549 (9/8/11)

131/8-16
ELIZABETH HANSON
3B CEDARBROOK AVE
ROCHESTER; NH 03867
4457/435 (2/9/17)
3719/769 (3/10/09)

131/8-31 OLD DOG PROPERTIES

DOVER NH 03820 4027/158 (5/29/12)

LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148



| Design: JAC   | Draft: LAZ    | Date: 04/29/21         |
|---------------|---------------|------------------------|
| Checked: JAC  | Scale: AS NO  | TED Project No.: 21090 |
| Drawing Name: | 21090-PLAN.dw | g                      |

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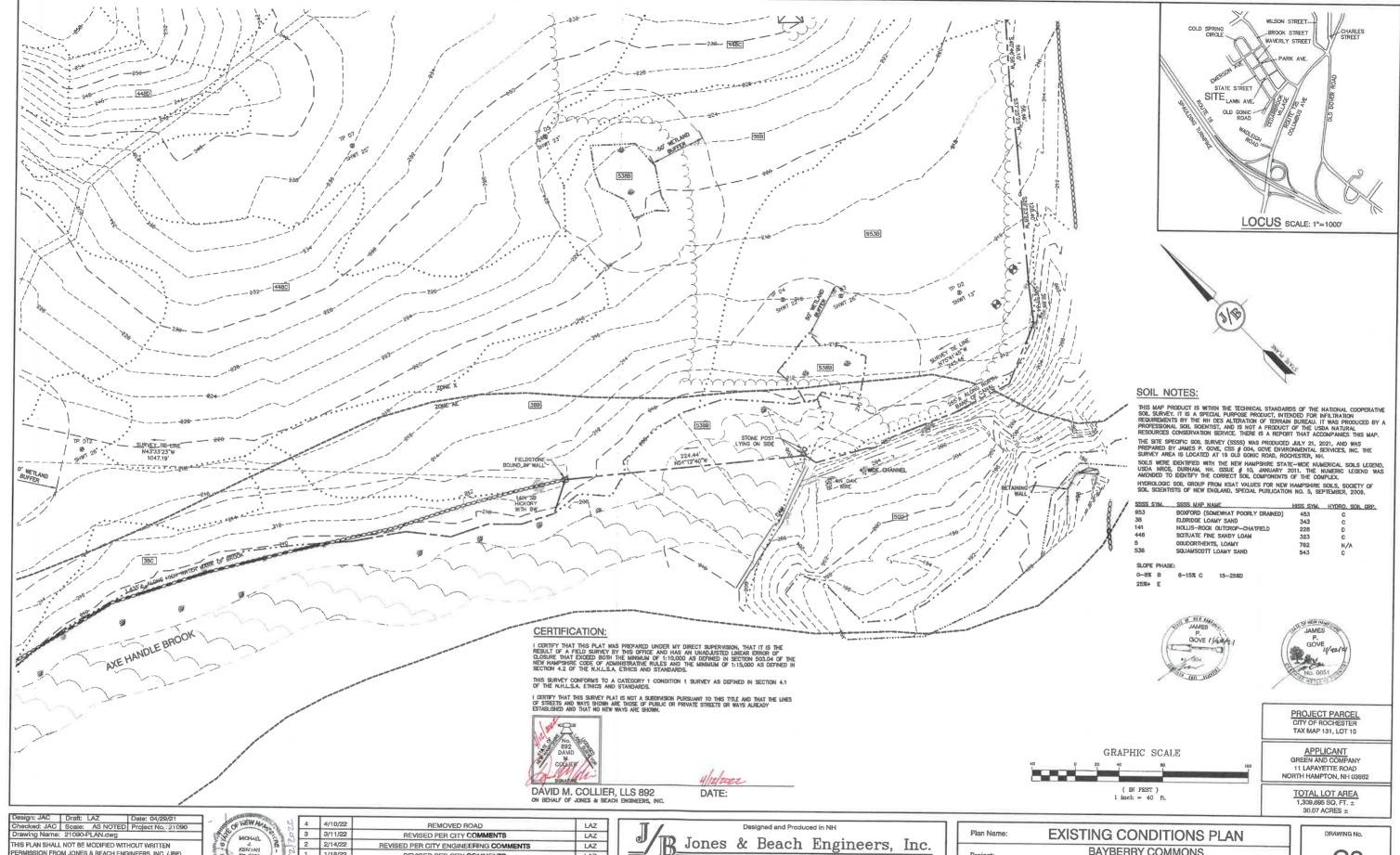
85 Portsmouth Ave. Civil Engineering Services
PO Box 219
Stratham, NH 03885
E-MAIL: JBE@

E-MAIL: JBE@JONESANDBEACH.COM

BAYBERRY COMMONS 19 OLD GONIC ROAD, ROCHESTER, NH Project:

LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148 Owner of Record:

**C1** SHEET 3 OF 45 JBE PROJECT NO. 21090



| Design: JAC     | Draft: | LAZ          | Date: 04/29/21                       |
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| Checked: JAC    | Scale: | AS NOTED     | Project No.: 21090                   |
| Drawing Name:   | 21090- | PLAN.dwg     |                                      |
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PO Box 219
Stratham, NH 03885
E-MAIL: JBE@ 603-772-4746 Services 603-772-4746 FAX: 803-772-0227 E-MAIL: JBE@JONESANDBEACH.COM

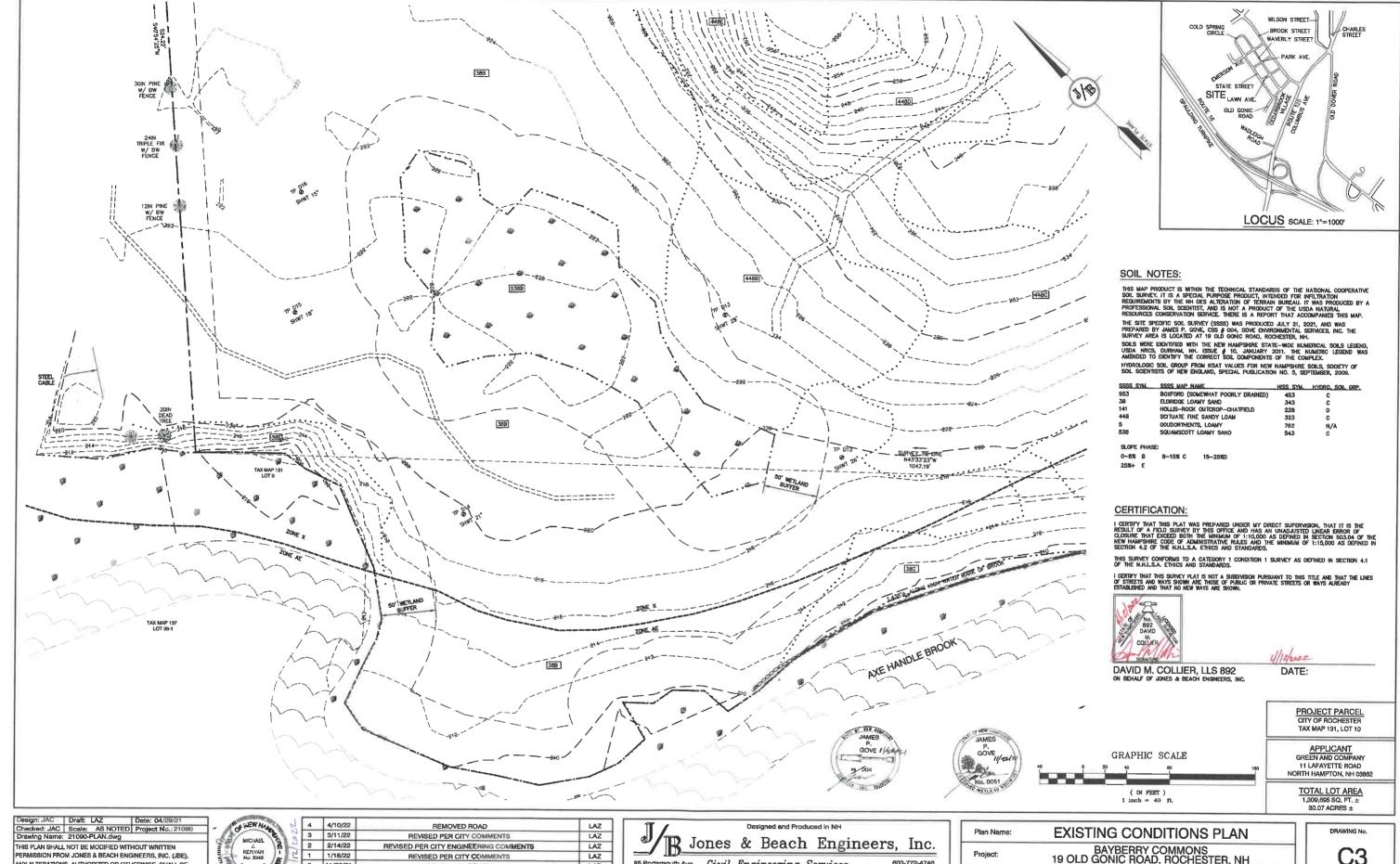
Project:

BAYBERRY COMMONS 19 OLD GONIC ROAD, ROCHESTER, NH

LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148 Owner of Record:

C2

SHEET 4 OF 45 JBE PROJECT NO. 21090



| Draft:  | LAZ      | Date: 04/29/21                                  |
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| Scale:  | AS NOTED | Project No.: 21090                              |
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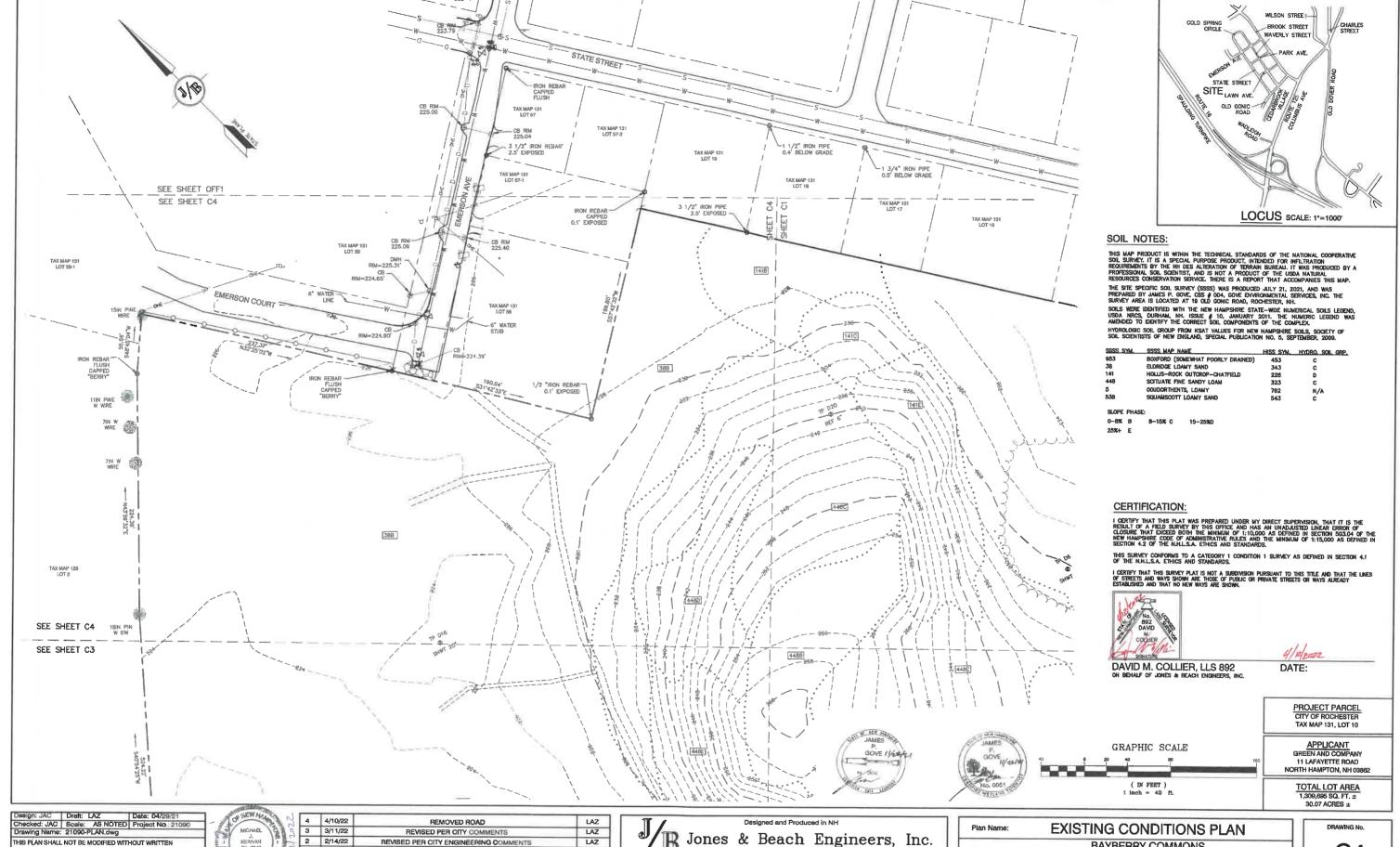
85 Portsmouth Ave. Civil Engineering Services
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Services 603-772-4746 FAX: 603-772-0227 E-MAIL: JBE@JONESANDBEACH.COM

BAYBERRY COMMONS 19 OLD GONIC ROAD, ROCHESTER, NH Project:

Owner of Record: LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148

**C3** 



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BAYBERRY COMMONS 19 OLD GONIC ROAD, ROCHESTER, NH Project:

LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148 Owner of Record:





#### **DEMOLITION NOTES:**

- THIS PLAN IS INTENDED TO PROVIDE MINIMUM GUIDELINES FOR SITE DEMOLITION, IT SHOULD BE NO THAT ALL MANNADE FEATURES, PAVEMENT, SIGNS, POLES, CURBING, CONGRETE WALKS, UTILITIES, ETC., SHALL BE REMOVED AS INCESSARY TO CONSTRUCT WORK, UNLESS OTHERWISE NOTED TO REMAIN. THROUGHOUT THE CONSTRUCTION PROCESS, THE CONTRACTOR SHALL INFORM THE ENGINE IMMEDIATELY OF ANY FIELD DISSREPANCIES FROM DATA AS SHOWN ON DESIGN PLANS. THIS INCLUDES ANY UNFORCESSED CONDITIONS, SUBJECTACE OF OTHERWISE FOR EVALUATION AND RECOMMENDATIONS. ANY CONTRADICTION BETWEEN TITMS OF THIS PLAN/PLAN SET, OR BETWEEN TO PLANS AND ON—SITE CONDITIONS MUST BE RESOLVED BEFORE RELATED CONSTRUCTION HAS BEEN MITATED.
- 2. A TEMPORARY CULVERT AND ROADBED SHALL BE IN PLACE PRIOR TO ANY USE OF A WETLAND
- WETLAND IMPACTS SHALL NOT OCCUR UNTIL ALL PERMITS HAVE BEEN ACQUIRED AND IMPACT MITIGATION REQUIREMENTS HAVE BEEN SATISFIED.

- ALL EXISTING PAVED SURFACES WITHIN THE LIMITS OF WORK THAT ARE TO REMAIN SHALL BE RECLAIMED TO MINIMUM DEPTH OF 12" AND REGRADED AS SHOWN ON THE GRADING AND DRAPPLAN, RECLAIMED ASPHALT SHALL CONFORM TO STATE SPECIFICATIONS, PRICIOR TO REMOVAL, PAVEMENT SHALL BE SAWCUT AT ALL ENTRANCES AND LIMITS OF REMOVAL.
- ALL EIGSTING GRANITE CURBING TO BE REMOVED SHALL BE STOCKPILED IN AN AREA TO BE DESIGNATED BY THE OWNER OR OWNER'S REPRESENTATIVE. THE OWNER SHALL INSPECT GRACUPBING TO BE RESET AND APPROVE LOCATIONS.

  INSTALL USED CURBING AT ANY ENTRANCE LOCATIONS.
- 9. EXISTING WATERLINES AND HYDRANTS TO BE REMOVED SHALL BE CAPPED AT EXISTING WATERMAIN.
- EXISTING GAS SERVICE LINES ARE TO BE REMOVED ON-SITE UP TO EXISTING GASMAIN LINES OR VALVES.
- THE CONTRACTOR SHALL REMOVE AND PROPERLY DISPOSE OF ALL CONTAMINATED MATERIAL LOCATED IN THE AREA OF EXISTING LEACHFIELDS IN ACCORDANCE WITH LOCAL AND STATE REQUILATIONS.
- 13. SEE LANDSCAPE PLAN FOR "TREES TO BE SAVED" AND DETAILS ASSOCIATED WITH LANDSCAPED
- THE CONTRACTOR SHALL OBTAIN TREE CLEARING PERMIT FROM LOCAL AND STATE AUTHORITIES PRIOR TO START OF CONSTRUCTION (IF REQUIRED).
- 15. CONTRACTOR SHALL HAVE THE OPTION TO REMOVE DRAINAGE/SEWER STRUCTURES, OR REMOVE MANHOLE FRAME AND GRATE/COVER TO A MINIMUM OF 38" BELOW FINISH GRADE, FRACTURE BOTTOM AND FILL WITH COMPACTED BORROW.
- 17. Edisting sanitary sewer line and structures located within the existing sewer easements shall be martaned or modified as noted on plans, sewer lines shall be disconnected in accordance with local strudards and regulations.
- EXCAVATED MATERIALS WILL BE PLACED WITHIN UPLAND AREAS AS FILL MATERIAL OR HAULED OFF-SITE FOR DISPOSAL IN AM APPROPRIATE UPLAND LOCATION.

PROJECT PARCEL TAX MAP 131, LOT 10

APPLICANT GREEN AND COMPANY 11 LAFAYETTE ROAD

TOTAL LOT AREA 1,309,695 SQ. FT. ± 30.07 ACRES ±

| Design: JAC  | Draft: LAZ      | Date: 04/29/21     |
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| Checked: JAC | Scale: AS NOTED | Project No.: 21090 |

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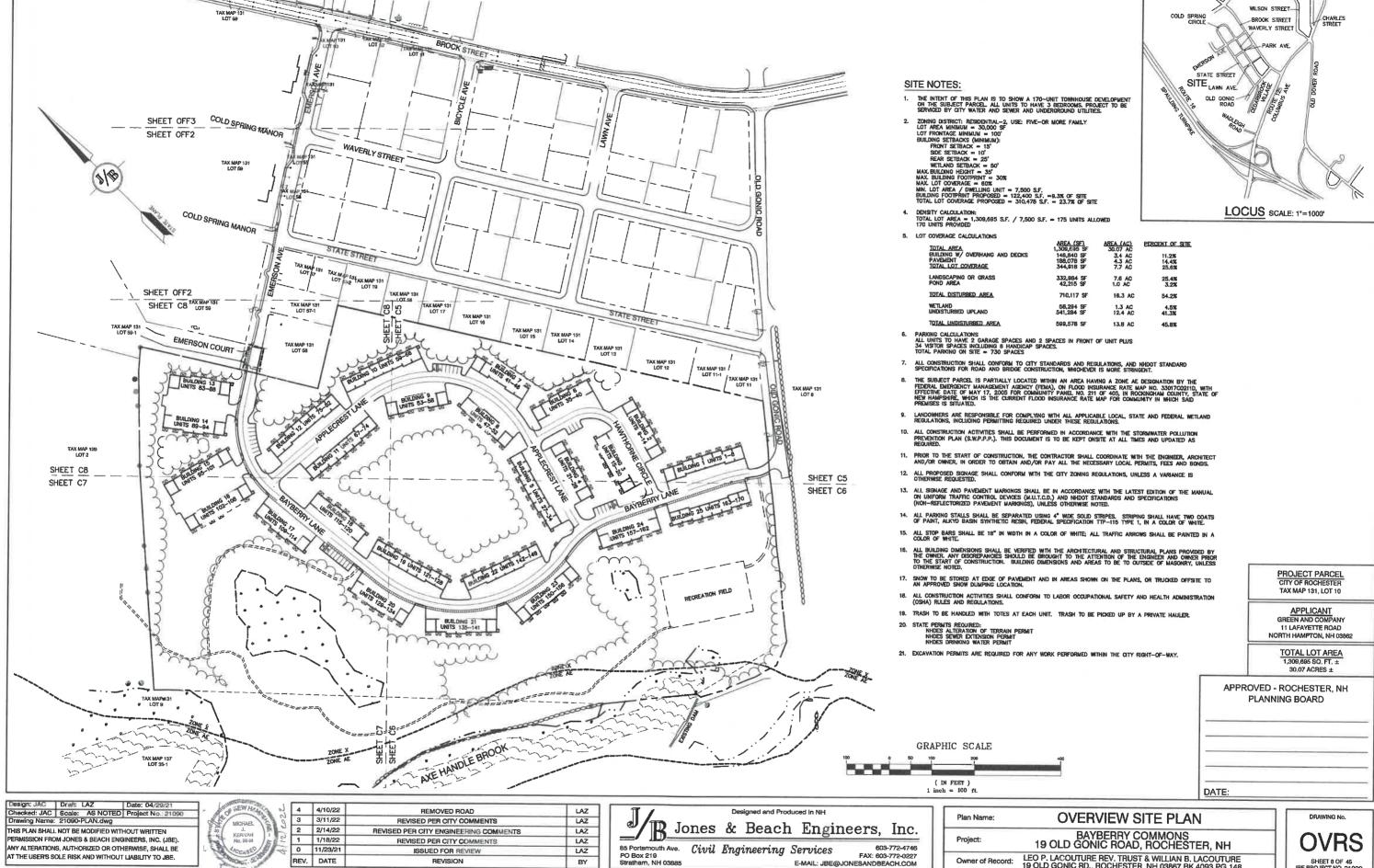
Designed and Produced in NH B Jones & Beach Engineers, Inc. 85 Portsmouth Ave. PO Box 219
Stratham, NH 03885

E-MAIL: JBE@

FAX: 603-772-0227 E-MAIL: JBE@JONESANDBEACH.COM Plan Name: **DEMOLITION PLAN** BAYBERRY COMMONS 19 OLD GONIC ROAD, ROCHESTER, NH Project:

Owner of Record: LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148





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**OVRS** 

LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148

Owner of Record:

E-MAIL: JBE@JONESANDBEACH.COM



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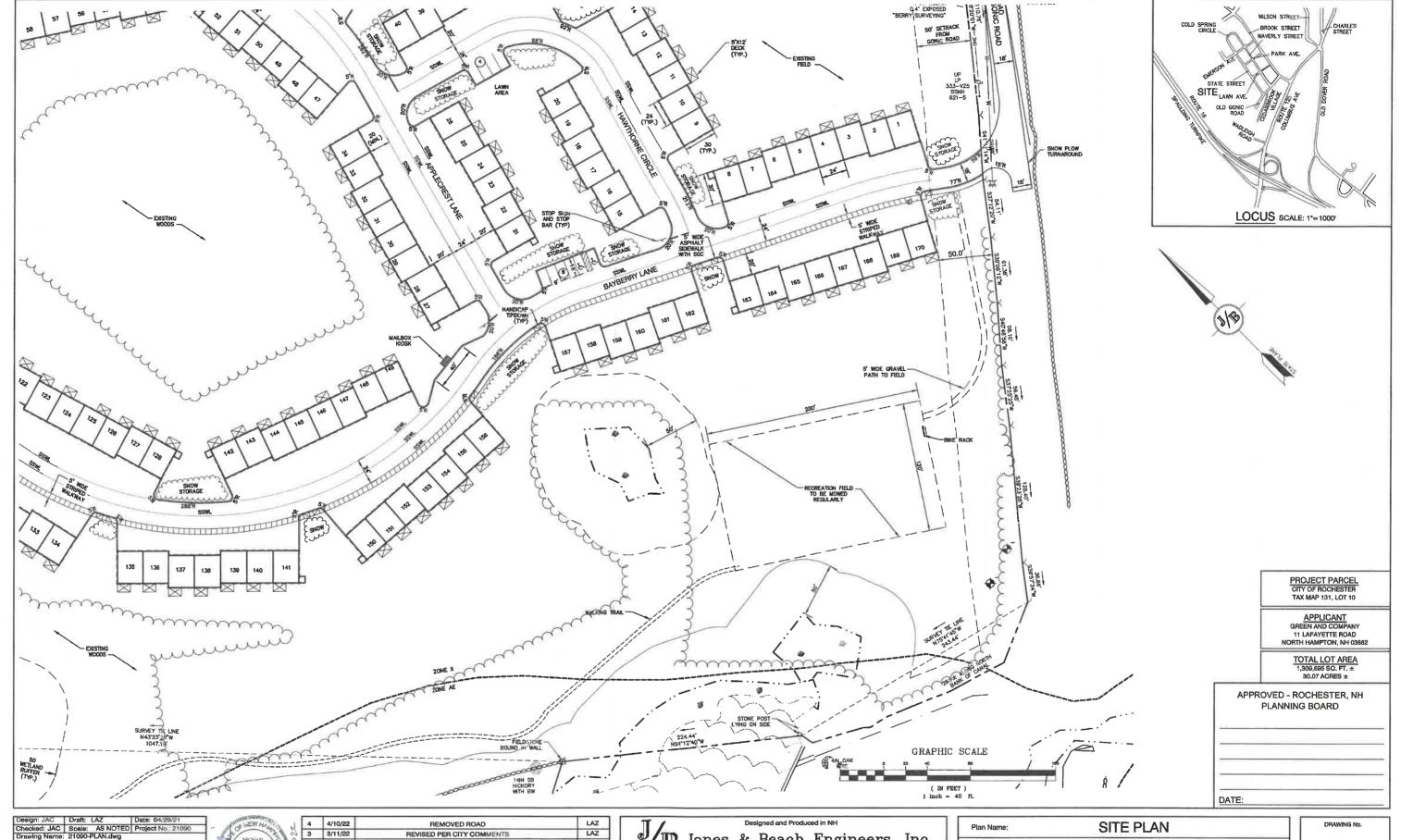
85 Portsmouth Ave. PO Box 219
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E-MAIL: JBE@ Services 609-772-4746 FAX: 603-772-0227 E-MAIL: JBE@JONESANDBEACH.COM Project:

BAYBERRY COMMONS 19 OLD GONIC ROAD, ROCHESTER, NH

Owner of Record: LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148

**C5** SHEET 9 OF 45 JBE PROJECT NO. 21090



Design: JAC Draft: LAZ Date: 04/29/21
Checked: JAC Scale: AS NOTED Project No.: 21090
Drawing Name: 21090-PLAN.dwg
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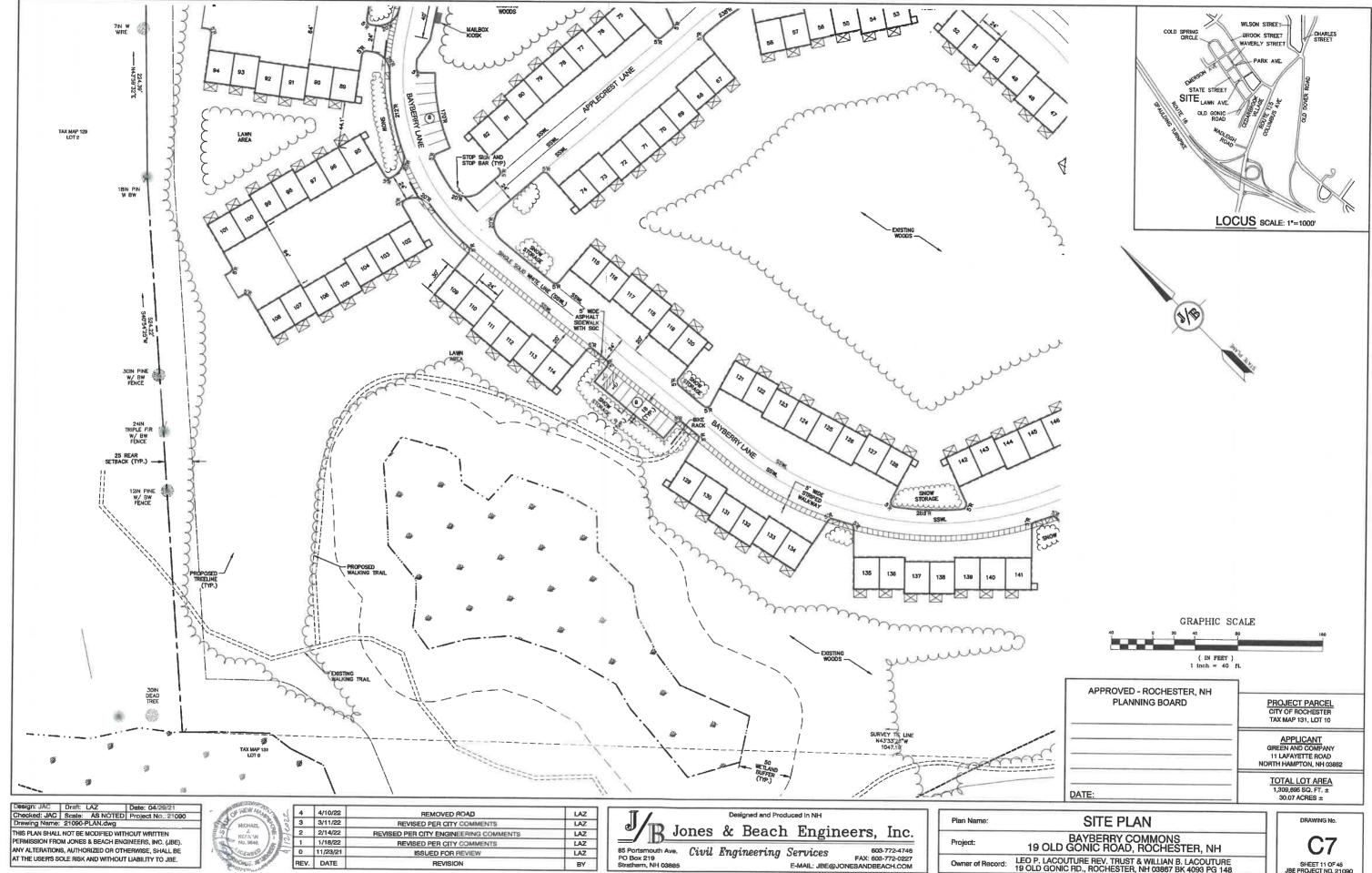
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|                             | Jones | & | ${\tt Beach}$ | Engineers, | Inc. |  |
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| Plan Name:       | SITE PLAN  | $\Box$ |
|------------------|--|--------|
| Project:         | BAYBERRY COMMONS<br>19 OLD GONIC ROAD, ROCHESTER, NH   |        |
| Owner of Record: | LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE<br>19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148 | ] [.   |
|                  | 19 OLD GONIC ROAD, ROCHESTER, NH LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE                        | _      |

C6 SHEET 10 OF 45 JBE PROJECT NO. 21090



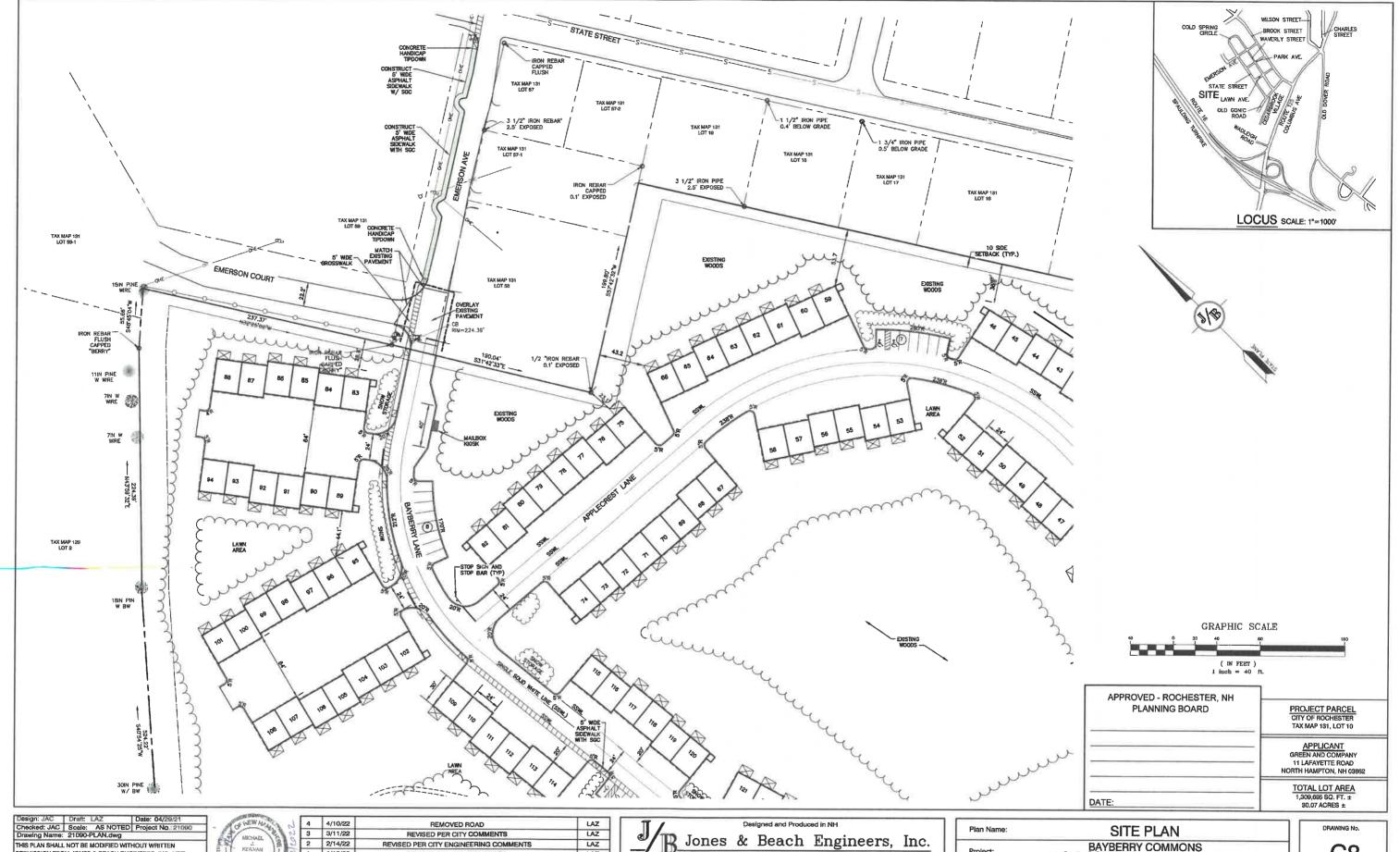
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Owner of Record: LEO P, LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148

**C7** SHEET 11 OF 45 JBE PROJECT NO. 21090



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| MICHAEL E   | 3    | 3/11/22  | REVISED PER CITY COMMENTS             | LAZ |
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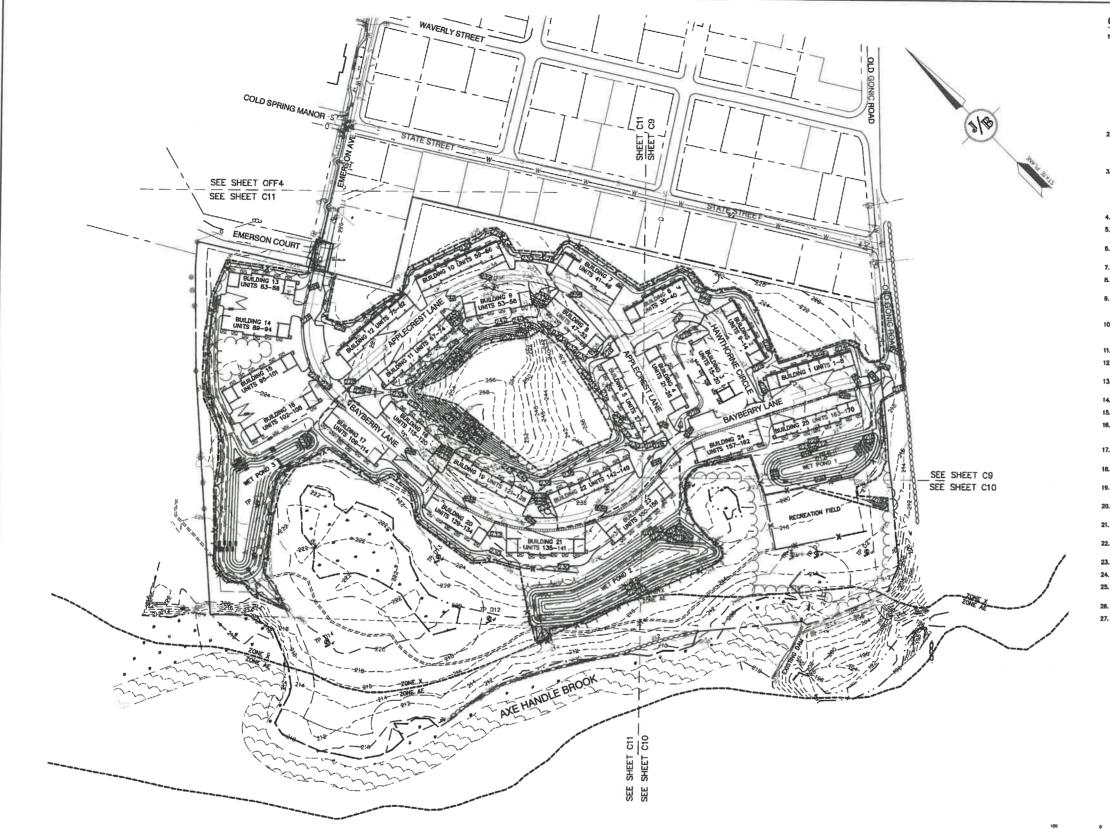
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BAYBERRY COMMONS 19 OLD GONIC ROAD, ROCHESTER, NH Project:

Owner of Record: LEO P, LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148

**C8** SHEET 12 OF 45 JBE PROJECT NO. 21090



#### GRADING AND DRAINAGE NOTES:

- 1. THIS STE WILL REQUIRE A USEPA NPDES PERMIT FOR STORMWATER DISCHARGE FOR THE CONSTRUCTION STE.

  THE CONSTRUCTION STE OPERATOR SHALL DEVELOP AND IMPLEMENT A CONSTRUCTION STORM WATER POLLUTION
  PREVENTION PLAN (SWEPP), WHICH SHALL REMAIN ON SITE AND BE MADE ACCESSIBLE TO THE PUBLIC. THE
  CONSTRUCTION SITE OPERATOR SHALL SUBMIT A NOTICE OF INTENT (NO) TO THE EPA REGIONAL OFFICE SEVEN
  DAYS PRIOR TO COMMENCEMENT OF ANY WORK ON SITE, EPA WILL POST THE NO! AT
  HTTP://CPUBLIPPA.COV/NPDES/STORMWATER/NO/NOISEARCHOFM. AUTHORIZATION IS GRANTED UNDER THE
  PERMIT ONCE THE NO! IS SHOWN IN "ACTIVE" STATUS ON THIS WEBSITE. A COMPLETED NOTICE OF TERMINATION
  SHALL BE SUBMITTED TO THE NPDES PERMITTING AUTHORITY WITHIN 30 DAYS AFTER ETHER OF THE FOLLOWING
  CONDITIONS HAVE BEEN MET:
  A FINAL STRABULATION HAS BEEN ACHIEVED ON ALL PORTIONS OF THE SITE FOR WHICH THE PERMITTEE IS
  RESPONSIBLE. OR

  B. ANDTHER DEPRATOR PERMITTEE HAS ASSUMED CONTRIBUTIONS AND ALL ACCESSION.

  - ANOTHER OPERATOR/PERMITTEE HAS ASSUMED CONTROL OVER ALL AREAS OF THE SITE THAT HAVE NOT BEEN FINALLY STABILIZED. PROVIDE DPW WITH A COPY OF THE NOTICE OF TERMINATION (NOT).
- IF THIS CONSTRUCTION SITE IS NOT STABILIZED WITH PAYEMENT, A ROAD GRAVEL BASE, 85 % MATURE VEGETATION COVER, OR RIPRAP BY OCTOBER 15, THEN THE SITE MUST BE PROTECTED WITH OVER-WINTER STABILIZATION. THE WINTER CONSTRUCTION PERIOD IS FROM OCTOBER 15 THROUGH MAY 15. WINTER EXCAVATION AND EARTHWORK ACTIVITIES SHALL BE LIMITED IN EXTENT AND DURATION, TO MINIMIZE POTENTIAL EROSION AND SODIMENTATION IMPACTS.
- UNDERGROUND FACILITIES, UTILITIES AND STRUCTURES HAVE BEEN PLOTTED FROM FIELD OBSERVATION AND THEIR LOCATION MUST BE CONSIDERED APPROGNATE ONLY. NEITHER JONES & BEACH ENGINEERS, INC., NOR ANY OF THEIR EMPLOYEES TAKE RESPONSIBILITY FOR THE LOCATION OF ANY UNDERGROUND STRUCTURES AND/OR UTILITIES FOR SHOWN THAT MAY EXIST. IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO HAVE ALL UNDERGROUND STRUCTURES AND/OR UTILITIES LOCATED PRIOR TO EXCAVATION WORK BY CALLING 888-DIG-SAFE (888-344-7233).
- 4. ALL BENCHMARKS AND TOPOGRAPHY SHOULD BE FIELD VERIFIED BY THE CONTRACTOR.
- SITE GRADING SHALL NOT PROCEED UNTIL EROSION CONTROL MEASURES HAVE BEEN INSTALLED. SEE CONSTRUCTION SEQUENCE ON SHEET E1.
- PRIOR TO THE START OF CONSTRUCTION, THE CONTRACTOR IS REQUIRED TO HAVE THE PROJECT'S LAND SURVEYOR STAKE OR FLAG CLEARING LIMITS. A MINIMUM OF 48 HOURS NOTICE IS REQUIRED.
- 7. ALL SWALES AND DETENTION PONDS ARE TO BE STABILIZED PRIOR TO DIRECTING RUNOFF TO THEM.
- PROPOSED RUM ELEVATIONS OF DRAINAGE STRUCTURES ARE APPROXIMATE. FINAL ELEVATIONS ARE TO BE SET FLUSH WITH FOUSH GRADES.
- ALL SWALES AND ANY SLOPES GREATER THAN 3:1 SHALL BE STABILIZED WITH NORTH AMERICAN GREEN 575 EROSION CONTROL BLANKETS (OR AN EQUIVALENT APPROVED IN WRITING BY THE ENGINEER), UNLESS OTHERWISE
- ALL DRAINAGE AND SANITARY STRUCTURE INTERIOR DIAMETERS (4' MIN) SHALL BE DETERMINED BY THE MANUFACTURER BASED ON THE PIPE CONFIGURATIONS SHOWN ON THESE PLANS. CATCH BASINS SHALL HAVE 3' DEEP SUMPS WITH GREASE HOODS, UNLESS DITHERWISE NOTED.
- 11. ALL DRAINAGE STRUCTURES SHALL BE PRECAST, UNLESS OTHERWISE SPECIFIED.
- ALL DRAINAGE STRUCTURES AND STORM SEWER PIPES SHALL MEET HEAVY DUTY TRAFFIC H20 LOADING AND SHALL SE INSTALLED ACCORDINGLY.
- 13. THE CONTRACTOR SHALL INSTALL ORANGE CONSTRUCTION FENCING ALONG PROPERTY LINES AND ALONG WETLAND
- 14. ALL DRAINAGE PIPE SHALL BE NON-PERFORATED ADS N-12 OR APPROVED EQUAL.
- 15. STONE INLET PROTECTION SHALL BE PLACED AT ALL CATCH BASINS, SEE DETAIL WITHIN THE DETAIL SHEETS.
- 16. LAND DISTURBING ACTIVITIES SHALL NOT COMMENCE UNTIL APPROVAL TO DO SO HAS BEEN RECEIVED BY ALL GOVERNING AUTHORITIES. THE GENERAL CONTRACTOR SHALL STRICTLY ADHERE TO THE EPA SWPPP DURING CONSTRUCTION OPERATIONS.
- ALL EXPOSED AREAS SHALL RE SEEDED AS SPECIFIED WITHIN 3 DAYS OF FINAL GRADING AND ANYTIME CONSTRUCTION STOPS FOR LONGER THAN 3 DAYS.
- MAINTAIN EROSION CONTROL MEASURES AFTER EACH RAIN EVENT OF 0.5" OR GREATER IN A 24 HOUR PERIOD AND AT LEAST ONCE A WEEK.
- 19. THIS PLAN SHALL NOT BE CONSIDERED ALL INCLUSIVE, AS THE GENERAL CONTRACTOR SHALL TAKE ALL NECESSARY PRECAUTIONS TO PREVENT SEDIMENT FROM LEAVING THE SITE.
- 20. CONSTRUCTION VEHICLES SHALL UTILIZE THE STABILIZED CONSTRUCTION ENTRANCE TO THE EXT
- 21. IF INSTALLATION OF STORM DRAINAGE SYSTEM SHOULD BE INTERRUPTED BY WEATHER OR NIGHTFALL, THE PIPE ENDS SHALL BE COVERED WITH FILTER FARRIC.
- 22. THE GENERAL CONTRACTOR SHALL BE RESPONSIBLE TO TAKE WHATEVER MEANS NECESSARY TO ESTABLISH PERMANENT SOIL STARILIZATION
- 23. SEDIMENT SHALL BE REMOVED FROM ALL SEDIMENT BASINS BEFORE THEY ARE 25% FULL.
- 24. ALL WORK SHALL BE DONE IN STRICT ACCORDANCE WITH PROJECT SPECIFICATIONS.
- Additional erosion and sediment control measures shall be installed, if deemed necessary by on-site inspection by engineer and/or regulatory officials.
- 26. SEE ALSO EROSION AND SEDIMENT CONTROL SPECIFICATIONS ON SHEET E1.
- PRIOR TO CLEARING OR GRADING DISTUBBANCE, THE CONTRACTOR SHALL IDENTIFY ALL AREAS OF TYPE 2 NIVASIVE SPECIES AS DEFINED BY NHOOT AND ADHERE TO THE PRACTICES OUTLINED IN BEST MANAGEMENT PRACTICES FOR THE CONTROL OF INVASIVE AND NODIOUS PLANT SPECIES MHOOT AND REST PRACTICES SHALL BE FOLLOWED FOR THE ENTIRE CONSTRUCTION. INCLUDING ESTABLISHMENT OF MADE ON AS THE SITE RE-VEGETATES AFTER CONSTRUCTION. LAINSCAPING CONTRACTOR TO INFORM THE OWNER IF ANY INVASIVE SPECIES START TO GROW. OWNER SHALL CONTACT A QUALIFIED REMOVAL COMPANY AND FOLLOW NHOES BEST MANAGEMENT PRACTICES.

GRAPHIC SCALE ( IN FEET ) 1 inch = 100 ft.

TAX MAP 131, LOT 10

APPLICANT GREEN AND COMP 11 LAFAYETTE ROAD NORTH HAMPTON, NH 03869

> TOTAL LOT AREA 1,309,695 SQ. FT. ± 30.07 ACRES ±

Design: JAC Draft: LAZ Date: 04/29/21 Checked: JAC Scale: AS NOTED Project No.. 21090 Drawing Name: 21090-PLAN.dwg

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| 4    | 4/10/22  | REMOVED ROAD                          | LAZ |
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| REV. | DATE     | REVISION                              | BY  |

Designed and Produced in NH B Jones & Beach Engineers, Inc. 603-772-4746

85 Portsmouth Ave. Civil Engineering Services
PO Box 219

Services 603-772-4746 FAX: 603-772-0227 E-MAIL: JBE@JONESANDBEACH.COM

OVERVIEW GRADING PLAN Plan Name:

BAYBERRY COMMONS 19 OLD GONIC ROAD, ROCHESTER, NH Project:

LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4083 PG 148 Owner of Record:





Design: JAC Draft: LAZ Date: 04/29/21 Checked: JAC Scale: AS NOTED Project No.: 21090 Drawing Name: 21090-PLAN.dwg THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN

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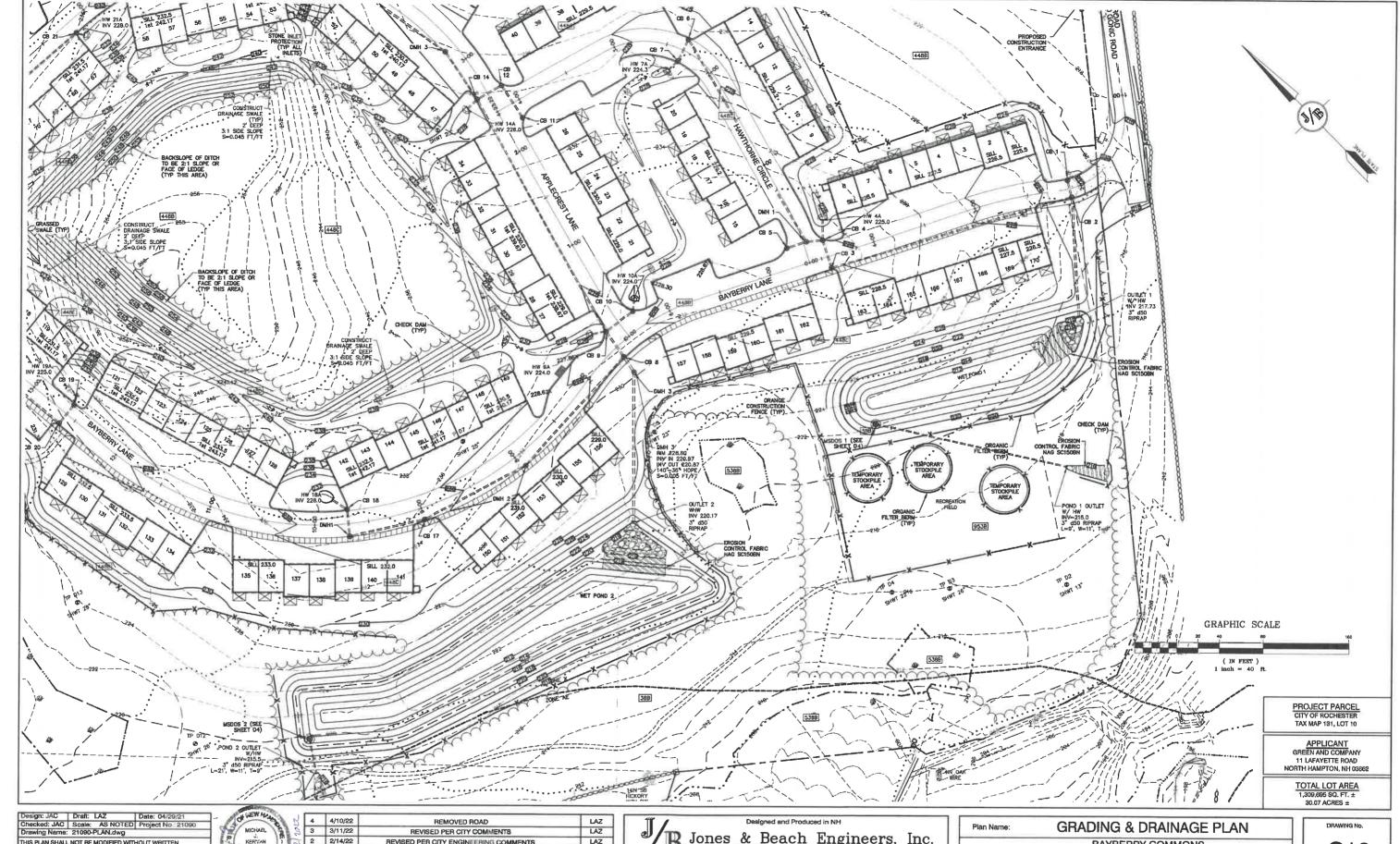
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| 2   | 2/14/22  | REVISED PER CITY ENGINEERING COMMENTS | LAZ |
| 1   | 1/18/22  | REVISED PER CITY COMMENTS             | LAZ |
| 0   | 11/23/21 | ISSUED FOR REVIEW                     | LAZ |
| REV | DATE     | REVISION                              | BV  |

Jones & Beach Engineers, Inc.

85 Portsmouth Ave. Civil Engineering Services
PO Box 219
Stretham, NH 03885
E-MAIL: JBEG Services 603-772-4746 FAX: 603-772-0227 E-MAIL: JBE@JONESANDBEACH.COM BAYBERRY COMMONS 19 OLD GONIC ROAD, ROCHESTER, NH

Owner of Record: LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148





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| MICHAEL T  | 3    | 3/11/22  | REVISED PER CITY COMMENTS             | LAZ |
| KERIVAN I  | 3 2  | 2/14/22  | REVISED PER CITY ENGINEERING COMMENTS | LAZ |
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85 Portsmouth Ave. Civil Engineering Services
PO Box 219
Stratham, NH 03885

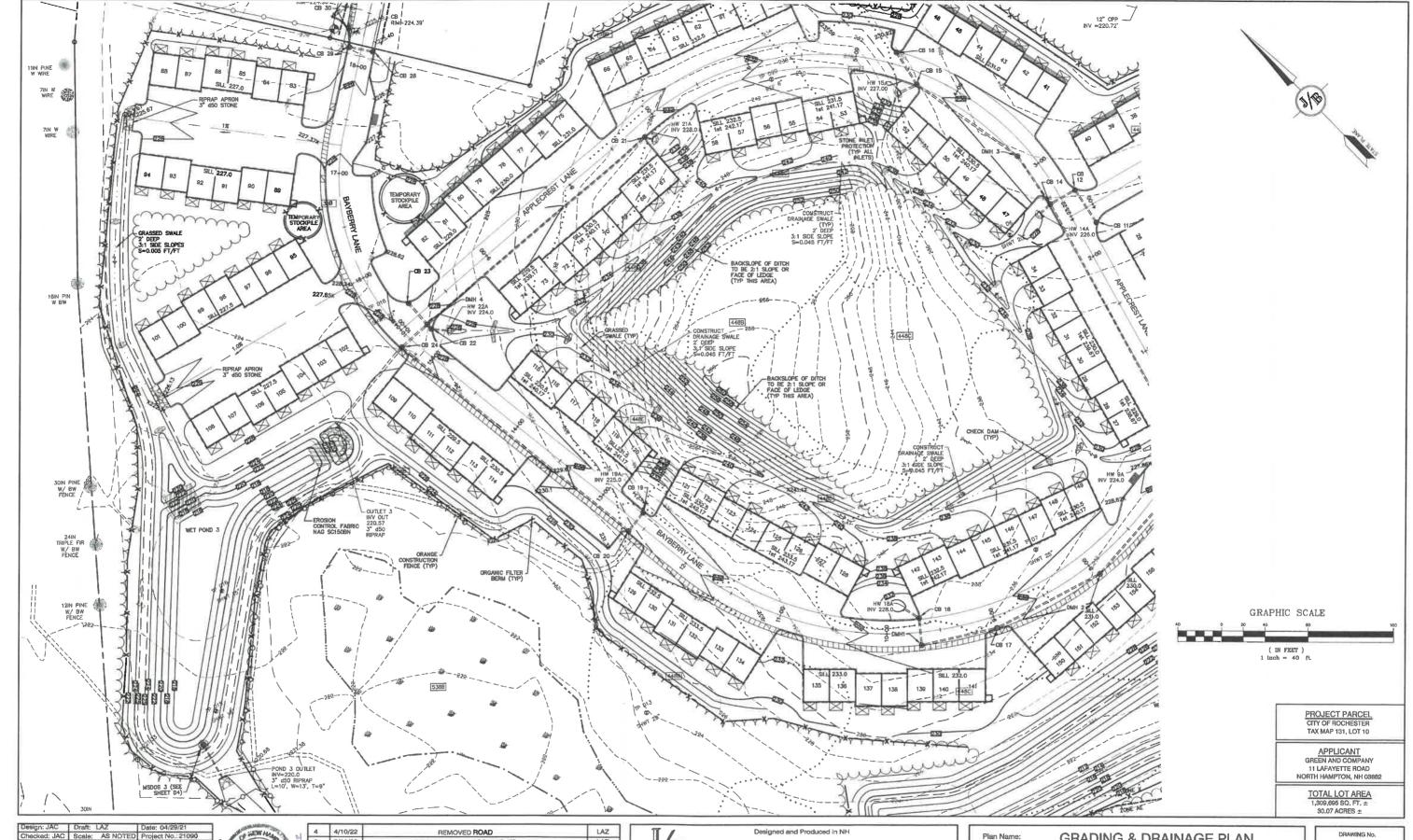
E-MAIL: JBE®

Services 603-772-4748 FAX: 603-772-0227 E-MAIL: JBE@JONESANDBEACH.COM

BAYBERRY COMMONS 19 OLD GONIC ROAD, ROCHESTER, NH Project:

Owner of Record: LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4083 PG 148

C10 SHEET 15 OF 45 JBE PROJECT NO. 21090



| Design: JAC   |                 | Date: 04/29/21     |
|---------------|-----------------|--------------------|
| Checked: JAC  | Scale: AS NOTED | Project No.: 21090 |
| Drawing Name: | 21090-PLAN.dwg  |                    |

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| ENHA.     | 4    | 4/10/22  | REMOVED ROAD                          | LAZ |
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| 713       | 3    | 3/11/22  | REVISED PER CITY COMMENTS             | LAZ |
| MICHAEL I | 2    | 2/14/22  | REVISED PER CITY ENGINEERING COMMENTS | LAZ |
| KERIVAN 1 | 1    | 1/18/22  | REVISED PER CITY COMMENTS             | LAZ |
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Jones & Beach Engineers, Inc.

B5 Portsmouth Ave. PO Box 219
Stratham, NH 03885

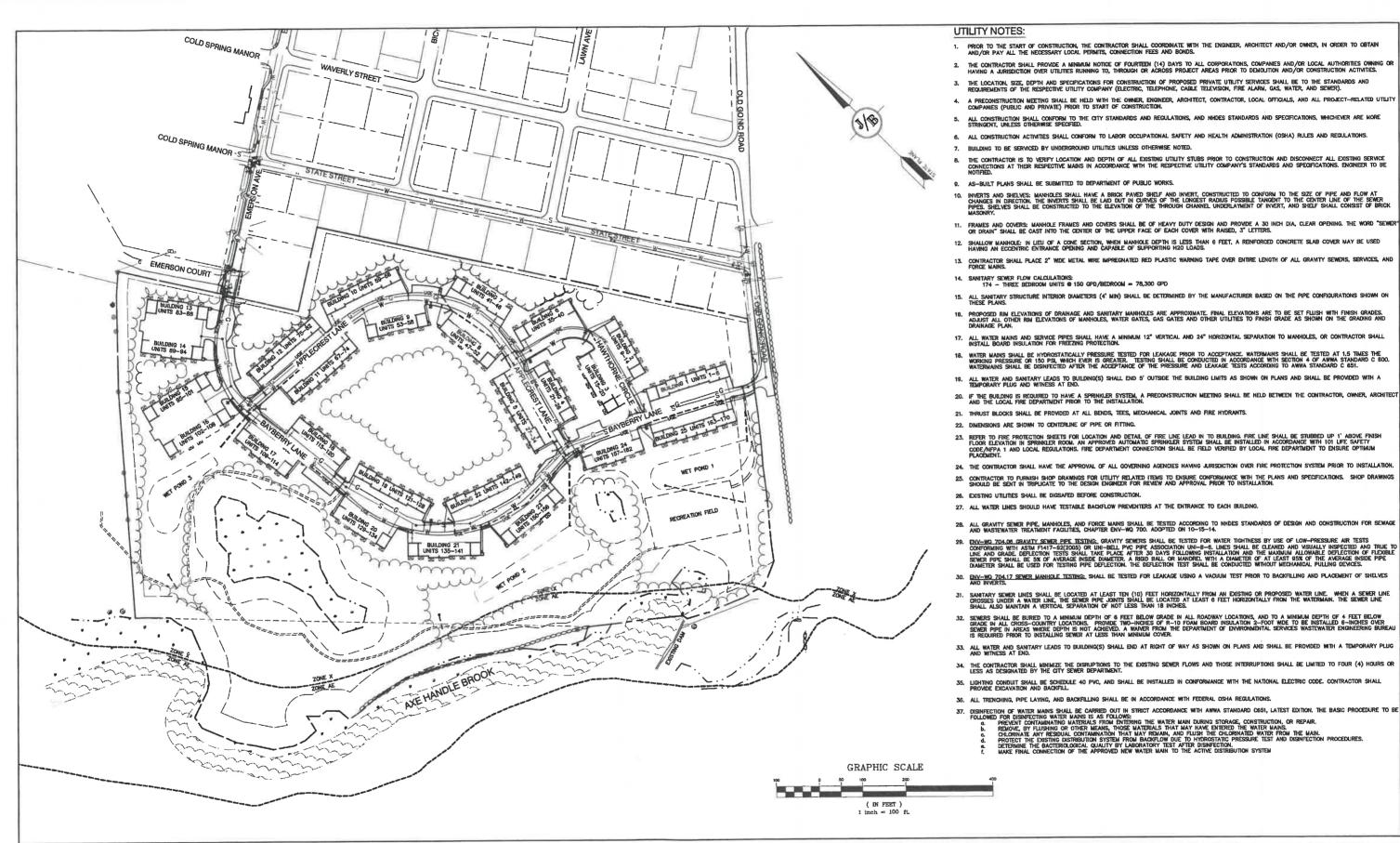
Civil Engineering Services
E-MAIL: JBE@ Services 603-772-4746 FAX: 803-772-0227 E-MAIL: JBE@JONESANDBEACH.COM

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| Plan Name: | GRADING | & | <b>DRAINAGE</b> | PL | AN |

BAYBERRY COMMONS 19 OLD GONIC ROAD, ROCHESTER, NH

Owner of Record: LEO P, LACOUTURE REV. TRUST & WILLIAN B, LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148

C11 SHEET 16 OF 45 JBE PROJECT NO. 21090



Design: JAC Draft: LAZ Date: 04/29/21
Checked: JAC Scale: AS NOTED Project No.: 21090
Drawing Name: 21090-PLAN.dwg

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| WEW HALL   | 4    | 4/10/22  | REMOVED ROAD                          | LAZ |
| MICHAEL  | 2 3  | 3/11/22  | REVISED PER CITY COMMENTS             | LAZ |
| 7. / 当日  | 2 2  | 2/14/22  | REVISED PER CITY ENGINEERING COMMENTS | LAZ |
| KERIVAN I  | 12   | 1/18/22  | REVISED PER CITY COMMENTS             | LAZ |
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Jones & Beach Engineers, Inc.

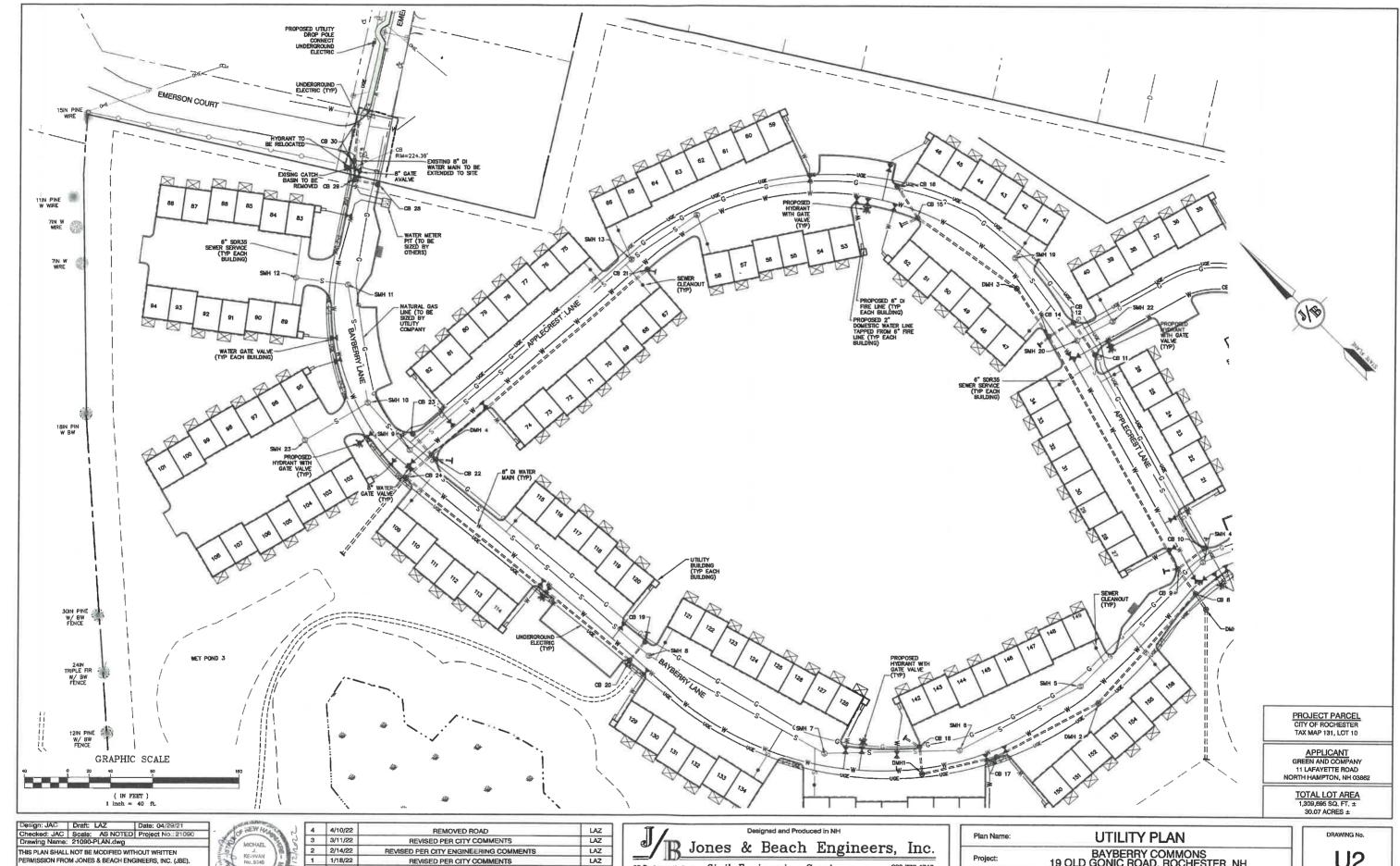
85 Portsmouth Ave. Civil Engineering Services
PO Box 219
Stretham, NH 03885
E-MAIL: JBE@

ring Services 603-772-4746 FAX: 603-772-0227 E-MAIL: JBE@JONESANDBEACH.COM Plan Name: OVERVIEW UTILITY PLAN

Project: BAYBERRY COMMONS 19 OLD GONIC ROAD, ROCHESTER, NH

Owner of Record: LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148





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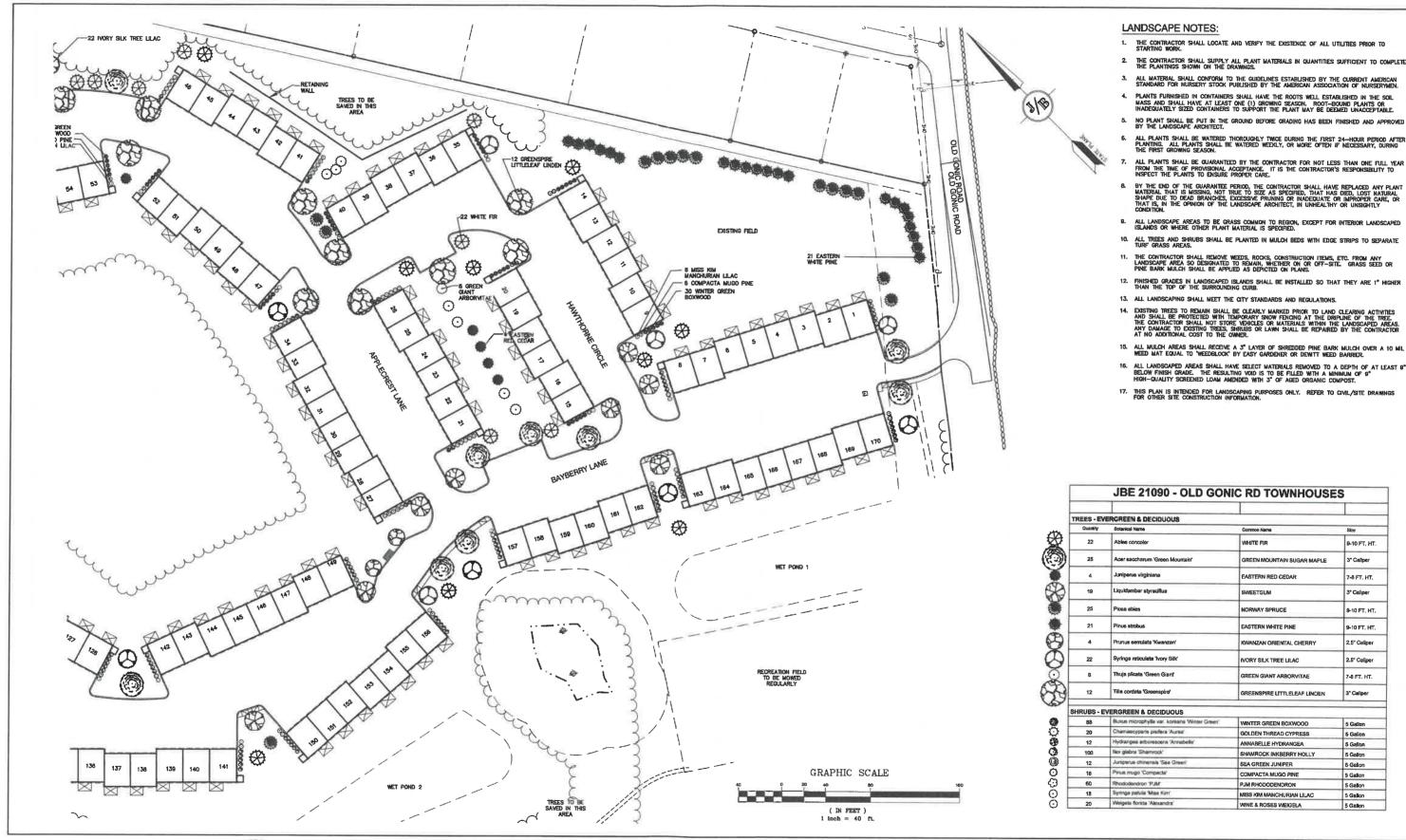
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B Jones & Beach Engineers, Inc.

as Portsmouth Ave. Civil Engineering Services
PO Box 219
Stratham, NH 03885

E-MAIL: JBE@ Services 603-772-4746 FAX: 603-772-0227 E-MAIL: JBE@JONESANDBEACH.COM

BAYBERRY COMMONS 19 OLD GONIC ROAD, ROCHESTER, NH LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148



| Design: JAC     | Draft: LAZ                                   | Date: 04/29/21      |
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| Checked: JAC    | Scale: AS NOTED                              | Project No.: 21090  |
| Drawing Name:   | 21090-PLAN.dwg                               |                     |
| THIS PLAN SHALL | NOT BE MODIFIED WITH                         | HOUT WRITTEN        |
| PERMISSION FRO  | M JONES & BEACH ENG                          | INEERS, INC. (JBE). |
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| 0    | 11/23/21 | ISSUED FOR REVIEW                     | LAZ |
| REV. | DATE     | REVISION                              | BY  |

Designed and Produced in NH B Jones & Beach Engineers, Inc.

85 Portsmouth Ave. PO Box 219
Stratham, NH 03885

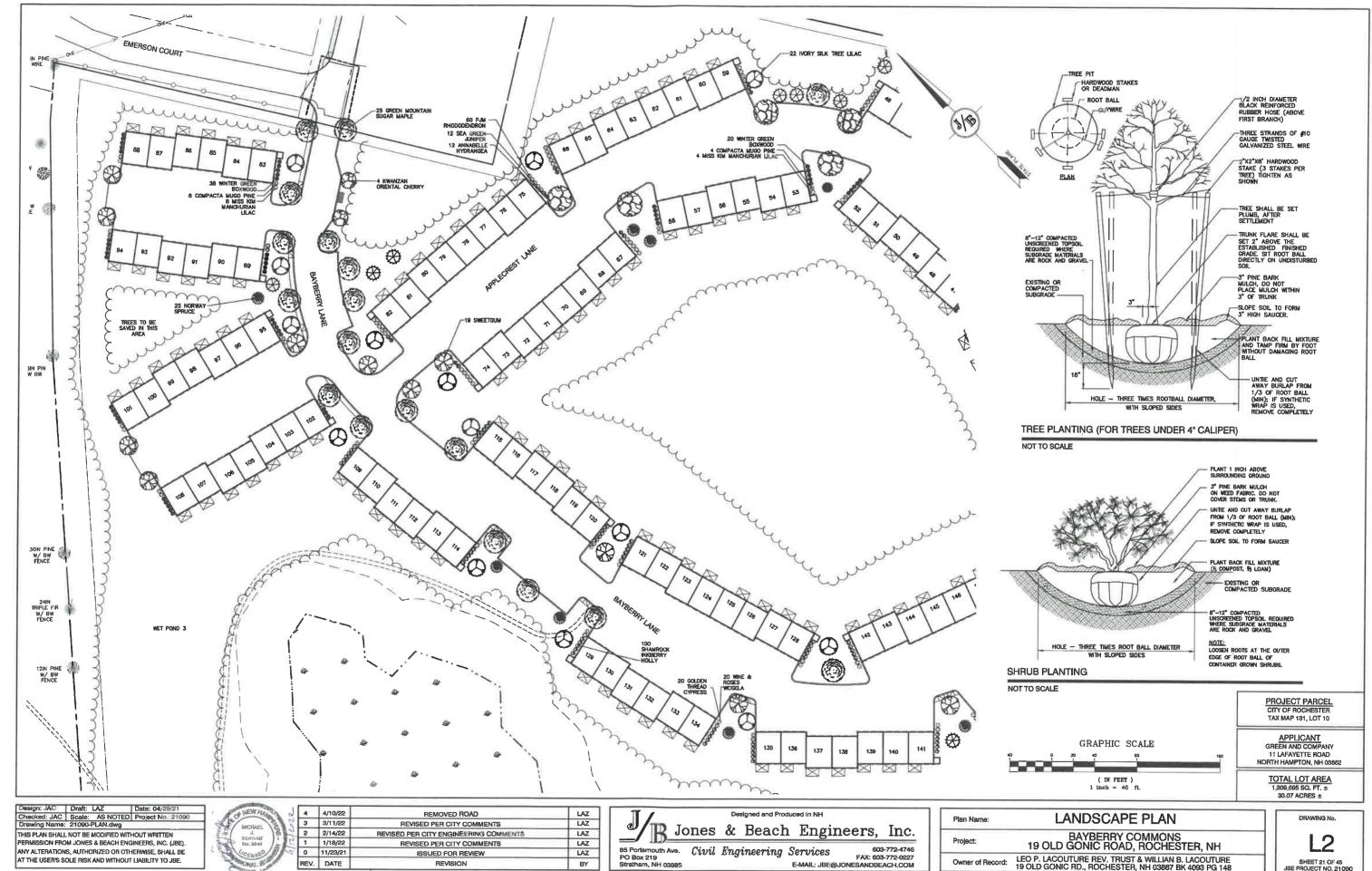
RE-MAIL: JBE@ FAX: 603-772-0227 E-MAIL: JBE@JONESANDBEACH.COM

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| an Name: |  | L | A | N |

NDSCAPE PLAN BAYBERRY COMMONS 19 OLD GONIC ROAD, ROCHESTER, NH

LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148

DRAWING No. SHEET 20 OF 45 JBE PROJECT NO. 21090



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REV. DATE

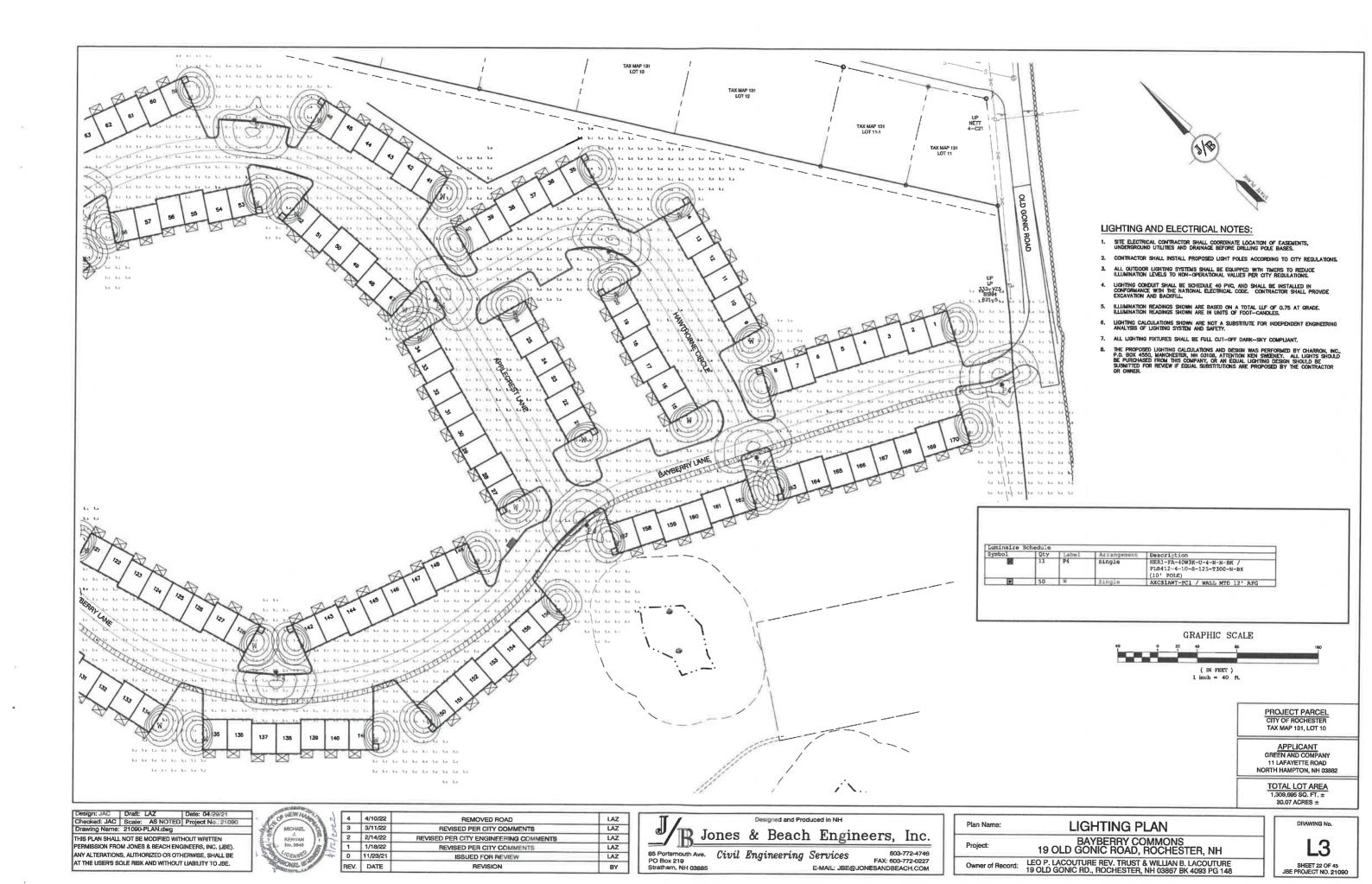
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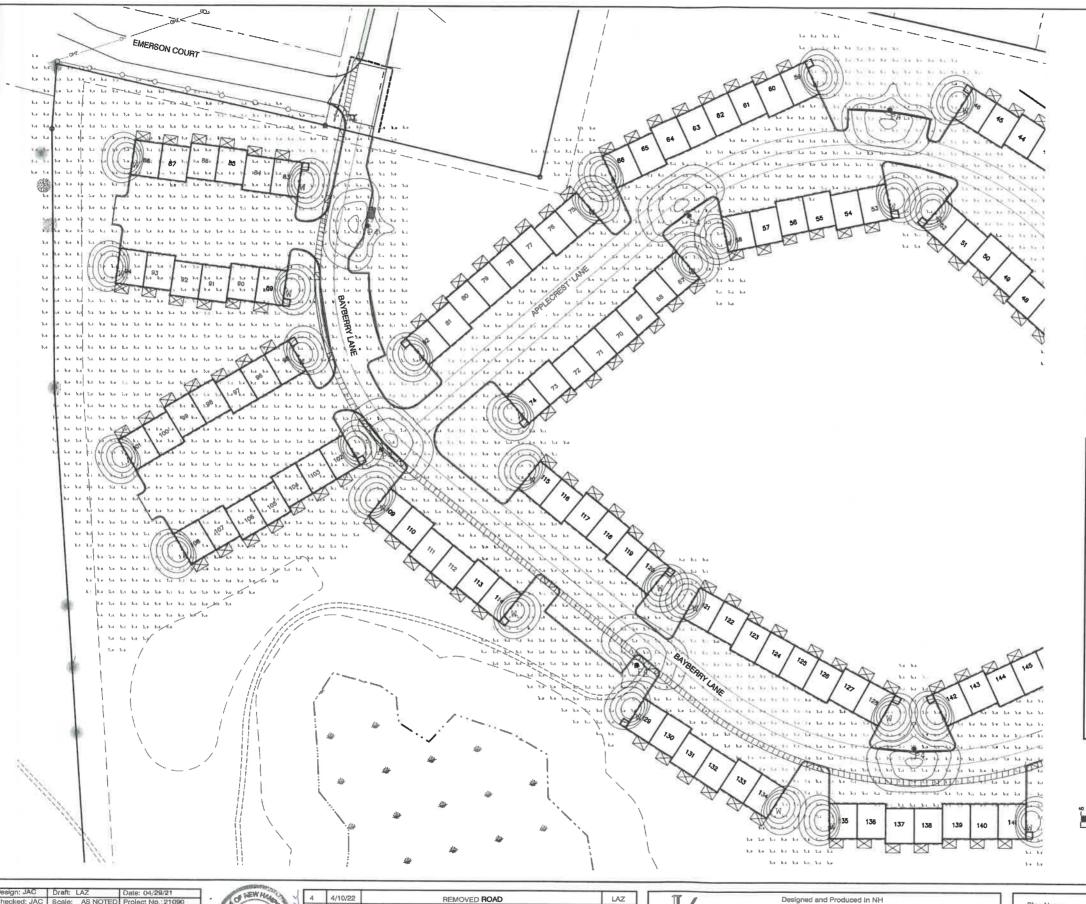
REVISION

603-772-4746

Owner of Record: LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148

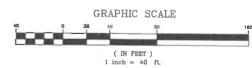
Services FAX: 603-772-0227 E-MAIL: JBE@JONESANDBEACH.COM











PROJECT PARCEL CITY OF ROCHESTER TAX MAP 131, LOT 10

APPLICANT
GREEN AND COMPANY
11 LAFAYETTE ROAD
NORTH HAMPTON, NH 03882

TOTAL LOT AREA 1,309,695 SQ. FT. ± 30.07 ACRES ±

| Design: JAC     | Drait:  | LAZ      | Date: 04/29/21     |
|-----------------|---------|----------|--------------------|
| Checked: JAC    | Scale:  | AS NOTED | Project No.: 21090 |
| Drawing Name:   | 21090-F | PLAN.dwg |                    |
| THIS PLAN SHALL |         |          |                    |
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PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE). ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.

| AND DESCRIPTION OF THE PERSON |      |          |                                       |     |
|---|------|----------|---------------------------------------|-----|
| OF REW HOLE   | 4    | 4/10/22  | REMOVED ROAD                          | LAZ |
| MICHAEL A   | 3    | 3/11/22  | REVISED PER CITY COMMENTS             | LAZ |
| MICHAEL<br>J.<br>KERIVAN  | 2    | 2/14/22  | REVISED PER CITY ENGINEERING COMMENTS | LAZ |
| No. 9848  | 1    | 1/18/22  | REVISED PER CITY COMMENTS             | LAZ |
| CICENSEO  | 0    | 11/23/21 | ISSUED FOR REVIEW                     | LAZ |
| GONEL B   | REV. | DATE     | REVISION                              | BY  |

Designed and Produced In NH B Jones & Beach Engineers, Inc.

Services 603-772-4746 FAX: 603-772-0227 E-MAIL: JBE@JONESANDBEACH.COM 85 Portsmouth Ave. PO Box 219
Stretham, NH 03885

RE-MAIL: JBE@

| Name: | LIGHTING | PLAN |
|-------|----------|------|
|-------|----------|------|

Project: BAYBERRY COMMONS
19 OLD GONIC ROAD, ROCHESTER, NH

Owner of Record: LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE
19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148

L4 SHEET 23 OF 45 JBE PROJECT NO. 21090



LAZ

LAZ

BY

#### NOTES:

- ALL ROAD AND DRAINAGE WORK SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE STANDARD SPECIFICATIONS FOR THE CITY, AND NHDOT SPECIFICATIONS FOR ROAD AND BRIDGE CONSTRUCTION, WHICHEVER IS MORE
- AS-BUILT PLANS TO BE SUBMITTED TO THE CITY PRIOR TO ACCEPTANCE OF THE ROADWAY.
- DEVELOPER IS RESPONSIBLE FOR COMPLYING WITH ALL APPLICABLE LOCAL, STATE AND FEDERAL WETLAND REGULATIONS, INCLUDING ANY PERMITTING AND SETBACK REQUIREMENTS REQUIRED UNDER THESE REGULATIONS.
- CONTRACTOR TO COORDINATE AND COMPLETE ALL WORK REQUIRED FOR THE RELOCATION AND/OR INSTALLATION OF ELECTRIC, CATV, TELEPHONE, AND FIRE ALARM PER UTILITY DESIGN AND STANDARDS, LOCATIONS SHOWN ARE APPROXIMATE. LOW PROFILE STRUCTURES SHALL BE USED TO THE GREATEST EXTENT POSSIBLE.
- THIS PLAN HAS BEEN PREPARED BY JONES & BEACH ENGINEERS, INC. FOR MUNICIPAL AND STATE APPROVALS AND FOR CONSTRUCTION BASED ON DATA GRIANED FROM ON-SITE FIELD SURVEY AND EDSTING MUNICIPAL RECORDS. THROUGHOUT INTE CONSTRUCTION PROCESS, THE CONTRACTOR SHALL INFORM THE ENGINEER IMMEDIATELY OF ANY FIELD DISCREPANCY FROM DATA SHOWN ON THE DESIGN PLANS. THIS INCLUDES ANY UNFORESEEN CONDITIONS, SUBSURFACE OR OTHERWISE, FOR EVALUATION AND RECOMMENDATIONS. ANY CONTRADICTION BETWEEN TEMS OF THIS PLANYFUAN SET, OR BETWEEN THE PLANS AND ON-SITE CONDITIONS MUST BE RESOLVED BEFORE RELATED CONSTRUCTION HAS BEEN INITIATED.
- SILTATION AND EROSION CONTROLS SHALL BE INSTALLED PRIOR TO CONSTRUCTION, SHALL BE MAINTAINED DURING CONSTRUCTION, AND SHALL REMAIN UNTIL STE HAS BEEN STABILIZED WITH PERMANENT VEGETATION SEE DETAIL SHEET ET FOR ADDITIONAL NOTES ON EROSION CONTROL
- ALL DISTURBED AREAS NOT STABILIZED BY NOVEMBER 1st SHALL BE COVERED WITH AN EROSION CONTROL BLANKET. PRODUCT TO BE SPECIFIED BY THE ENGINEER.
- 8. FINAL DRAINAGE, GRADING AND EROSION PROTECTION MEASURES SHALL CONFORM TO REGULATIONS OF THE
- 9. CONTRACTOR TO VERIFY EXISTING UTILITIES AND TO NOTIFY ENGINEER OF ANY DISCREPANCY IMMEDIATELY.
- ROADWAY INTERSECTIONS WITH SLOPE GRANITE CURB SHALL EXTEND AROUND RADIUS WITH 6' STRAIGHT PIECE ALONG TANGENT

- 13. ALL DRIVEWAYS TO BE CONSTRUCTED MAXIMUM 10% SLOPE SEE DETAIL SHEET.
- 14. SIDEWALK TO BE INSTALLED AT TIME OF TOP COURSE PAYING ALONG WITH DRIVEWAY APRONS.
- DRAINAGE INSPECTION AND MAINTENANCE SCHEDULE; SIT FENCING WILL BE INSPECTED DURING AND AFTER STORM EVENTS TO ENSURE THAT THE FENCE STILL HAS INTEGRITY AND IS NOT ALLOWING SEDIMENT TO PASS. SEDIMENT BUILD UP IN SWALES WILL BE REMOVED IF IT IS DEFERT THAN SIX INCHES, AND IS TO BE REMOVED FORM SUMPS BELOW THE INJECT OF CULVETS SEMANNUALLY, AS WELL AS FROM CATCH BASINS, FOLLOWING MAJOR STORM EVENTS, THE STAGE DISCHARGE OUTLET STRUCTURES ARE TO BE INSPECTED AND ANY DEBRIS REMOVED FROM THE ORDINGE, TRASH TRACK AND EMERGENCY SPILL WAY. INFREQUENTLY, SEDIMENT MAY ALSO HAVE TO BE REMOVED FROM THE ORDING. TRASH TRACK AND EMERGENCY SPILL WAY. INFREQUENTLY, SEDIMENT MAY ALSO HAVE TO BE REMOVED FROM THE ORDING.
- 16. ALL DRAINAGE INFRASTRUCTURE SHALL BE INSTALLED AND STABILIZED PRIOR TO DIRECTING ANY RUNOFF TO IT
- DETENTION PONDS REQUIRE TIMELY MAINTENANCE AND SHOULD BE INSPECTED AFTER EVERY MAJOR TO THE PERFORMANT RUNGE FOR THE TOTAL SWELL AS PREQUENTLY DURNO THE PIEST YEAR OF OPERATION, AND ANNUALLY THEREAFTER, EVERY FIVE YEARS, THE SERVICES OF A PROFESSIONAL ENGINEER SHOULD BE RETAINED TO PERFORM A THOROUGH INSPECTION OF THE DETENTION AND BITS IN THIS THE SHOULD BE RETAINED TO PERFORM A THOROUGH SHOULD BE REMOVED FROM THE OUTLET STRUCTURE(S) AND EMERGENCY SPILLWAY(S) AND DISPOSED OF PROFERLY, DETENTION POND BERMS SHOULD BE ROUGH STRUCTURE AND EMERGENCY SPILLWAY(S) AND DISPOSED OF PROFERLY, DETENTION FOND BERMS SHOULD BE ROUGH STRUCTURE AND EMERGENCY SPILLWAY(S) AND DISPOSED OF BESTALDETHING THE STRUCTURE AND INCREASE THE POTENTIAL FOR FAILURE AREAS SHOWING SIGNS OF EROSION OR THIN OR DYING VEGETATION SHOULD BE REPAIRED IMMEDIATELY BY WHATEVER MEANS INCESSARY, WITH THE EXCEPTION OF FERTILIZER RODERT BORROWS SHOULD BE REPAIRED IMMEDIATELY BY WHATEVER MAD THE ANSWERS AND THE ANIMALS SHOULD BE TRAPPED AND RELOCATED IF THE PROBLEM PERSISTS.
- THE DETENTION PONDS ARE TO BE CONSTRUCTED PRIMABILTY THROUGH PECANATION. IN THOSE AREAS WHERE THE BERMS MUST BE CONSTRUCTED BY THE PLACEMENT OF FILL, THE ENTIRE EMBANGMENT AREA OF THE DETENTION PONDS SHALL BE EXCANATED TO PROPOSED GRADE, STRIPPED OF ALL ORGANIC MATERIALS. IN THE CHART THE FOUNDATION MATERIAL EXCOMPACTED TO AT LEAST 95% AND SCARRIED PROR TO THE PLACEMENT OF THE EMBANIMENT MATERIAL. IN THE EVENT THE FOUNDATION MATERIAL DEPOSED DOES NOT ALLOW THE SPECIFIED COMPACTION, AN ADDITIONAL ONE FOOT (1) THOSE, THE PLACEMENT OF A ONE FOOT (1) THOSE, THE PLACEMENT OF THE MATERIAL DESCRIBED IN THE NOTE BELOW, COMPACTION, DO "THE MATERIAL DESCRIBED IN THE NOTE BE OF THE MATERIAL DESCRIBED IN THE NOTE BELOW, COMPACTION OF OPTIMUM PLUS OR MINUS 3%, AND NO PROCESS OR GRANKE MATERIAL SHOULD COLD THE MATERIAL SHOULD COLD THE MATERIAL SHOULD COLD THE SHOULD COLD THEM THE MATERIAL SHOULD COLD THE MATERIAL SHOULD COLD THE MATERIAL SHOULD COLD THE MATERIAL SHOULD COL
- 19. EMBANIQUENT MATERIAL FOR THE BERMS SHALL BE CLEAN MINERAL SOIL WITH A CLAY COMPONENT FREE OF ROOTS, ORGANIC MATTER, AND OTHER DELETERIOUS SUBSTANCES, AND SHALL CONTAIN NO ROCKS OR LUMPS OVER FOUR INCHES (4") IN DIAMETER. THIS MATERIAL SHOULD BE INSTALLED IN 6" LIFTS AND COMPACTED TO 95% OS ASTIM D-1957, AND SHOULD MEET THE FOLLOWING SPECIFICATIONS: 4" PASSING 100%, §4 SIEVE 25-70%, §200 SIEVE 10-29% (IN TOTAL SAMPLE).
- 20. EMBANIONENT IS TO HAVE 3:1 SIDE SLOPES (MAX.) AND IS TO BE BROUGHT TO SPECIFIED GRADES PRIOR TO THE ADDITION OF LOAM (4" MINISUM) SO AS TO ALLOW FOR THE COMPACTION OF THE STRUCTURE OVER TIME WHILE MAINTAINING THE PROPER BERM ELEVATION.
- COMPACTION TESTING SERVICES (I.E. NUCLEAR DENSITY TESTS) ARE TO BE PERFORMED BY AN INDEPENDENT GEOTECHNICAL ENGINEER RETAINED BY THE CONTRACTOR FOR ROADWAY CONSTRUCTION, AND ON THE FOUNDATION OF THE BERM AND ON EVERY LIFT OF NEWLY PLACED MATERIAL.
- 22. SLOPED GRANITE CURB TO BE TIPPED DOWN AT ALL DRIVEWAY ENTRANCES BY THE CONTRACTOR.

GRAPHIC SCALE ( IN FEET )

1 inch = 40 ft Horiz.
1 inch = 4 ft Vert.

**BAYBERRY LANE** 

ERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE). ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.

| 4    | 4/10/22  | REMOVED ROAD                      |
|------|----------|-----------------------------------|
| 7 3  | 3/11/22  | REVISED PER CITY COMMENTS         |
| 9 2  | 2/14/22  | REVISED PER CITY ENGINEERING COMM |
| 61 1 | 1/18/22  | REVISED PER CITY COMMENTS         |
| 0    | 11/23/21 | ISSUED FOR REVIEW                 |
| REV. | DATE     | REVISION                          |

Jones & Beach Engineers, Inc.

as Portsmouth Ave. Civil Engineering Services
PO Box 219

E-MAIL: JBE@JONESANDBEACH,COM

PLAN AND PROFILE

BAYBERRY COMMONS 19 OLD GONIC ROAD, ROCHESTER, NH Project:

LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148 Owner of Record:

DRAWING No. SHEET 24 OF 45 JBE PROJECT NO.21090



|                |                     |                             | Project No.: 21090   |
|----------------|---------------------|-----------------------------|--|
| Drawing Name:  | 21090-              | PLAN.dwg                    |  |
| ANY ALTERATION | M JONES<br>S, AUTHO | & BEACH ENG<br>RIZED OR OTH | HOUT WRITTEN<br>BINEERS, INC. (JBE).<br>HERWISE, SHALL BE<br>LIABILITY TO JBE. |

| COPW MA   | 4    | 4/10/22  | REMOVED ROAD                          | LAZ |
|-----------|------|----------|---------------------------------------|-----|
| 0         | 3    | 3/11/22  | REVISED PER CITY COMMENTS             | LAZ |
| MECHAEL 3 | 2    | 2/14/22  | REVISED PER CITY ENGINEERING COMMENTS | LAZ |
| KERIVAN I | 1    | 1/18/22  | REVISED PER CITY COMMENTS             | LAZ |
| No. 9848  | 0    | 11/23/21 | ISSUED FOR REVIEW                     | LAZ |
| CENSE     | REV. | DATE     | REVISION                              | BY  |

Jones & Beach Engineers, Inc.

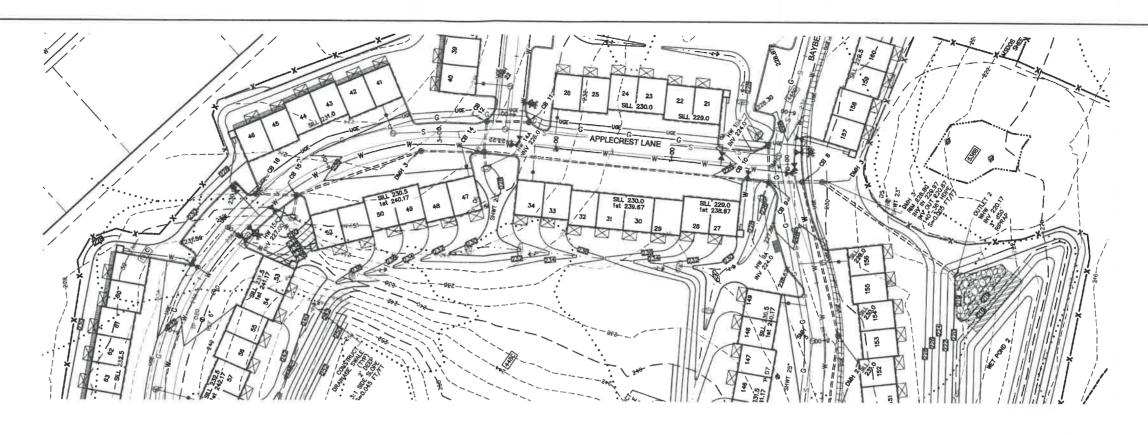
St Portsmouth Ave. Civil Engineering Services 603-772-4748
PO Box 219 FAX: 603-772-0227
Stratham, NH 03885 E-MAIL: JBE@JONESANDBEACH.COM

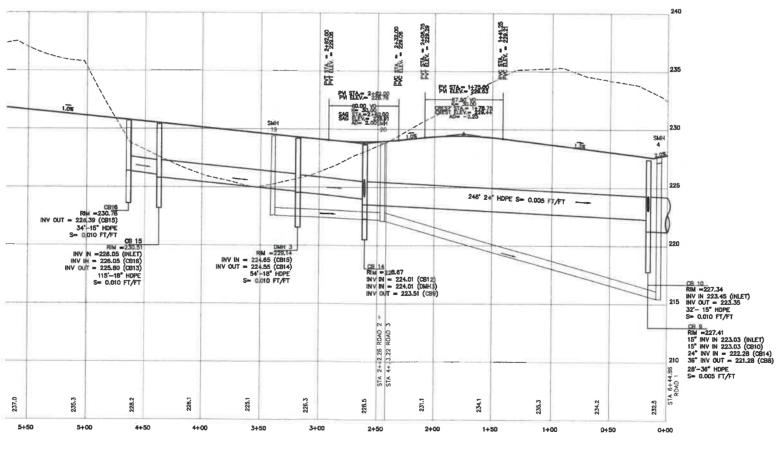
| Plan Name: | PLAN AND PROFILE |
|------------|------------------|
| Project:   | BAYBERRY COMMONS |

Owner of Record: 19 OLD GONIC ROAD, ROCHESTER, NH

LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE
19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148







GRAPHIC SCALE
(IN FEET)
linch = 40 ft Horiz.
linch = 4 ft Vert.

| Design: JAC     | Draft: LAZ           | Date: 04/29/21      |
|-----------------|----------------------|---------------------|
| Checked: JAC    | Scale: AS NOTED      | Project No.: 21090  |
| Drawing Name:   | 21090-PLAN.dwg       |                     |
| THIS PLAN SHALL | NOT BE MODIFIED WITH | HOUT WRITTEN        |
| PERMISSION FRO  | M JONES & BEACH ENG  | INEERS, INC. (JBE). |
|                 | S ALITHODIZED OD OTH |                     |

AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.

MICHAEL
KERWAN
NO. 9849

| 4    | 4/10/22  | REMOVED ROAD                          | LAZ |
|------|----------|---------------------------------------|-----|
| 3    | 3/11/22  | REVISED PER CITY COMMENTS             | LAZ |
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Jones & Beach Engineers, Inc.

85 Portsmouth Ave. PO Box 219
Strathern, NH 03885

Designed and Produced in NH

Engineers, Inc.

603-772-4748
FAX: 603-772-0227
E-MAIL: JBE@JONESANDBEACH.COM

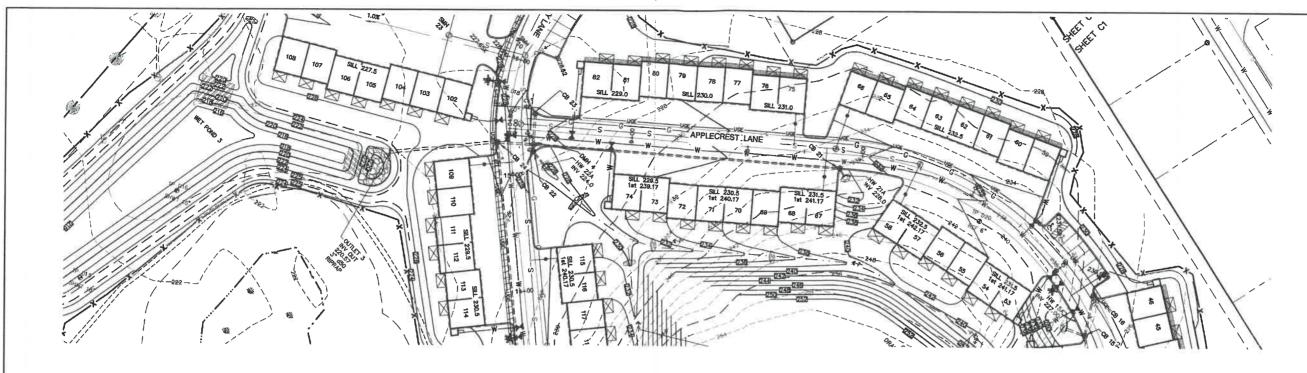
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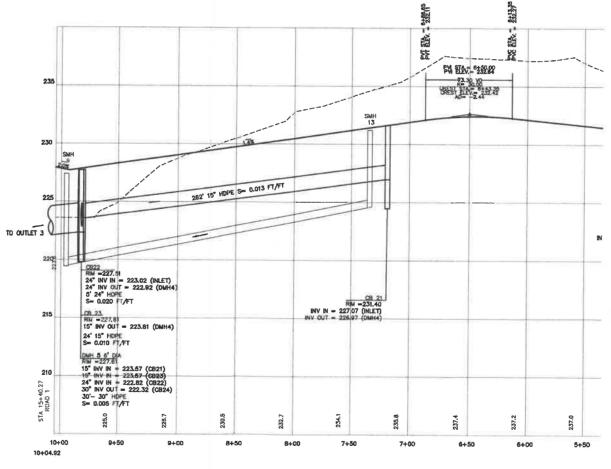
| Plan Name:       | PLAN AND PROFILE   |
|------------------|--|
| Project:         | BAYBERRY COMMONS<br>19 OLD GONIC ROAD, ROCHESTER, NH   |
| Owner of Record: | LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE<br>19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148 |

APPLECREST LANE

DRAWING No.

P3
SHEET 26 OF 45
JBE PROJECT NO. 21090





GRAPHIC SCALE
(IN FEET)
1 inch = 40 ft Horiz.
1 inch = 4 ft Vert.

APPLECREST LANE

Design: JAC Draft: LAZ Date: 04/29/21
Checked: JAC Scale: AS NOTED Project No.: 21090
Drawing Name: 21090-PLAN.dwg
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| REV. | DATE     | REVISION                              | BY  |
|------|----------|---------------------------------------|-----|
| 0    | 11/23/21 | ISSUED FOR REVIEW                     | LAZ |
| 1    | 1/18/22  | REVISED PER CITY COMMENTS             | LAZ |
| 2    | 2/14/22  | REVISED PER CITY ENGINEERING COMMENTS | LAZ |
| 3    | 3/11/22  | REVISED PER CITY COMMENTS             | LAZ |
| 4    | 4/10/22  | REMOVED ROAD                          | LAZ |

| 1/                 |      | De | signed and Prod | uced in NH |             |
|--------------------|------|----|-----------------|------------|-------------|
| JE 1               | ones | &  | Beach           | Engineers  | Inc.        |
| 85 Portsmouth Ave. |      |    | incomina        |            | 03-772-4746 |

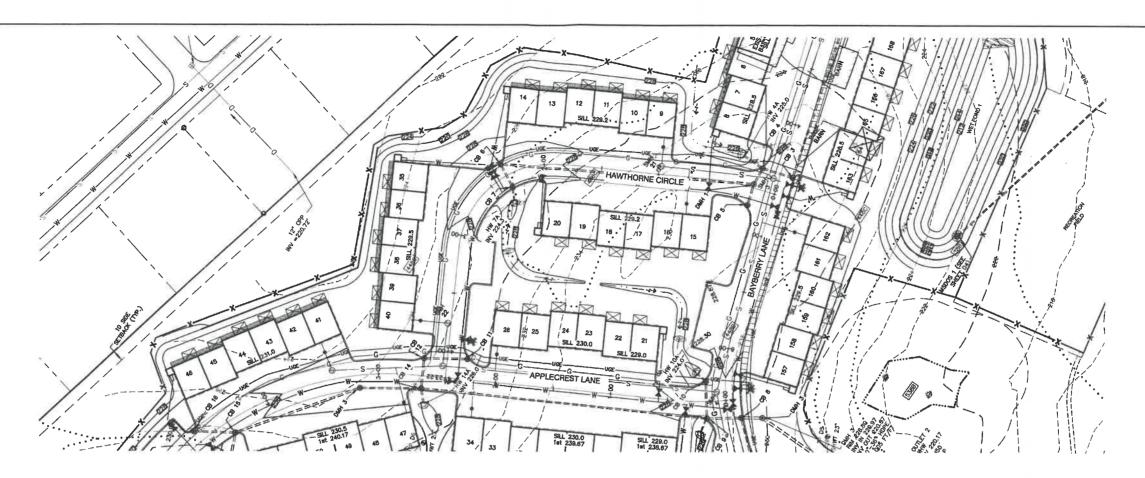
85 Portsmouth Ave. Civil Engineering Services 603-772-4746
PO Box 219 FAX: 603-772-0227
Stratham, NH 0S885 E-MAIL: JBE@JONESANDBEACH.COM

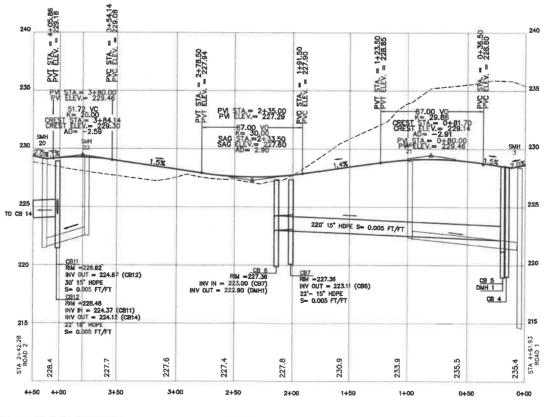
| Plan Name: | PLAN AND PROFILE |  |
|------------|------------------|--|
| Project:   | BAYBERRY COMMONS |  |

Project: 19 OLD GONIC ROAD, ROCHESTER, NH

Owner of Record: LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4083 PG 148







GRAPHIC SCALE (IN FEET )

1 inch = 40 ft Horiz.
1 inch = 4 ft Vert.

| Design: JAC  | Draft: LAZ                        | Date: 04/29/21     |
|--------------|-----------------------------------|--------------------|
| Checked: JAC | Scale: AS NOTED<br>21090-PLAN.dwg | Project No.: 21090 |

THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN
PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE). ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.

| CHEW ALA            | 4    | 4/10/22  | REMOVED ROAD                          | LAZ |
|---------------------|------|----------|---------------------------------------|-----|
|                     | 3    | 3/11/22  | REVISED PER CITY COMMENTS             | LAZ |
| MICHAEL )           | 2    | 2/14/22  | REVISED PER CITY ENGINEERING COMMENTS | LAZ |
| KERIVAN<br>No. 9843 | N 1  | 1/18/22  | REVISED PER CITY COMMENTS             | LAZ |
|                     | 0    | 11/23/21 | ISSUED FOR REVIEW                     | LAZ |
|                     | REV. | DATE     | REVISION                              | BY  |

Jones & Beach Engineers, Inc.

B5 Portsmouth Ave. Civil Engineering
PO Box 219
Stratham, NH 03885

| _ |                 |                   |
|---|-----------------|-------------------|
| , | Services        | 603-772-4746      |
| f | Delones         | FAX: 603-772-0227 |
|   | E-MAIL: JBF@.II | ONESANDBEACH COM  |

|            | HAWTHORNE CIRCLE |
|------------|------------------|
|            |                  |
| Plan Name: | PLAN AND PROFILE |

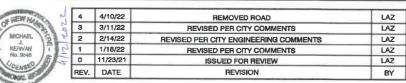
BAYBERRY COMMONS
19 OLD GONIC ROAD, ROCHESTER, NH
LEO P. LACOUTURE REV. TRUST & WILLIAM B. LACOUTURE
19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148 Project:

Owner of Record:

DRAWING No. **P5** SHEET 28 OF 45 JBE PROJECT NO.21090



THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN RMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE). ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.



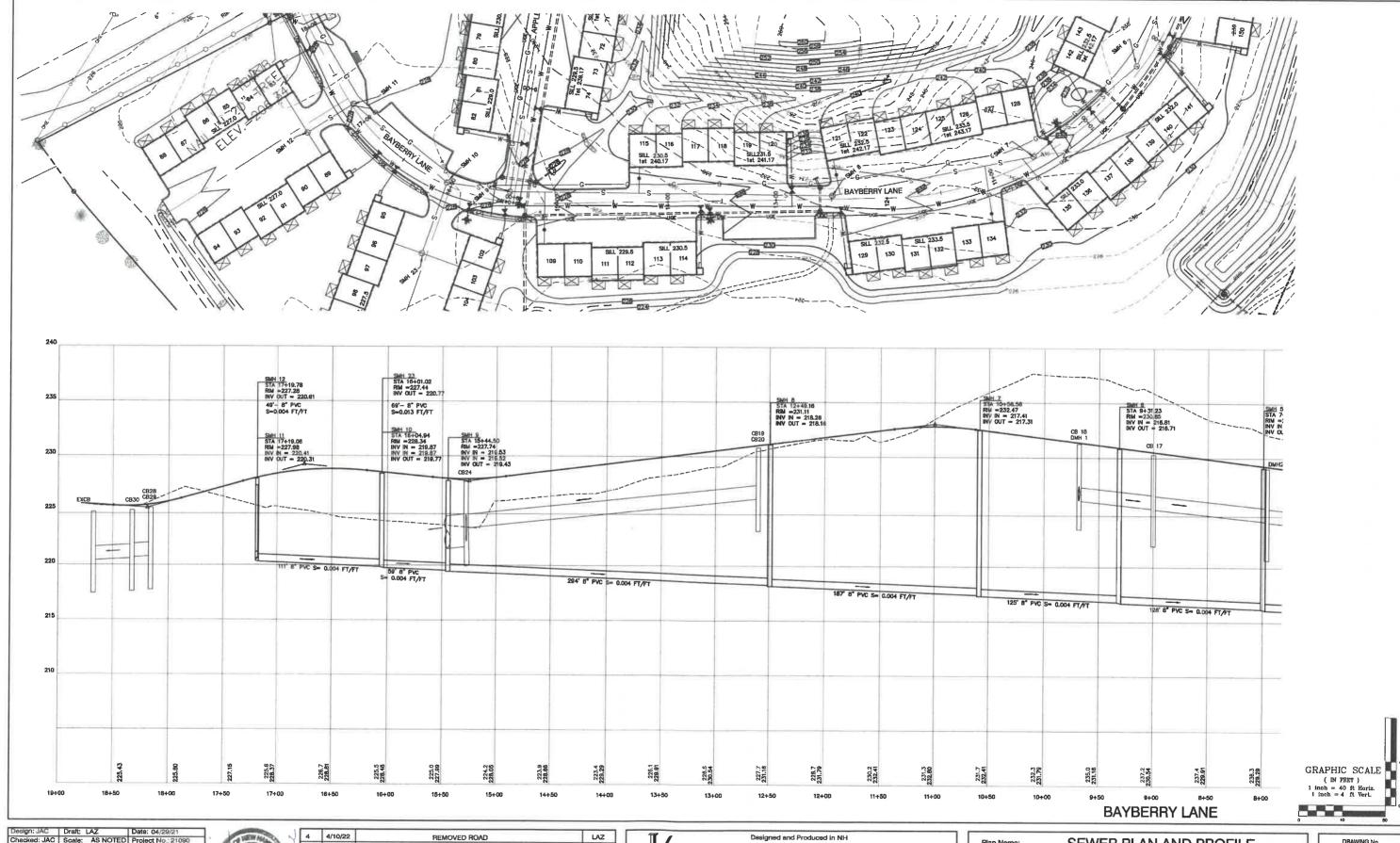
B Jones & Beach Engineers, Inc.

85 Portsmouth Ave. Civil Engineering Services
PO Box 219
Stratham, NH 03885
E-MAIL: JBE@ FAX: 603-772-0227
E-MAIL: JBE@JONESANDBEACH.COM

| Plan Name: | SEWER PLAN AND PROFILE |
|------------|------------------------|
| Project:   | BAYBERRY COMMONS       |

19 OLD GONIC ROAD, ROCHESTER, NH LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148 Owner of Record:

DRAWING No. **P6** SHEET 29 OF 45 JBE PROJECT NO.21090



Design: JAC Draft: LAZ Date: 04/29/21
Checked: JAC Scale: AS NOTED Project No.: 21090
Drawing Name: 21090-PLAN.dwg
THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN
PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE).
ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE
AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.

| A VEN HALL  | N 1   | 4/10/22  | REMOVED ROAD                          | LAZ |
|-------------|-------|----------|---------------------------------------|-----|
| 30          | 7 7 3 | 3/11/22  | REVISED PER CITY COMMENTS             | LAZ |
| MICHAEL /   | 9 2   | 2/14/22  | REVISED PER CITY ENGINEERING COMMENTS | LAZ |
| KERVAN I    | 10 1  | 1/18/22  | REVISED PER CITY COMMENTS             | LAZ |
| 4/4         | - 0   | 11/23/21 | ISSUED FOR REVIEW                     | LAZ |
| The same of | R     | V. DATE  | REVISION                              | BY  |

Jones & Beach Engineers, Inc.

85 Portsmouth Ave. Civil Engineering Services FAX: 603-772-70227 Stratham, NH 03885 E-MAIL: JBE@JONESANDBEACH.COM

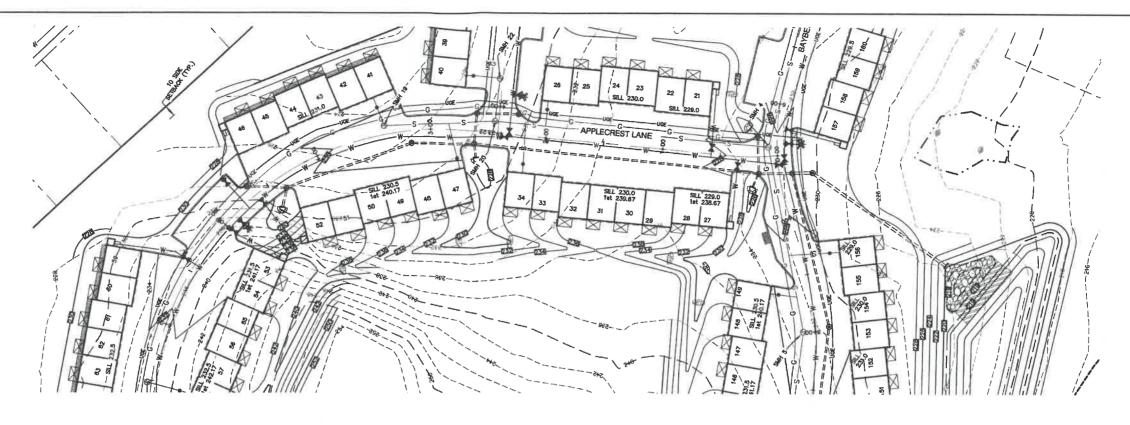
| Plan Name: | SEWER PLAN AND PROFILE |
|------------|------------------------|
|            | DAY/D====\( \)         |

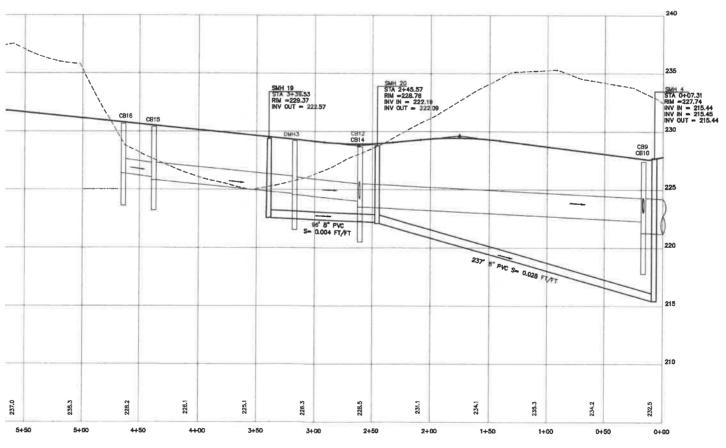
BAYBERRY COMMONS 19 OLD GONIC ROAD, ROCHESTER, NH

Owner of Record: LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148

DRAWING No.

P7
SHEET 30 OF 45
JBE PROJECT NO. 21090





GRAPHIC SCALE
(IN FEET)
1 inch = 40 ft Horts.
1 inch = 4 ft Vert.

| Design: JAC | Draft: LAZ | Date: 04/29/21 |
| Checked: JAC | Scale: AS NOTED | Project No.: 21090 |
| Drawing Name: 21090-PLAN.dwg

THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN
PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE).
ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE
AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.

| de | FREW HE             | Ch. I |
|----|---------------------|-------|
| V  | MICHAEL.            | 191   |
| 3  | KERIVAN<br>No. 9848 | )     |
| 3  | CEMBEO              |       |
| 2  | Wallians of         | -     |

| 4    | 4/10/22  | REMOVED ROAD                          | LAZ |
|------|----------|---------------------------------------|-----|
| 3    | 3/11/22  | REVISED PER CITY COMMENTS             | LAZ |
| 2    | 2/14/22  | REVISED PER CITY ENGINEERING COMMENTS | LAZ |
| 1    | 1/18/22  | REVISED PER CITY COMMENTS             | LAZ |
| 0    | 11/23/21 | ISSUED FOR REVIEW                     | LAZ |
| REV. | DATE     | REVISION                              | BY  |

Designed and Produced in NH

Jones & Beach Engineers, Inc.

85 Portsmouth Ave. Civil Engineering Services 603-772-4746
PO Box 219
Stratham, NH 03885 E-MAIL: JBE@JONESANDBEACH.COM

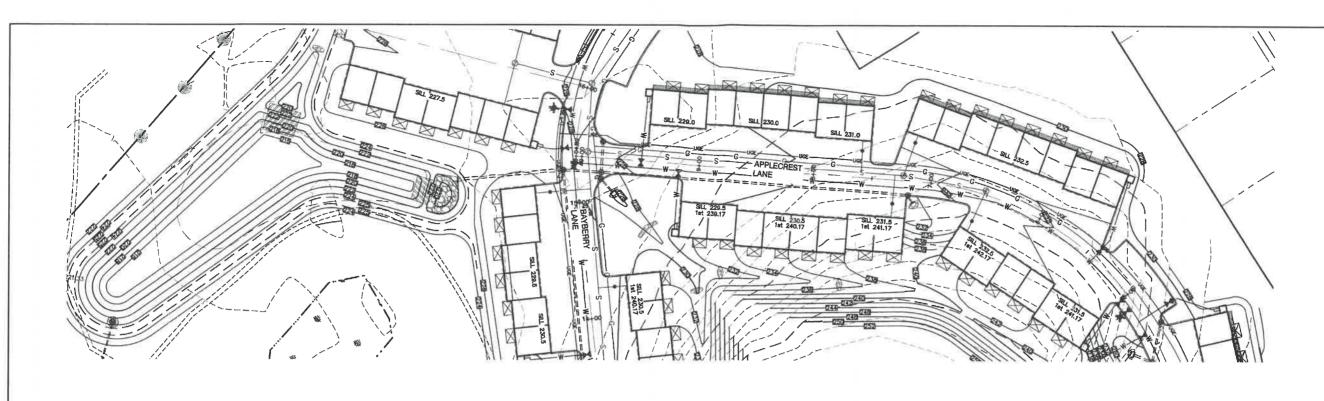
| Plan Name: | SEWER PL | AN AND P | ROFILE |
|------------|----------|----------|--------|
|            |          |          |        |

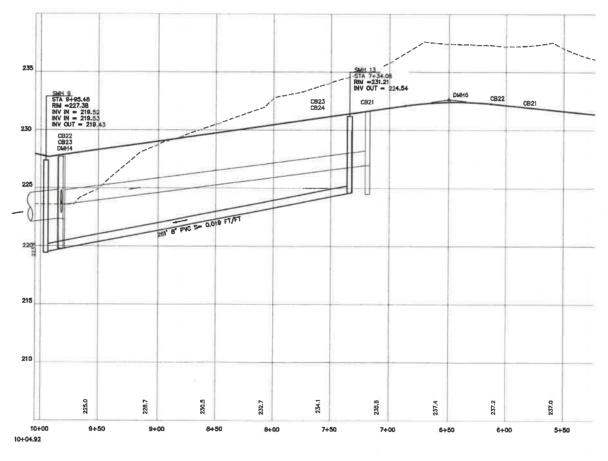
oject: BAYBERRY COMMONS 19 OLD GONIC ROAD, ROCHESTER, NH

Owner of Record: LEO P. LACOUTURE REV. TRUST & WILLIAM B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148

APPLECREST LANE







GRAPHIC SCALE
(IN PEET)
1 inch = 40 ft Horiz.
1 inch = 4 ft Vert.

APPLECREST LANE

| Design: JAC     |                      | Date: 04/29/21     |
|-----------------|----------------------|--------------------|
| Checked: JAC    | Scale: AS NOTED      | Project No.: 21090 |
| Drawing Name:   | 21090-PLAN.dwg       |                    |
| THIS PLAN SHALL | NOT BE MODIFIED WITH | HOUT WRITTEN       |

IHIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN
PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE).
ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE
AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.

| A SEW Ass. Co. 1 | 4    | 4/10/22  | REMOVED ROAD                          | LAZ |
|------------------|------|----------|---------------------------------------|-----|
|                  | 3    | 3/11/22  | REVISED PER CITY COMMENTS             | LAZ |
| AHCHAEL          | 3 2  | 2/14/22  | REVISED PER CITY ENGINEERING COMMENTS | LAZ |
| KERIVAN I C      | 3 1  | 1/18/22  | REVISED PER CITY COMMENTS             | LAZ |
| No. 9846         | 0    | 11/23/21 | ISSUED FOR REVIEW                     | LAZ |
| CEMBE            | REV. | DATE     | REVISION                              | BY  |

| 1/ |       | De | signed and Produc | ed in NH   |          |
|----|-------|----|-------------------|------------|----------|
| P  | Jones | &  | Beach             | Engineers, | Inc.     |
|    |       | _  |                   |            | 770 4740 |

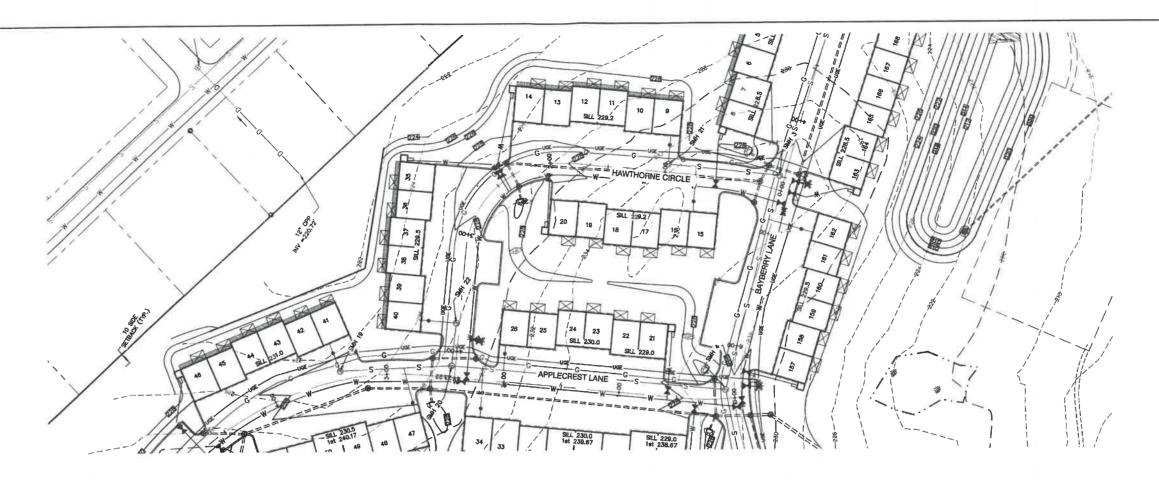
SF Portsmouth Ave. Civil Engineering Services 603-772-4748
PO Box 219
Stratham, NH 03885

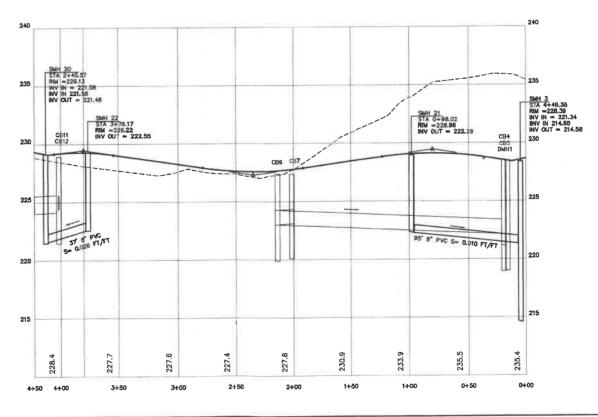
E-MAIL: JBE@JONESANDBEACH.COM

| Plan Name: | PLAN AND PROFILE                                     |
|------------|--|
| Project:   | BAYBERRY COMMONS<br>19 OLD GONIC ROAD, ROCHESTER, NH |

Owner of Record: LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148







GRAPHIC SCALE ( IN FEET )

1 inch = 40 ft Horiz.

1 inch = 4 ft Vert.

HAWTHORNE CIRCLE

Design: JAC Draft: LAZ Date: 04/29/21
Checked: JAC Scale: AS NOTED Project No.:21090
Drawing Name: 21090-PLAN.dwg Drawing Name: 27050-PDAN.0Wg
THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN
PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE).
ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE
AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.

| id | SEW MA                   | b.  |
|----|--------------------------|-----|
| 1  |                          | 1   |
| 0  | MICHAEL<br>J.<br>KERIVAN | 13  |
| M  | No. 9840                 |     |
| 10 | CICENSEO                 |     |
| 9  | WORLD LAND               | gr. |

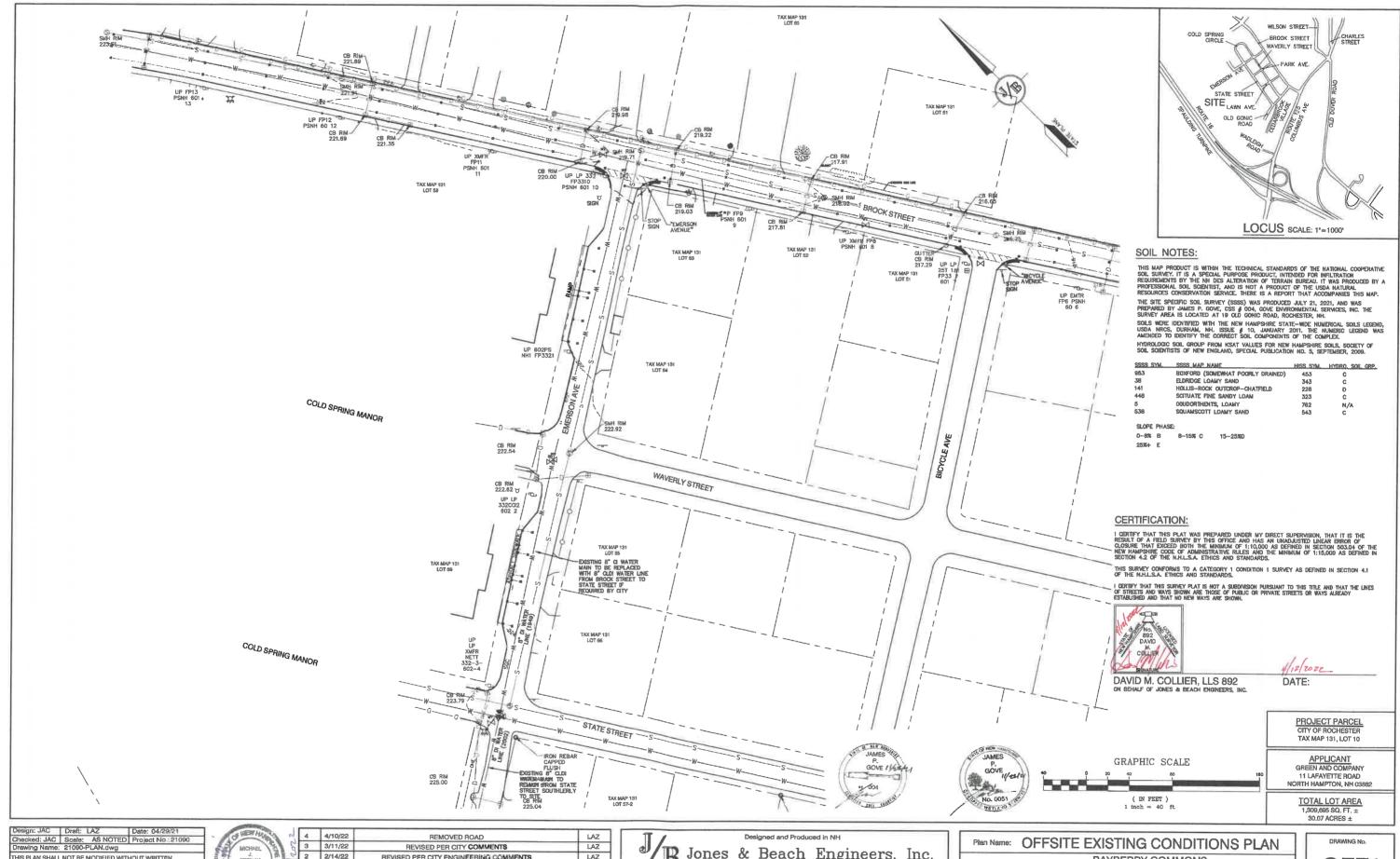
| 4    | 4/10/22  | REMOVED ROAD                          | LAZ |
|------|----------|---------------------------------------|-----|
| 3    | 3/11/22  | REVISED PER CITY COMMENTS             | LA2 |
| 2    | 2/14/22  | REVISED PER CITY ENGINEERING COMMENTS | LAZ |
| 1    | 1/18/22  | REVISED PER CITY COMMENTS             | LAZ |
| 0    | 11/23/21 | ISSUED FOR REVIEW                     | LAZ |
| REV. | DATE     | REVISION                              | BY  |

Designed and Produced in NH Jones & Beach Engineers, Inc. Services 603-772-4748 FAX: 603-772-0227 E-MAIL: JBE@JONESANDBEACH.COM

85 Portsmouth Ave. Civil Engineering Services
PO Box 219
Stratham, NH 03885
E-MAIL: JBE@

| ĺ | Plan Name: | SEWER PLAN AND PROFILE |
|---|------------|------------------------|
|   |            |                        |

BAYBERRY COMMONS 19 OLD GONIC ROAD, ROCHESTER, NH Project: Owner of Record: LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148 P10



| Design. JAC                                     | Drait.  | LAZ  |        | Date: 04/29/21                          |  |  |
|---|---------|------|--------|---|--|--|
| Checked: JAC                                    | Scale:  | AS   | NOTED  | Project No.:21090                       |  |  |
| Drawing Name:                                   | 21090-  | PLAN | .dwg   | *************************************** |  |  |
| THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN |         |      |        |   |  |  |
| PERMISSION FRO                                  | M JONES | & BE | ACH EN | GINEERS, INC. (JBE).                    |  |  |
| *****   | -       |      |        |   |  |  |

AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JIBE.

| No. of Concession, Name of Street, or other Persons, or other Pers |      |          |                                       |     |
|--|------|----------|---------------------------------------|-----|
| OF SHEW HAVE   | 4    | 4/10/22  | REMOVED ROAD                          | LAZ |
| MICHAEL &  | 3    | 3/11/22  | REVISED PER CITY COMMENTS             | LAZ |
| J. KERVAN  | 2    | 2/14/22  | REVISED PER CITY ENGINEERING COMMENTS | LAZ |
| No. 8848   | 1    | 1/18/22  | REVISED PER CITY COMMENTS             | LAZ |
| CENSE!   | 0    | 11/23/21 | ISSUED FOR REVIEW                     | LA2 |
| CONT. OF STREET  | REV. | DATE     | REVISION                              | BY  |
| Linkshipman  |      |          |                                       |     |

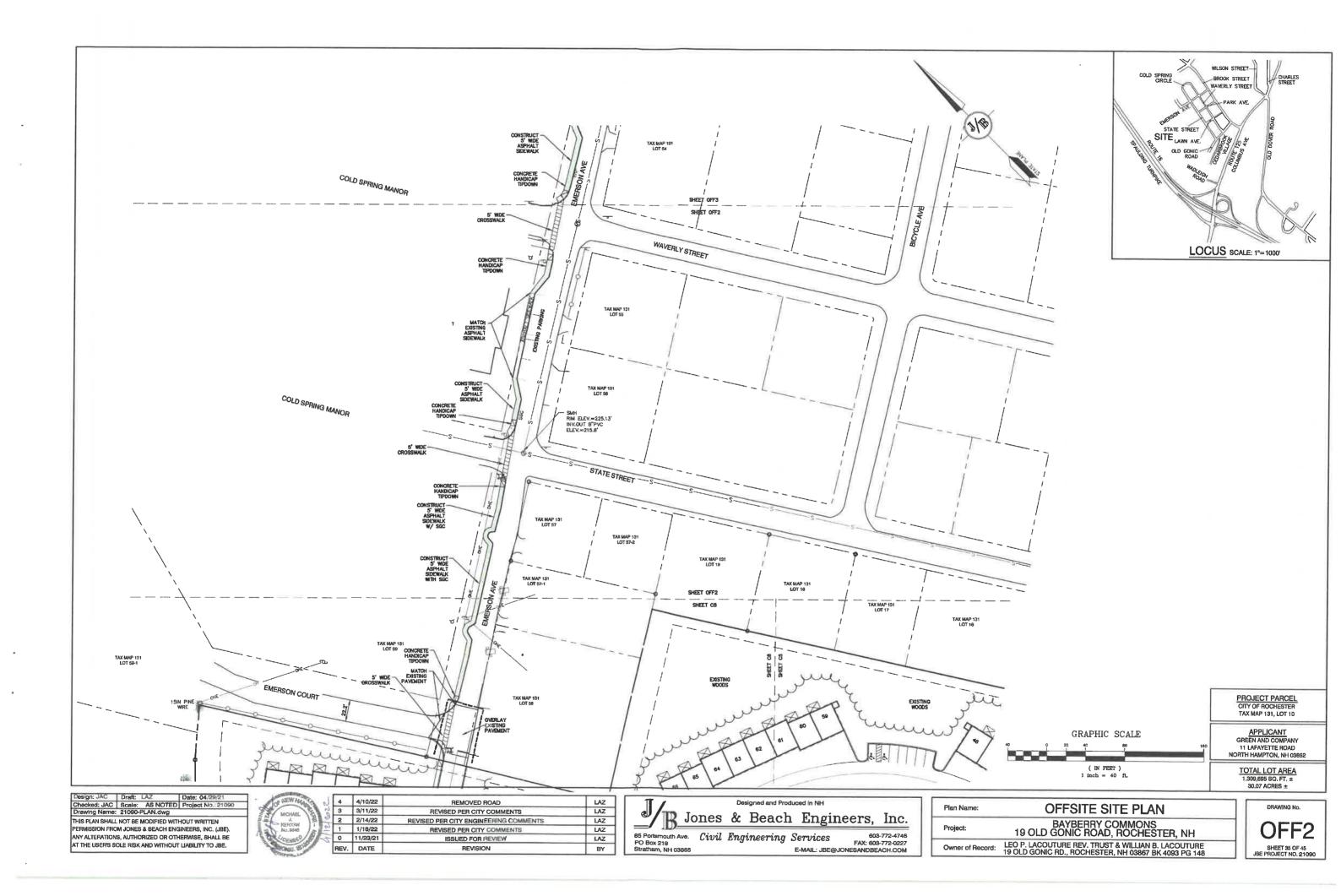
B Jones & Beach Engineers, Inc.

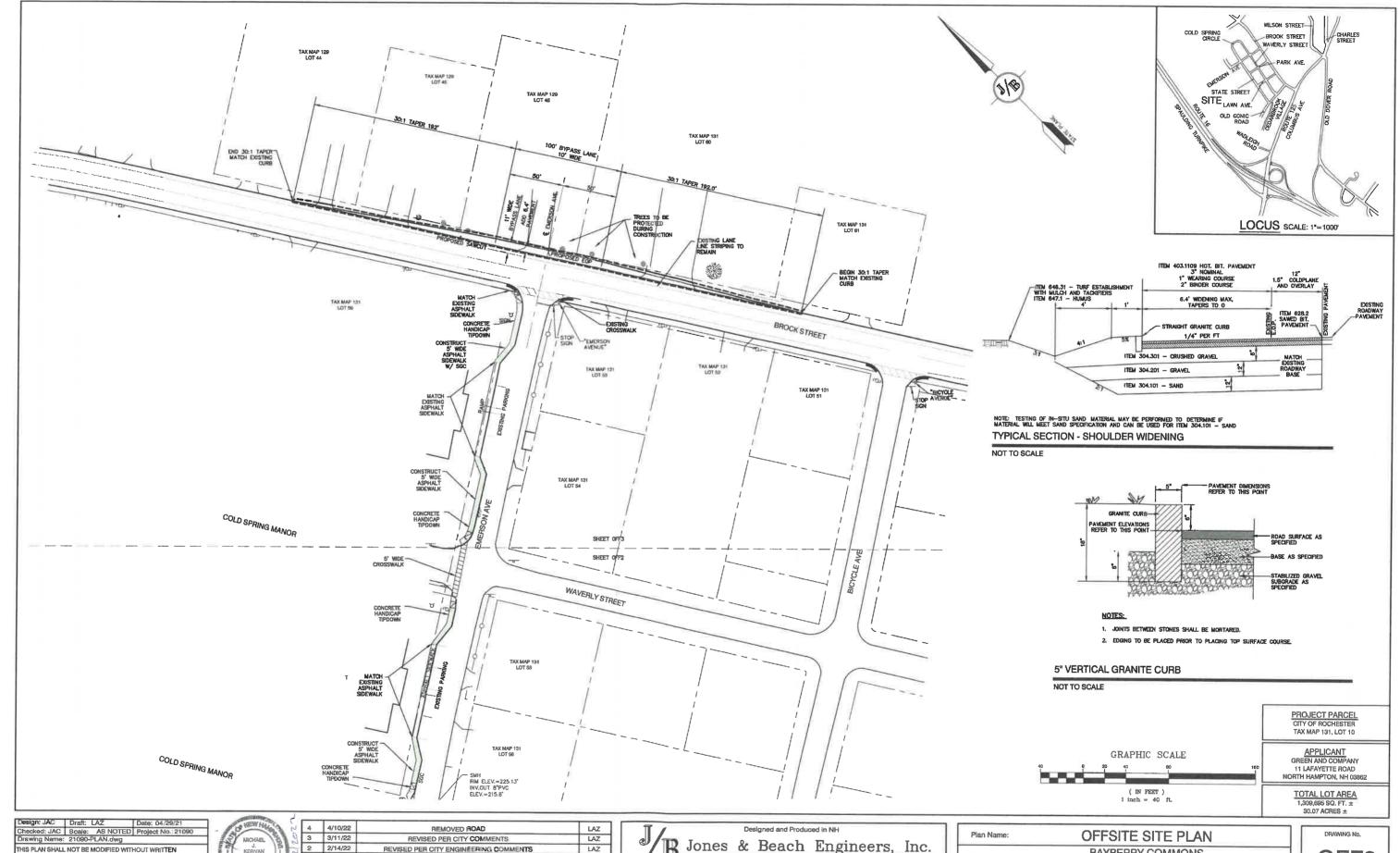
Services 603-772-4746 FAX: 603-772-0227 E-MAIL: JBE@JONESANDBEACH.COM 85 Portsmouth Ave. Civil Engineering Services
PO Box 219
Stratham, NH 03885 E-MAIL: JBE@

BAYBERRY COMMONS 19 OLD GONIC ROAD, ROCHESTER, NH

Owner of Record: LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148



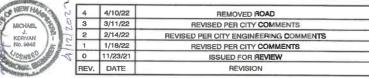




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LAZ

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B Jones & Beach Engineers, Inc.

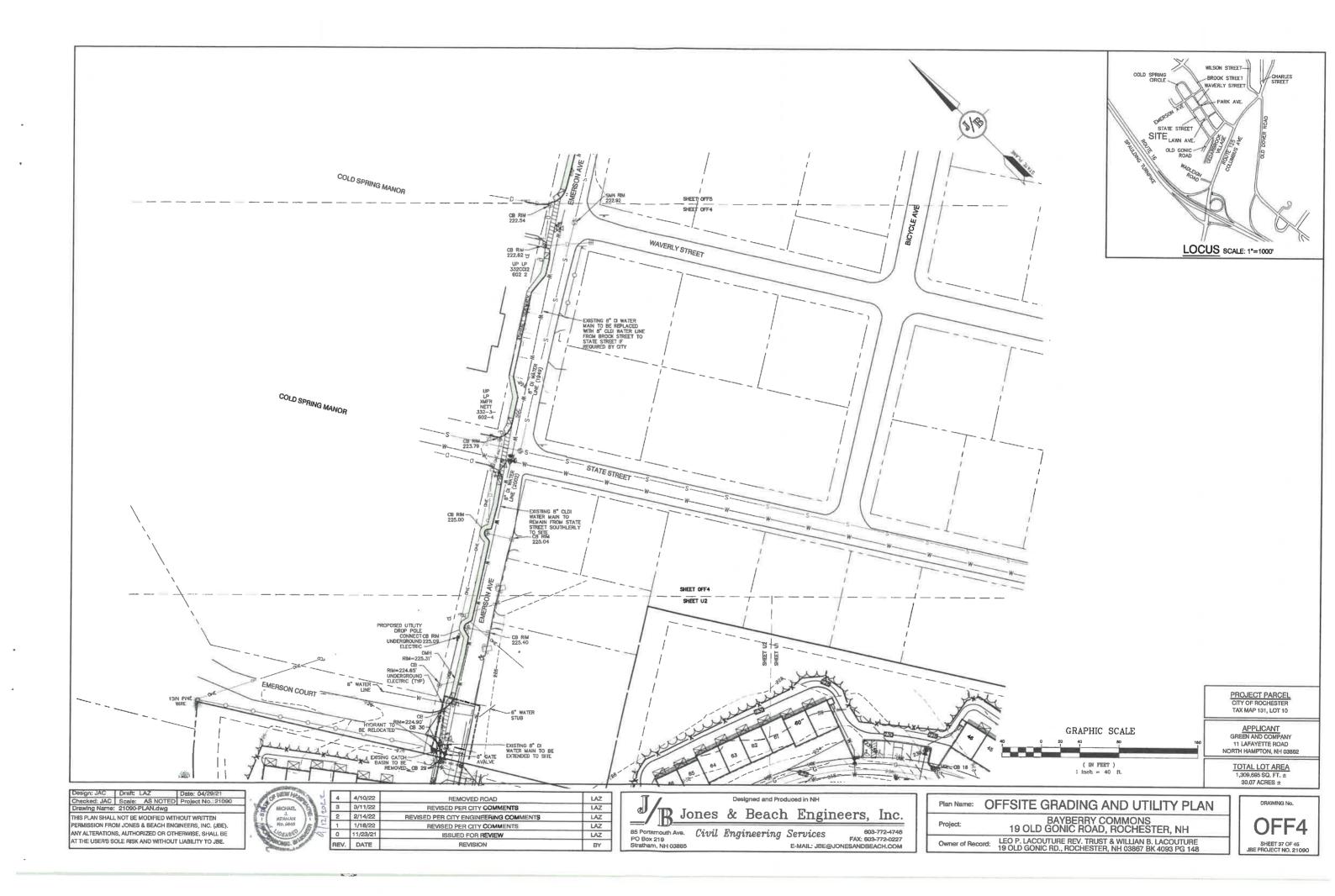
85 Portsmouth Ave. Civil Engineering Services
PO Box 219
Stratham, NH 03885

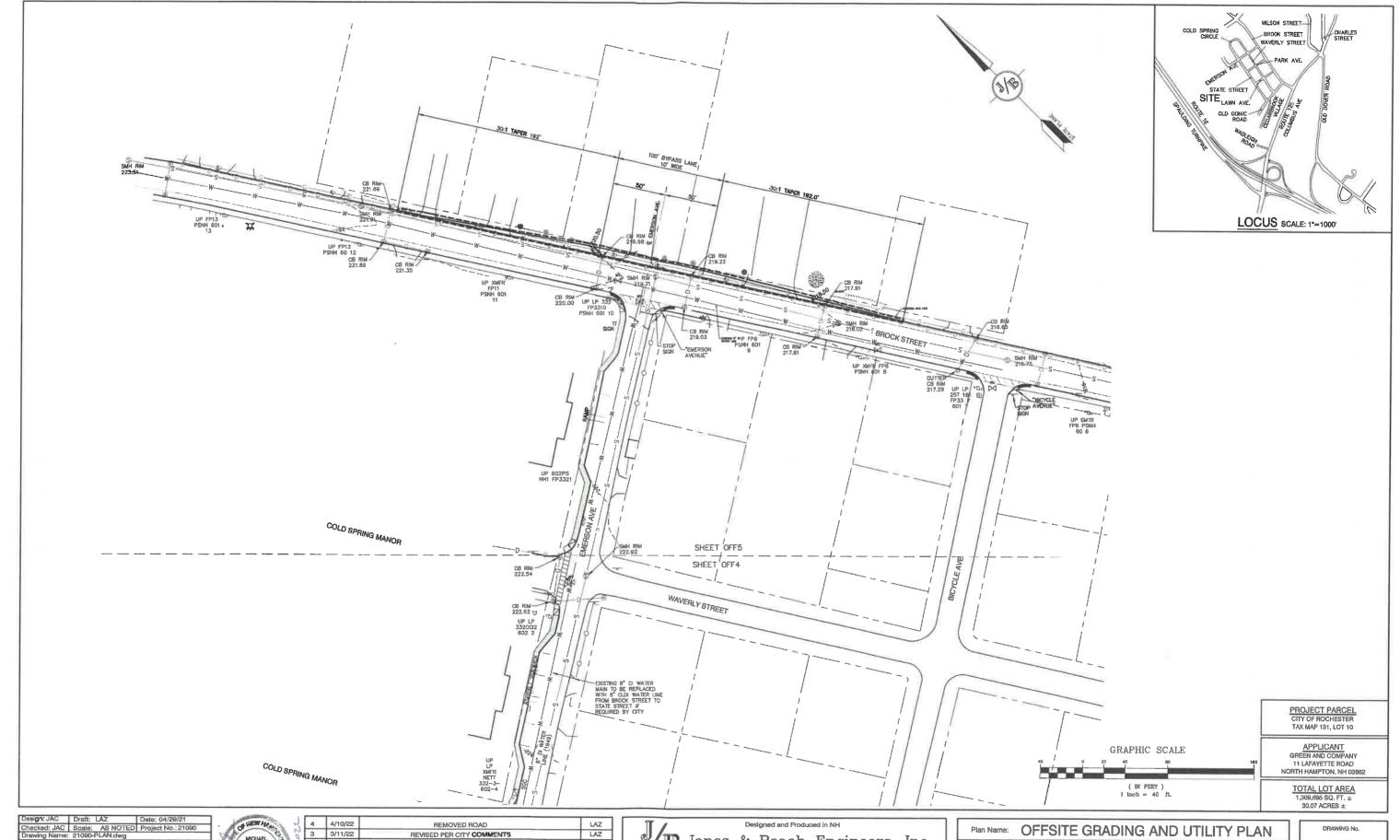
E-MAIL: JBE@ 603-772-4746 FAX: 603-772-0227 E-MAIL: JBE@JONESANDBEACH.COM

| Plan Name: | OFFSITE SITE PLAN                                    |
|------------|--|
| Project:   | BAYBERRY COMMONS<br>19 OLD GONIC ROAD, ROCHESTER, NH |

Owner of Record: LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148







| Design: JAC | Draft: LAZ | Date: 04/29/21 |
| Checked: JAC | Scale: AS NOTED | Project No.: 21090 |
| Drawing Name: 21090-PLAN.dwg |
| THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE).
ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE
AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.

| 4   | 4/10/22  | REMOVED ROAD              | LAZ |
|---|----------|---------------------------|-----|
| 3   | 3/11/22  | REVISED PER CITY COMMENTS | LAZ |
| 2 2/14/22 REVISED PER CITY ENGINEERING COMMENTS |          | LA2                       |     |
| 1   | 1/18/22  | REVISED PER CITY COMMENTS | LAZ |
| 0   | 11/23/21 | ISSUED FOR REVIEW         | LAZ |
| REV.  | DATE     | REVISION                  | BY  |

B Jones & Beach Engineers, Inc.

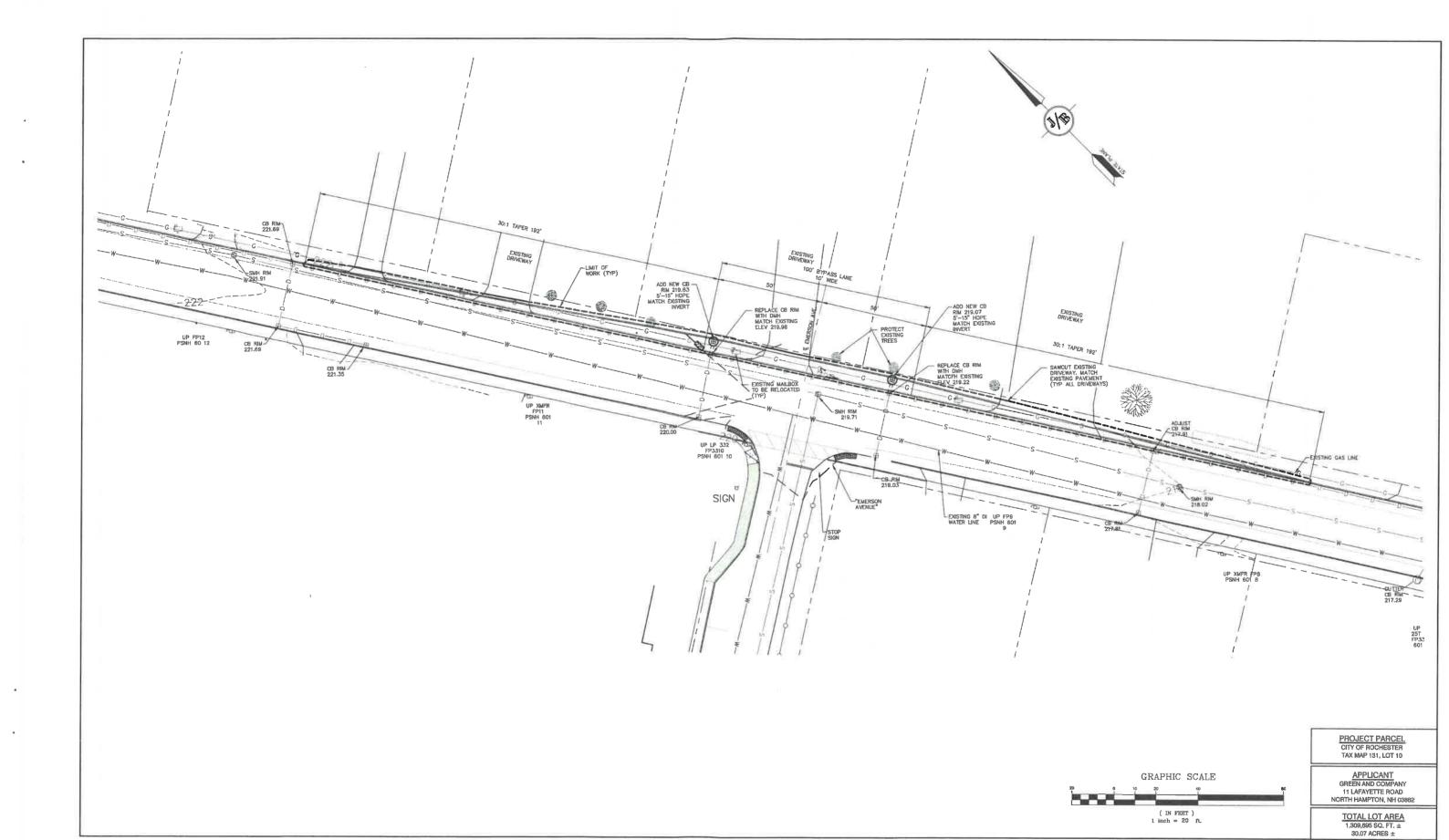
Services 603-772-4746 FAX: 603-772-0227 E-MAIL: JBE@JONESANDBEACH.COM 85 Portsmouth Ave. PO Box 219
Stratham, NH 03885

RE-MAIL: JBE@

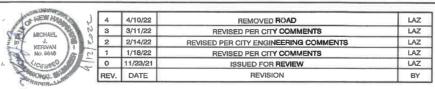
BAYBERRY COMMONS 19 OLD GONIC ROAD, ROCHESTER, NH

Owner of Record: LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4083 PG 148





| Design: JAC       | Draft: LAZ           | Date: 04/29/21     |
|-------------------|----------------------|--------------------|
| Checked: JAC      | Scale: AS NOTED      | Project No.: 21090 |
| Drawing Name:     | 21090-PLAN.dwg       |                    |
|                   | NOT BE MODIFIED WITH |                    |
|                   | S, AUTHORIZED OR OTH |                    |
| AT THE HIGEDIS OF | OF BIEN AND MUTHOLIT | LIADE ITY TO IDE   |



Designed and Produced in NH

Jones & Beach Engineers, Inc.

B5 Portsmouth Ave. Civil Engineering Services 603-772-4748
PO Box 219
Stratham, NH 03865 E-MAIL: JBE@JONESANDBEACH.COM

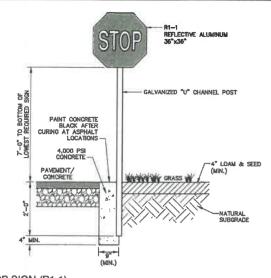
# Plan Name: OFFSITE GRADING AND UTILITY PLAN

Project: BAYBERRY COMMONS
19 OLD GONIC ROAD, ROCHESTER, NH

Owner of Record: LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148

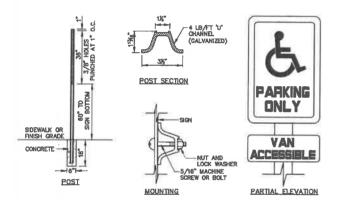
DRAWING No.

OFF6
SHEET 39 OF 45
JBE PROJECT NO. 21090



STOP SIGN (R1-1)

NOT TO SCALE



## HANDICAP SIGN DETAILS

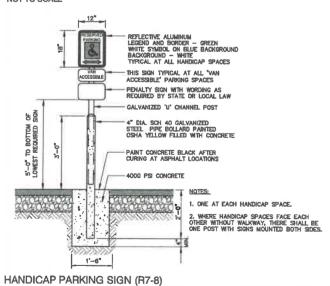
NOT TO SCALE

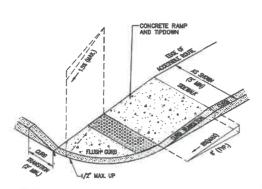
NOT TO SCALE

ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE

AT THE USER'S SOLE RISK AND WITHOUT HARILITY TO JIRE

THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN ERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE)





NOTES:

1. THE MAXBAIN ALLOWABLE CROSS SLOPE OF ACCESSIBLE ROUTE (SIDEWALK) AND CURB SHALL BE 1.5X.

2. THE MAXBAIN ALLOWABLE SLOPE OF ACCESSIBLE ROUTE EXCLUDING CURB RAMPS SHALL BE 5X.

3. THE MAXBAIN ALLOWABLE SLOPE OF ACCESSIBLE ROUTE (SIDEWALK) CURB RAMPS SHALL BE 5X.

4. MINIARIN OF 4 FEET CLARS SHALL BE MAXBAINED AT ANY PERMANENT OBSTACLE IN ACCESSIBLE ROUTED HORANTS, UILITY POLS, TREE WELLS, SIGNS, ETC.).

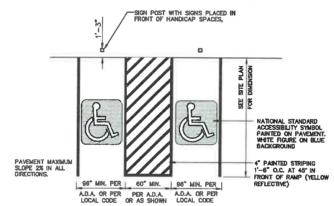
4. MINIARIN CURTY POLS, TREE WELLS, SIGNS, ETC.).

5. BASE OF RAMP SHALL BE GRANDED TO PROPERTY PORGING.

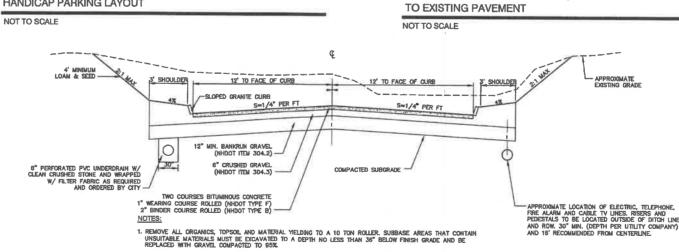
7. SEE TYPICAL SECTION FOR RAMP CONSTRUCTION.

ACCESSIBLE CURB RAMP (TYPE 'B')

NOT TO SCALE



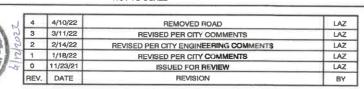
HANDICAP PARKING LAYOUT



- ALL MATERIALS TO BE AS SPECIFIED PER CITY STANDARDS AND NHDDT, WHICHEVER IS MOST STRINGENT. GRADATION AND COMPACTION TEST RESULTS (95% MIN.) SHALL BE SUBMITTED FOR REVIEW AND APPROVAL
- 3. CITY MAY REQUIRE UNDERDRAIN, ADDITIONAL GRAVEL AND/OR ADDITIONAL DRAINAGE IF SOIL CONDITIONS WARRANT
- 4. WOVEN GEOTEXTILE FABRIC SHALL BE PLACED ABOVE SUBGRADE AT ALL WETLAND CROSSINGS,

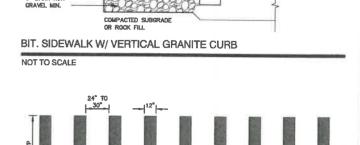
TYPICAL ROADWAY SECTION W/CURBING

NOT TO SCALE



# Designed and Produced in NH Jones & Beach Engineers, Inc.

85 Portsmouth Ave. Civil Engineering Services
PO Box 219
Stratham, NH 03885
E-MAIL: JBE@ E-MAIL: JBE@JONESANDBEACH.COM



WIDTH VARIES SEE SITE PLANS

VERTICAL GRANITE CLIRA

1" WEARING COURSE -

1 5" BASE COURSE

000000000 000000000 00000000 000000000 000000000 000000000

DETECTABLE WARRINGS SHALL CONSIST OF A SURFACE OF TRUNCATED DOMES AND SHALL COMPLY WITH THE FOLLOWING:

A. TRUNCATED DOMES SHALL HAVE A BASE DIAMETER OF 0.9" (MIN.) AND 1.4" (MIX.). A TOP DIAMETER OF 50% OF THE BASE DIAMETER MINIMUM TO 65% OF THE BASE DIAMETER MINIMUM TO 65% OF TRUNCATED DOMES SHALL HAVE A CHIEFA-TO-CHERT SPACING OF 1.6" MINIMUM AND 2.4" MADIBUM, AND A BASE-TO-BASE SPACING OF .65" MINIMUM AND 1.2" MADIBUM, AND A BASE-TO-BASE SPACING OF .65" MINIMUM AND 1.5" MADIBUM, AND A BASE-TO-BASE SPACING DOMES ON A SUMPLE OF DAMES TO BE CAST FROM PER NHOOT SPECIFICATIONS.

C. SOUNCE OFFI DAMES TO BE CAST FROM PER NHOOT SPECIFICATIONS.

D. DETECTABLE WARRING SURFACES SHALL CONTRAST WISUALLY WITH ADJACENT WALKING SURFACES ETHER LIGHT-ON-DARK OR DARK-ON-LUGHT.

Truncated domes to be placed in Sidewalk base in Public Traffic Areas. ACCESSIBLE CURB RAMP TRUNCATED DOMES

"1" HOT BIT. PAVEMENT WEARING COURSE

95% COMPACTED SUBGRADE OR ROCK FILL

KEYWAY

KEYWAY DETAIL FOR CONNECTION

TYPICAL BITUMINOUS PAVEMENT

NOT TO SCALE

BIRER COURSE

BASE COURSE -

-6" NHDOT ITEM 304.3 CRUSHED GRAVEL 95% MIN. COMPACTION INCLUDING RECLAIMED MATERIAL

- NHDOT (TEM 304.2 BANK

TOP COURSE

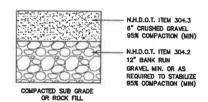
-6" CRUSHED GRAVE

-12° MIN CRAVE

- TRANSVERSE CROSSWALK LINES SHALL BE THERMOPLASTIC, NOT LESS THAN 6" WIDE AND NOT LESS THAN 6" APART.
- . SPACING FOR THE CONTINENTAL CLOCK MARKINGS SHALL BE LINIFORM FOR EACH INDIVIDUAL CROSSWALK BUT CAN BE MODIFIED FOR ONE CROSSWALK TO THE NEXT TO EDIMINATE A CROSSWALK MARKING DIRECTLY IN THE WHEELPATH,

#### NHDOT CONTINENTAL BLOCK MARKING DETAIL

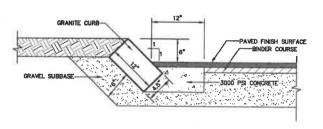
NOT TO SCALE



NOTE: IN AREAS OF ROCK EXCAVATION, MINIMUM 9" BANK RUN GRAVEL SHALL BE PLACED

#### GRAVEL SECTION

NOT TO SCALE



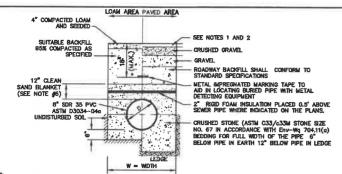
CURB TO BE PLACED PRIOR TO PLACING TOP SURFACE COURSE.
 JOINTS BETWEEN STONES SHALL BE MORTARED.

## SLOPED GRANITE CURB

NOT TO SCALE

| Plan Name:       | DETAIL SHEET   | ] [ | DRAWI               |
|------------------|--|-----|---------------------|
| Project:         | BAYBERRY COMMONS<br>19 OLD GONIC ROAD, ROCHESTER, NH   | 1   |                     |
| Owner of Record: | LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE<br>19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148 | 11  | SHEET<br>JBE PROJEC |

AING No SHEET 40 OF 45 JBE PROJECT NO. 21090

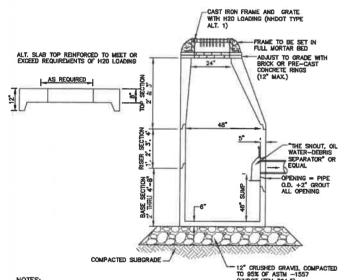


NOTES:
1. PAVEMENT REPAIR IN EXISTING ROADWAYS SHALL CONFORM TO PAVEMENT DETAILS.

- 2. NEW ROADWAY CONSTRUCTION SHALL CONFORM TO SUBDIVISION SPECIFICATIONS.
- TRENCH BACKFILL SHALL CONFORM WITH ENV. Wq 704.11(n) AND BE FREE OF DEBRIS, PAVEMENT, ORGANIC MATTER, TOP SOIL, WET OR SOFT MUCK, PEAT OR CLAY, EXCAVATED LEDGE OR ROCKS OVER SIX INCHES.
- 4. We MAXIMUM ALLOWABLE TRENCH WIDTH TO A PLANE 12" INCHES ABOVE THE PIPE. FOR PIPES 15 INCHES NOMINAL DIAMETER OR LESS, WIDTH SHALL BE NO MORE THAN 36"; FOR PIPES GREATER THAN 15 INCHES NOMINAL DIAMETER, WIDTH SHALL BE 24 INCHES PLUS PIPE D.D. WIDTH SHALL ALSO BE THE PAYMENT WIDTH FOR LEDGE EXCAVATION AND FOR ORDERDE EXCAVATION BELOW GRADE.
- 5. RIGID FOAM INSULATION TO BE PROVIDED WHERE COVER IN THE ROADWAY IS LESS THAN 6' AND CROSS COUNTRY IS LESS THAN 4', PURSUANT TO DES WAIVER BEING ISSUED.
- PIPE SAND BLANKET MATERIAL SHALL BE GRADED SAND, FREE FROM ORGANIC MATERIALS, GRADED SUCH THAT 100% PASSES A 1/2 " SIEVE AND A MAXIMUM OF 15% PASSES A #200 SIEVE IN ACCORDANCE WITH Env-Wq 704.11(b).
- JOINT SEALS FOR PVC PIPE SHALL BE OIL RESISTANT COMPRESSION RINGS OF ELASTOMERIC MATERIAL AND CERTIFIED BY THE MANUFACTURER AS CONFORMING TO THE ASTM 03212 STANDARD IN EFFECT WHEN THE JOINT SEALS WERE MANUFACTURED, AND SHALL BE PUSH-ON, BELL-AND-SPIGOT TYPE PER ENV-WIG 704.05 (e).

#### SEWER TRENCH

NOT TO SCALE

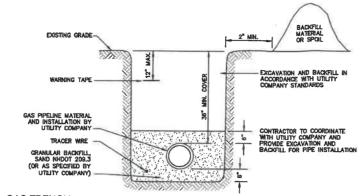


- NOTES:

  1. BASE SECTION SHALL BE MONOLITHIC WITH 48" INSIDE DIAMETER.
- 2. ALL SECTIONS SHALL BE DESIGNED FOR H20 LOADING
- 3. CONCRETE SHALL BE COMPRESSIVE STRENGTH 4000 PSI, TYPE II CEMENT.
- 4. FRAMES AND GRATES SHALL BE HEAVY DUTY AND DESIGNED FOR H20 LOADING
- PROVIDE "V" KNOCKOUTS FOR PIPES WITH 2" MAX. CLEARANCE TO OUTSIDE OF PIPE. MORTAR ALL PIPE CONNECTIONS SO AS TO BE WATERTIGHT.
- 6. JOINT SEALANT BETWEEN PRECAST SECTIONS SHALL BE BUTYL RUBBER.
- ALL CATCH BASIN FRAMES AND GRATES SHALL BE NHDOT CATCH BASIN TYPE ALTERNATE 1 OR NEENAH R-3570 OR APPROVED EQUAL (24"x24" TYPICAL).
- STANDARD CATCH BASIN FRAME AND GRATE(S) SHALL BE SET IN FULL MORTAR BED. ADJUST TO GRADE WITH CLAY BRICK AND MORTAR (2 BRICK COURSES TYPICALLY, 5 BRICK COURSES MAXIMUM, BUT NO MORE THAN 12"), OR PRECAST CONCERTE "DONUTS".
- 9. ALL CATCH BASINS ARE TO BE FITTED WITH GREASE HOODS.

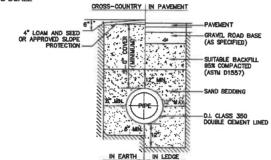
## CATCH BASIN WITH GREASE HOOD

NOT TO SCALE

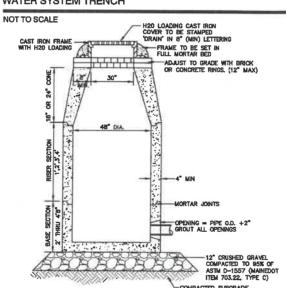


#### **GAS TRENCH**

NOT TO SCALE



#### WATER SYSTEM TRENCH

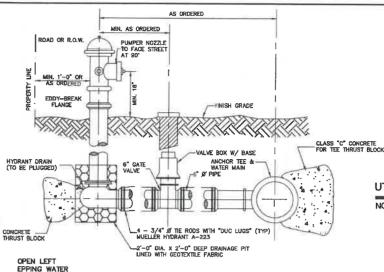


#### NOTES:

- 1. BASE SECTION SHALL BE MONOUTHIC WITH 48" INSIDE DIAMETER
- 2. ALL SECTIONS SHALL BE DESIGNED FOR H20 LOADING.
- 3. CONCRETE SHALL BE COMPRESSIVE STRENGTH 4000 PSI, TYPE II CEMENT.
- 4. FRAMES AND GRATES SHALL BE HEAVY DUTY AND DESIGNED FOR H20 LOADING
- PROVIDE "V" KNOCKOUTS FOR PIPES WITH 2" MAX. CLEARANCE TO OUTSIDE OF PIPE. MORTAR ALL PIPE CONNECTIONS SO AS TO BE WATERTIGHT.
- 8. JOINT SEALANT BETWEEN PRECAST SECTIONS SHALL BE BUTYL RUBBER,
- ALL DRAIN MANHOLE FRAMES AND GRATES SHALL BE NEENAH R-1798 OR APPROVED EQUAL (30" DIA. TYPICAL).
- STANDARD FRAME(S) AND GRATE(S) SHALL BE SET IN FULL MORTAR BED. ADJUST TO GRADE WITH CLAY BRICK AND MORTAR (2 BRICK COURSES TYPICALLY, 5 BRICK COURSES MAXIMUM, BUT NO MORE THAN 12"), OR PRECAST CONCRETE "DOWNITS".

#### DRAIN MANHOLE (4' DIAM.)

NOT TO SCALE



EPPING WATER DEPARTMENT SPECS.

- NOTES

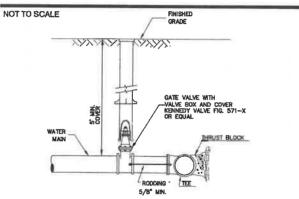
  1. ALL PIPE FITTINGS TO BE D.L. PRESSURE CLASS 350, THICKNESS CLASS 52.

  2. HYDRANT TO BE PAINTED RED WITH WHITE "REPLECTOR" PAINT ON BONNET.

  3. MECHANICAL JOINTS SHALL HAVE MEGALUG RETAINING GLANDS AS MADE BY EBBA OR APPROVED EQUAL.

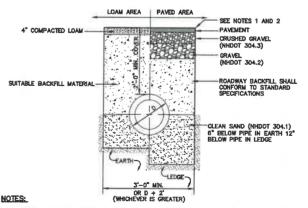
  3. TOTAL STANDARY TYPE.
- 4. STEAMER NOZZLE TO BE "STORCH" TYPE.
  5. NATIONAL STANDARD THREAD.

#### HYDRANT INSTALLATION



#### **BURIED GATE VALVE DETAIL**

NOT TO SCALE



1. PAVEMENT REPAIR IN EXISTING ROADWAYS SHALL CONFORM TO STREET OPENING RECULATIONS

E-MAIL: JBE@JONESANDBEACH.COM

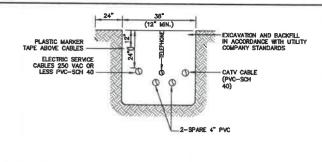
2. NEW ROADWAY CONSTRUCTION SHALL CONFORM WITH PROJECT AND CITY SPECIFICATIONS.

3. ALL MATERIALS ARE TO BE COMPACTED TO 95% OF ASTM D-1557.

DRAINAGE TRENCH

NOT TO SCALE

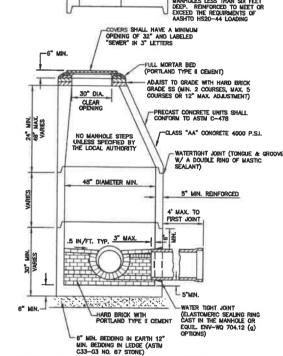
Strathern, NH 03885



NOTE: ALL UTILITIES SHALL BE REVIEWED AND APPROVED BY APPROPRIATE LITHITY COMPANY

#### UTILITY TRENCH

NOT TO SCALE



- PER NIDES ENV-WO 704.13(C), MORTAR USED IN MANHOLE CONSTRUCTION SHALL COMPLY WITH THE FOLLOWING:

  a. MORTAR SHALL BE COMPOSED OF TYPE II PORTLAND CEMENT AND SAND WITH OR WITHOUT HYBRATED LIME ADDITION

  b. PREPORTIONS IN MORTAR PARTS BY VOLUMES SHALL BE PER TABLE 704-4;

  (2.4.5 PARTS SAND, ONE PART COMPLY; OR

  (2.4.5 PARTS SAND, ONE PART COMPLY; OR

  (2.4.5 PARTS SAND, ONE PART COMPLY; OR

  (2.4.5 PARTS SAND, ONE PART COMPLY THAT IS CORTIFED BY ITS MANUFACTURER AS CONFORMING TO THE ASTM CISO/CISOM STANDARD IN EFFECT AT THE TIME THE THE THE CEMENT WAS MANUFACTURED LIME SHALL BE TYPE S THAT IS CORTIFED BY ITS MANUFACTURER AS CONFORMING TO THE ASTM CISO/CISOM STANDARD IN EFFECT AT THE TIME THE KYDRATED LIME WAS PROCESSED ON SAND SHALL CONSIST OF NERTH NATURAL SAND THAT IS CORTIFIED BY ITS UPPLIER AS CONFORMING TO THE ASTM CISO/CISOM STANDARD IN EFFECT AT THE TIME THE KYDRATED LIME WAS PROCESSED BY STANDARD TO THE ASTM CISO STANDARD IN EFFECT AT THE TIME THE SAND IS PROCESSED BY STANDARD SPECIFICATIONS FOR CONCRETE, FIRE AGGREGATES

  CONCRETE FOR DROP SUPPORTS SHALL CONFORM TO THE REQUIREMENT FOR CLASS AAA CONCRETE FOR BOWN AND BRIDGE CONSTRUCTION S AVAILABLE AT:

HTTP://WWW.NH.GOV/DOT/ORG/PROJECTDEVELOPMENT/HIGHWAYDESIGN/SPECIFICATIONS/INDEX.HTM

- SHELVES SHALL BE CONSTRUCTED TO THE ELEVATION OF THE HIGHEST PIPE CROWN AND SLOPED TO DRAIN TOWARD THE FLOWING THROUGH CHANNEL IN ACCORDANCE WITH ENV-WO 704.12 (K).
- 3. ALL MANHOLES SHALL BE TESTED FOR LEAKAGE IN ACCORDANCE WITH ENV-WQ 704.17 (o) THROUGH
- 4. SEWER MANHOLE COVERS SHALL CONFORM TO ASTM A48/48M WITH A CASTING EQUAL TO CLASS 30 IN ACCORDANCE WITH ENV-WQ 704.13 (a) (a). ALL PRECAST SECTIONS SHALL BE COATED ON THE EXTERIOR WITH A BITUMINOUS DAMP-PROOFING COATING IN ACCORDANCE WITH ENV-WQ 704.12 (d).
- 6. ALL PRECAST SECTIONS AND BASES SHALL HAVE THE DATE OF MANUFACTURE AND THE MAME OR TRADEMARK OF THE MANUFACTURER IMPRESSED OR INDELIBLY MARKED ON THE INSIDE WALL PER
- 7. BRICK MASONRY SHALL CONFORM TO ASTM C32 (ENV-WQ 704.12(a)(9))

#### SEWER MANHOLE

NOT TO SCALE

THIS PLAN SHALL NOT BE MODIFIED WITHOUT WHITTEN ION FROM JONES & BEACH ENGINEERS, INC. (JBE). ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.

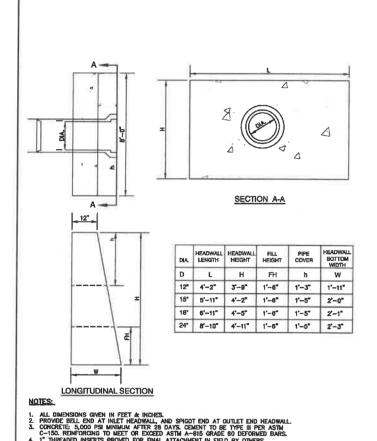


| REV. | DATE     | REVISION                              | BY |
|------|----------|---------------------------------------|----|
| 0    | 11/23/21 | ISSUED FOR REVIEW                     | LA |
| 1    | 1/18/22  | REVISED PER CITY COMMENTS             | LA |
| 2    | 2/14/22  | REVISED PER CITY ENGINEERING COMMENTS | LA |
| 3    | 3/11/22  | REVISED PER CITY COMMENTS             | LA |
| 4    | 4/10/22  | REMOVED ROAD                          | LA |

Designed and Produced in NH B Jones & Beach Engineers, Inc. 85 Portsmouth Ave. Civil Engineering Services FAX: 603-772-0227 PO Box 219

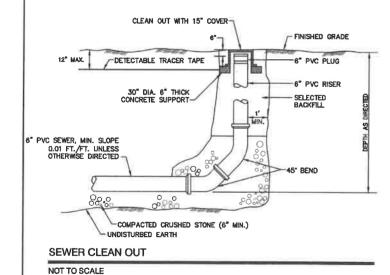
|  | Plan Name:      | DETAIL SHEET  |  |  |  |  |
|--|-----------------|---|--|--|--|--|
|  | Project:        | BAYBERRY COMMONS<br>19 OLD GONIC ROAD, ROCHESTER, NH  |  |  |  |  |
|  | Owner of Record | LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148 |  |  |  |  |

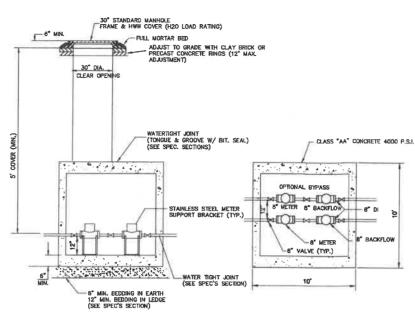
DRAWING No **D2** SHEET 41 OF 45 PROJECT NO. 21090



# PRECAST CONCRETE HEADWALL

## NOT TO SCALE





## **ELEVATION**

#### PLAN VIEW

- NOTES

  1. METER TO BE SENSUS OMNI C2 OF APPROPRIATE SIZE.

  2. BACKPLOW TO BE TESTABLE DOUBLE CHECK VALVE ASSEMBLY WITH CENTER-SHAFT OR TOP HINGE CHECKS (MULCHS TO THE PROPRIATE SIZE, IF APPLICATION IS DESIGNED LOW HAZARD.

  3. OPTIONAL BYFASS MY SE SIZED FOR DOMESTIC SERVICE ONLY.

  4. VAULT TO HAVE ADEQUATE ANTI-BOUYDANCY PEATURES.

  5. VAULT COVERS TO BE STAMPED WITH "WATER" AND MATCH EXISTING CITY OF ROCHESTER INFRASTRUCTURE STANDARDS.

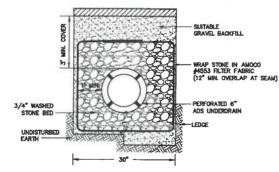
  6. ISCALTION VALVES REQUIRED AROUND EQUIPMENT FOR MAINTENCE, TESTING AND SERVICE.

  7. F APPLICATION VS. DESIGNATED HIGH HAZARD, THE ASSEMBLY MUST USE RYZ BACKFLOW DEWICES AND BE LOCATED IN AN ABOVE GRADE, HEATED AND INSULATED ENCLOSURE TO ALLOW FOR DRAINING.

BYPASS USAGE: 9. F OPTIONAL BYPASS LINE IS INSTALLED, WHEN MAIN FEED IS TAKEN OFLINE AND BYPASS ENGAGED, OWNER SHALL CALL 330-7128 TO COORDINATE LOW FLOW CONDITION WITH ROCHESTER FIRE DEPARTMENT AND ROCHESTER PUBLIC W

#### WATER METER PIT ROCHESTER

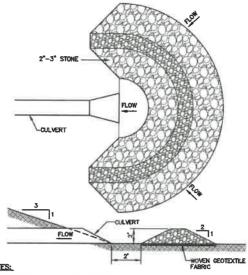
#### NOT TO SCALE



- 1. PAVEMENT REPAIR IN EXISTING ROADWAYS SHALL CONFORM TO STREET OPENING REGULATIONS
- 2. NEW ROADWAY CONSTRUCTION SHALL CONFORM TO PROJECT AND CITY SPECIFICATIONS

# ROADWAY UNDERDRAIN TRENCH

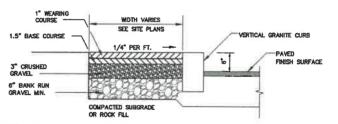
NOT TO SCALE



- TEMPORARY CULVERT INLET PROTECTION CHECK DAMS SHALL BE CONSTRUCTED OF 2-3" STONE OVER WOVEN GEOTEXTILE FABRIC.
- SEDIMENT SHALL BE REMOVED FROM BEHIND THE STRUCTURE WHEN IT HAS ACCUMULATED TO ONE HALF THE ORIGINAL HEIGHT OF THE STRUCTURE.
- STRUCTURES SHALL BE REMOVED WHEN THE SITE IS STABILIZED WITH VEGETATION AND THE CHANNEL SHALL BE SMOOTHED AND REVEGETATED.

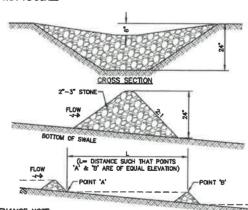
## TEMPORARY CULVERT INLET PROTECTION CHECK DAM

#### NOT TO SCALE



#### BIT. SIDEWALK W/ VERTICAL GRANITE CURB

## NOT TO SCALE

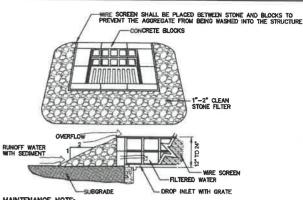


#### MAINTENANCE NOTE:

1. STONE CHECK DAMS SHOULD BE CHECKED AFTER EACH RAINFALL AND AT LEAST DAILY DURING PROLONGED RAINFALL. ANY NECESSARY REPAIRS SHOULD BE MADE IMMEDIATELY. PARTICULAR ATTENTION SHOULD BE GYEN TO EXD RUN AND EROSION AT THE DOWNSTREAM TOE OF THE STRUCTURE WHEN THE STRUCTURES ARE REMOVED, THE DISTURBED PORTION SHOULD BE BROUGHT TO THE DASTING CHANNEL GRADE AND HELP AREAS PREPARED, SEEDED AND MILLOHED. WHILE THIS PRACTICE IS NOT INTENDED TO BE USED PRIMARILY FOR SEDIMENT WAS ESTIMANT WILL ACCUMULATE BEHIND THE STRUCTURES. SOMEON THE SOMEON THE STRUCTURES WHEN IT HAS ACCUMULATED TO ONE HALF OF THE CRIGNAL HEIGHT OF THE STRUCTURE.

#### STONE CHECK DAM

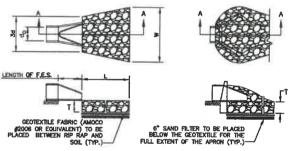
NOT TO SCALE



#### MAINTENANCE NOTE:

#### TEMPORARY CATCH BASIN INLET PROTECTION (Block and Gravel Drop Inlet Sediment Filter)

NOT TO SCALE



SECTION A-A PIPE OUTLET TO FLAT AREA
WITH NO DEFINED CHANNEL SECTION A-A PIPE OUTLET TO

| TABLE 7-24                     | RECOMMENDED  | RIP RAP GR | ADAT | ION RANGES        |
|--------------------------------|--------------|------------|------|-------------------|
| THICKNESS OF                   | RIP RAP = 1. | 5 FEET     |      |                   |
| d50 StZE=                      | 0.50         | FEET       | 6    | INCHES            |
| % OF WEIGHT S<br>THAN THE GIVE |              | SIZE OF    | STO  | NE (INCHES)<br>TO |
| 100%                           |              | 9          |      | 12                |
| 85%                            |              | 8          |      | 11                |
| 50%                            |              | 6          |      | 9                 |
| 15%                            |              | 2          |      | 3                 |

- . The subgrade for the geotextile fabric and RIP RAP shall be prepared to the lines and grades shown on the plans.
- 2. THE RIP RAP SHALL CONFORM TO THE SPECIFIED GRADATION
- 4. STONE FOR THE RIP RAP MAY BE PLACED BY EQUIPMENT AND SHALL BE CONSTRUCTED TO THE FULL LAYER THICKNESS. IN ONE OPERATION AND IN SUCH A MANNER AS TO PREVENT SEGREGATION OF THE STONE SIZE.
- 6. MAINTENANCE: THE OUTLET PROTECTION SHOULD BE CHECKED AT LEAST ANNUALLY AND AFTER EVERY MAJOR STORM. IF THE RIP RAP HAS BEEN DISPLACED, UNDERMINED OR DAMAGED, IT SHOULD BE REPAIRED IMMEDIATELY. THE CHANNEL IMMEDIATELY BELOW THE OUTLET SHOULD BE CHECKED TO SEE THAT EROSION IS NOT OCCURRING. THE DOWNSTREAM CHANNEL SHOULD BE KEPT OLEAR OF CESTRUCTIONS SUCH AS FALLEN TREES, DEBINS, AND SEDIMENT THAT COULD CHANGE FLOW PATTERNS AND/OR TAILWATER DEPTHS ON THE PIPES, REPAIRS MUST BE CARRIED OUT IMMEDIATELY TO AVOID ADDITIONAL DAMAGE TO OUTLET PROTECTION.

#### RIP RAP OUTLET PROTECTION APRON

NOT TO SCALE

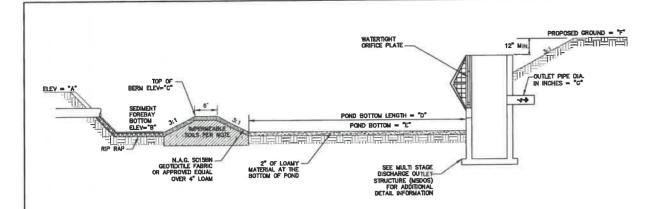
| 1/                               |       | De  | signed and Pro | duced in NH  |            |                          |
|----------------------------------|-------|-----|----------------|--------------|------------|--------------------------|
| B Jo                             | nes   | &   | Beach          | ı Engii      | neers,     | Inc.                     |
| 85 Portsmouth Ave.<br>PO Box 219 | Civil | Eng | ineering       | Services     |            | 3-772-4748<br>3-772-0227 |
| Stratham, NH 03885               |       |     |                | E-MAIL: JBE@ | JONESANDBE | ACH.COM                  |

| Plan Name:       | DETAIL SHEET   |
|------------------|--|
| Project:         | BAYBERRY COMMONS<br>19 OLD GONIC ROAD, ROCHESTER, NH   |
| Owner of Record: | LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE<br>19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148 |

| Design: JAC       | Draft: LAZ                                  | Date: 04/29/21       |
|-------------------|---|----------------------|
| Checked: JAC      | Scale: AS NOTED                             | Project No.: 21090   |
| Drawing Name:     | 21090-PLAN.dwg                              |                      |
| PERMISSION FRO    | NOT BE MODIFIED WITH<br>M JONES & BEACH ENG | BINEERS, INC. (JBE). |
| ANY ALTERATION    | S, AUTHORIZED OR OTH                        | HERWISE, SHALL BE    |
| AT THE LISER'S SO | OLE BISK AND WITHOUT                        | LIABILITY TO JRE     |



| 4    | 4/10/22  | REMOVED ROAD                          | LAZ |
|------|----------|---------------------------------------|-----|
| 3    | 3/11/22  | REVISED PER CITY COMMENTS             | LAZ |
| 2    | 2/14/22  | REVISED PER CITY ENGINEERING COMMENTS | LAZ |
| 1    | 1/18/22  | REVISED PER CITY COMMENTS             | LAZ |
| 0    | 11/23/21 | ISSUED FOR REVIEW                     | LAZ |
| REV. | DATE     | REVISION                              | BY  |



#### POND TABLE

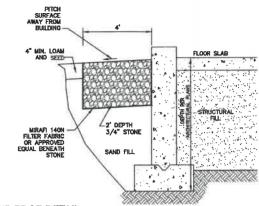
| POND   |        |        | ELEVA" | TIONS/DIME | ENSIONS |        |     |
|--------|--------|--------|--------|------------|---------|--------|-----|
|        | A      | В      | С      | D          | E       | F      | G   |
| POND 1 | 220.00 | 216.00 | 218.00 | 169'       | 212.00  | 220.00 | 12" |
| POND 2 | 220.00 | 217.00 | 219.00 | 310        | 212.00  | 220.00 | 12° |
| POND 3 | 225.00 | 220.00 | 222.00 | 200'       | 216.00  | 225.50 | 12° |

#### WET POND SECTION (PONDS 1, 2 & 3)

NOT TO SCALE

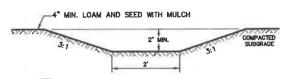
## WET POND CONSTRUCTION CRITERIA

- PROTECTION --- A-PROTECTIVE COVER OF VEGETATION SHALL BE ESTABLISHED ON ALL EXPOSED SUFFACES OF THE EMBANGMENT, SPILLWAY, AND BORROW AREA IF SOIL AND CLIMATIC CONDITIONS PERMIT. IF SOIL OR CLIMATIC CONDITIONS PRECLUDE THE USE OF VEGETATION AND PROTECTION IS NEEDED, NON-VEGETATIVE MEANS SUCH AS MULCHES OR GRAVEL MAY BE USED. IN SOME PLACES, TEMPORARY VEGETATION MAY BE USED UNTIL CONDITIONS PERMIT ESTABLISHMENT OF PERMANENT VEGETATION. THE EMBANGMENT AND SPILLWAY SHALL BE PENCED IF NECESSARY TO PROTECT THE VEGETATION.
- SECTION DOFFBARATION SEFTING FERTILIZING AND MILLCHING SHALL COMPLY WITH THE APPROPRIATE VEGETATIVE 8MP'S.
- CONCRETE THE MIX DESIGN AND TESTING OF CONCRETE SHALL BE CONSISTENT WITH THE STRENGTH REQUIREMENTS OF THE JOB. MIX REQUIREMENTS OR RECESSARY STRENGTH SHALL BE SPECIFED. THE TYPE OF CRUENT, AIR ENTRAPHENT, SLUIP, AGGREGATE, OR OTHER PROPERTIES SHALL BE SPECIFED IN THE CONCRETE IS TO CONSIST OF A WORKABLE MIX THAT CAN BE PLACED AND FINISHED IN AN ACCEPTABLE MANNER. NECESSARY CURING SHALL BE SPECIFED, REINFORCING STEEL SHALL BE PLACED AS INDICATED ON THE PLANS AND SHALL BE HOLD SEQURELY IN PLACE DURING CONCRETE PLACEMENT. SUB-GRADES AND FORMS SHALL BE INSTALLED TO LINE AND GRADE, AND THE FORMS SHALL BE MOSTART TIGHT AND UNYBLINING AS THE CONCRETE IS PLACED.
- THE CONTRACTOR WILL NOTIFY JONES AND BEACH ENGINEERS AFTER EACH OF THE GRAVEL WETLAND PONDS HAVE BEEN EXCAVATED TO THE BOTTOM OF THE SYSTEM FOR A MANDATORY INSPECTION PRIOR TO BUILDING BERMS, PLACING STONE OR INSTALLING PIPE SYSTEM.
- BERMS AND WEIRS SEPARATING THE FOREBAY AND TREATMENT CELLS SHOULD BE CONSTRUCTED WITH CLAY, OR NON-CONDUCTIVE SOILS, AND/OR A FINE GEOTEXTILE, OR SOINE COMBINATION THEREOF, TO AVOID WATER SEEPAGE AND SOIL PIPING THROUGH THESE EARTHEN DIVIDERS.



DRIP EDGE DETAIL

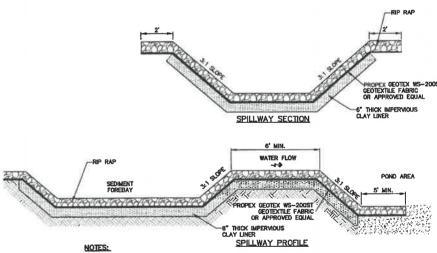
NOT TO SCALE



1. ALL VEGETATED SWALES ARE TO BE STABILIZED WITH NORTH AMERICAN GREEN EROSION CONTROL BLANKET SECURED WITH BIODEGRADABLE 'BIO' OR 'ECO-STAKES'.

#### VEGETATED SWALE

NOT TO SCALE



- A 6" THICK IMPERVIOUS CLAY LINER IS TO BE PLACED UNDER ENTIRE SEDIMENT FOREBAY AND SPILLWAY AND ONLY AROUND THE SIDES OF THE ENTIRE BIORETENTION AREA.
- SEDIMENT SHALL BE REMOVED FROM BEHIND THE STRUCTURE WHEN IT HAS ACCUMULATED TO ONE HALF THE ORIGINAL HEIGHT OF THE STRUCTURE.
- EMBANKMENT MATERIAL SHALL BE CLEAN MINERAL SOIL FREE OF ROOTS, ORGANIC MATTER, AND OTHER DELETERIOUS SUBSTANCES, IT SHALL CONTAIN NO ROCKS OR LUMPS OVER FOUR INCHES (4") IN DIAMETER. THIS MATERIAL SHALL BE INSTALLED IN 8" LIFTS COMPACTED TO 92% OF ASTM D-1557, AND SHALL MEET THE FOLLOWING SPECIFICATIONS: 6" PASSING 100%, #4 SIEVE 40-80%, #40 SIEVE 50-80%, #100 SIEVE 25-40%, #200 SIEVE 15-30% (OF THE TOTAL SAMPLE).
- ). 8" THICK IMPERMOUS CLAY LINER MATERIAL SHALL BE CLEAN SILTY—CLAY BORROW FREE OF ROOTS, ORGANIC MATTER, AND OTHER DELETERIOUS SUBSTANCES, AND SHALL CONTAIN NO ROCKS OR LINERS OVER THREE RICKES (3") IN DIMERER. THIS MATERIAL SHALL BE INSTALLED IN 8" URST COMPACTED TO 92% OF AST ID—1557, AND SHALL MEET THE FOLLOWING SPECIFICATIONS: 8" PASSING 100%, \$4 SERVE 95—100%, \$400 SERVE 80—80%, \$100 SIEVE 40—80%, \$200 SIEVE 25—48% (OF THE FRACTION PASSING THE \$4 SIEVE). THE CLAY COMPONENT SHALL HAVE A PLASTICITY INDEX OF AT LEAST 8 AND A HYDRAULIC CONDUCTIVITY OF 10 TO THE —6 CM/SEC.
- 5. COMPACTION AND MATERIALS TESTING SERVICES SHALL BE PERFORMED BY AN INDEPENDENT GEOTECHNICAL ENGINEER RETAINED BY THE OWNER.

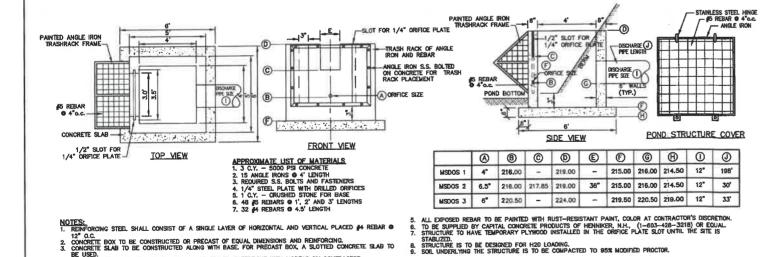
#### SEDIMENT FOREBAY SPILLWAY

NOT TO SCALE

**DETAIL SHEET** Plan Name: **BAYBERRY COMMONS** Project: 19 OLD GONIC ROAD, ROCHESTER, NH

LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148

DRAWING No **D4** SHEET 43 OF 45 JBE PROJECT NO. 21090



Design: JAC Draft: LAZ Date: 04/29/21 Checked: JAC Scale: AS NOTED Project No.:21090 Drawing Name: 21090-PLAN.dwg

NOT TO SCALE

THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN ION FROM JONES & BEACH ENGINEERS, INC. (JBE). ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.



BE USED.
SECTION JOINTS AND PIPE OPENING SHALL BE SEALED WATERTIGHT WITH MORTAR BY CONTRACTOR.

MULTI-STAGE DISCHARGE OUTLET STRUCTURE (MSDOS)

| 4    | 4/10/22  | REMOVED ROAD                          | LAZ |
|------|----------|---------------------------------------|-----|
| 3    | 3/11/22  | REVISED PER CITY COMMENTS             | LAZ |
| 2    | 2/14/22  | REVISED PER CITY ENGINEERING COMMENTS | LAZ |
| 1    | 1/18/22  | REVISED PER CITY COMMENTS             | LAZ |
| 0    | 11/23/21 | ISSUED FOR REVIEW                     | LAZ |
| REV. | DATE     | REVISION                              | BY  |

Designed and Produced in NH B Jones & Beach Engineers, Inc.

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#### **BLASTING SPECIFICATIONS**

LACS TINGS SPECIFICATIONS ENGINEERS. ALL ACTIVITIES RELATED TO BLASTING SHALL FOLLOW BEST MANAGEMENT PRACTICES FOR BLASTING, ALL ACTIVITIES RELATED TO BLASTING SHALL FOLLOW BEST MANAGEMENT PRACTICES (BMPS) TO PREVENT CONTAMINATION OF GROUNDWATER INCLUDING PREPARING, REVIEWING AND FOLLOWING AN APPROVED BLASTING PLAN; PROPER DRILLING, EDPLOSIVE HANDING AND LOADING PROCEDURES; OSSERVING THE ENTIRE BLASTING PROFEDURES; AND HANDLING AND STORAGE OF BLASTED ROCK.

## LOADING PRACTICES. THE FOLLOWING BLASTHOLE LOADING PRACTICES TO MINIMIZE ENVIRONMENTAL EFFECTS SHALL BE FOLLOWED.

- SHALL BE FOLLOWED:

  (a) DRILLING LOGS SHALL BE MAINTAINED BY THE DRILLER AND COMMUNICATED DIRECTLY TO THE BLASTER. THE LOGS SHALL INDICATE DEPTHS AND LENGTHS OF YOURS, CANTIES, AND FAULT ZONES OR OTHER WEAK ZONES SHALL INDICATE DEPTHS AND LENGTHS OF YOURS, CANTIES, AND FAULT ZONES OR OTHER WEAK ZONES

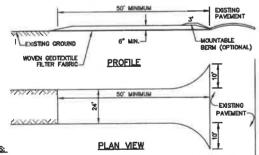
  (b) EXPLOSIVE PRODUCTS SHALL BE MANAGED ON SITE SO THAT THEY ARE EITHER USED IN THE BOREHOLE, RETURNED TO THE DELIVERY VEHICLE, OR PLACED IN SEQUIRE CONTAINERS FOR OFF- SITE DISPOSAL.

  (c) SPILLAGE AROUND THE BOREHOLE SHALL EITHER BE PLACED IN THE BOREHOLE OR CLEANED UP AND RETURNED TO AN APPROPRIATE VEHICLE FOR HANDLING OR PLACEMENT IN SECURED CONTAINERS FOR OFF-SITE DISPOSAL.

- LOADED EXPLOSIVES SHALL BE DETONATED AS SOON AS POSSIBLE AND SHALL NOT BE LEFT IN THE BLASTHOLES OVERNIGHT, UNLESS WEATHER OR OTHER SAFETY CONCERNS REASONABLY DICTATE THAT DETONATION SHOULD BE
- (e) LOADING EQUIPMENT SHALL BE CLEANED IN AN AREA WHERE WASTEWATER CAN BE PROPERLY CONTAINED AND HANDLED IN A MANNER THAT PREVENTS RELEASE OF CONTAINMANTS TO THE ENVIRONMENT.
- HANULEU IN A MANNER THAT PREVENTS RELEASE OF CONTAMINANTS TO THE ENVIRONMENT.

  (1) EXPLOSIVES SHALL BE LOADED TO MAINTAIN GOOD CONTINUITY IN THE COLUMN LOAD TO PROMOTE COMPLETE DETONATION. NDUSTRY ACCEPTED LOADING PRACTICES FOR PRIMING, STEMMING, DECKING AND COLUMN RISE NEED TO BE ATTENUED TO
- (2) EXPLOSIVE SELECTION. THE FOLLOWING BMPS SHALL BE FOLLOWED TO REDUCE THE POTENTIAL FOR CROUNDWATER CONTAMINATION WHEN EXPLOSIVES ARE USED:
- (a) EXPLOSIVE PRODUCTS SHALL BE SELECTED THAT ARE APPROPRIATE FOR SITE CONDITIONS AND SAFE BLAST
- (b) EXPLOSIVE PRODUCTS SHALL BE SELECTED THAT HAVE THE APPROPRIATE WATER RESISTANCE FOR THE SITE CONDITIONS PRESENT TO MINIMIZE THE POTENTIAL FOR HAZARDOUS EFFECT OF THE PRODUCT UPON GROUNDWATER.
- (3) PREVENTION OF MISSIRES, APPROPRIATE PRACTICES SHALL BE DEVELOPED AND IMPLEMENTED TO PREVENT
- (4) MUCK PILE MANAGEMENT, MUCK PILES (THE BLASTED PIECES OF ROCK) AND ROCK PILES SHALL BE MANAGED IN A MANNER TO REDUCE THE POTENTIAL FOR CONTAMINATION BY IMPLEMENTING THE FOLLOWING MEASURES:
- REMOVE THE MUCK PILE FROM THE BLAST AREA AS SOON AS REASONABLY POSSIBLE.
- REMOVE THE INJUN PILE FRUM THE BLAST AREA AS SUUM AS REASONABLY POSSIBLE.

  MANAGE THE INTERACTION OF BLASTED ROCK PILES AND STORMWATER TO PREVENT CONTAMINATION OF WATER
  SUPPLY WELLS OR SURFACE WATER.
- (5) SPILL PREVENTION MEASURES AND SPILL MITIGATION, SPILL PREVENTION AND SPILL MITIGATION MEASURES SHALL BE IMPLEMENTED TO PREVENT THE RELEASE OF FUEL AND OTHER RELATED SUBSTANCES TO THE ENVIRONMENT. THE MEASURES SHALL INJURIED AT A MANUAL MAN SHALL SH
  - Q. THE FUEL STORAGE REQUIREMENTS SHALL INCLUDE:
  - 1. STORAGE OF REGULATED SUBSTANCES ON AN IMPERVIOUS SURFACE.
  - 2. SECURE STORAGE AREAS AGAINST UNAUTHORIZED ENTRY.
  - 3. LABEL REGULATED CONTAINERS CLEARLY AND VISIBLY.
  - 4 INSPECT STORAGE AREAS WEEKLY.
  - 5. COVER REGULATED CONTAINERS IN OUTSIDE STORAGE AREAS.
  - 6. WHEREVER POSSIBLE, KEEP REGULATED CONTAINERS THAT ARE STORED OUTSIDE MORE THAN 50 FEET FROM SURFACE WATER AND STORM DRAINS, 75 FEET FROM PRIVATE WELLS, AND 400 FEET FROM PUBLIC WELLS.
  - 7. SECONDARY CONTAINMENT IS REQUIRED FOR CONTAINERS CONTAINING REGULATED SUBSTANCES STORED OUTSIDE, EXCEPT FOR ON PREMISE USE HEATING FUEL TANKS, OR ABOVEGROUND OR UNDERGROUND STORAGE TANKS OTHERWISE REGULATED.
  - b. THE FUEL HANDLING REQUIREMENTS SHALL INCLUDE:
  - 1. EXCEPT WHEN IN USE, KEEP CONTAINERS CONTAINING REGULATED SUBSTANCES CLOSED AND SEALED.
  - 2. PLACE DRIP PANS UNDER SPIGOTS, VALVES, AND PUMPS. 3. HAVE SPILL CONTROL AND CONTAINMENT EQUIPMENT READILY AVAILABLE IN ALL WORK AREAS.
  - 4 LISE FLINNELS AND DRIP PANS WHEN TRANSFERRING REGULATED SUBSTANCES.
  - 5.PERFORM TRANSFERS OF REGULATED SUBSTANCES OVER AN IMPERVIOUS SURFACE.
  - c. THE TRAINING OF ON-SITE EMPLOYEES AND THE ON-SITE POSTING OF RELEASE RESPONSE INFORMATION DESCRIBING WHAT TO DO IN THE EVENT OF A SPILL OF REGULATED SUBSTANCES.
  - d. Fueling and maintenance of excavation, earthnowing and other construction related equipment will comply with the regulations of nindes (note these requirements are summarzed in wooned 22-8: "Best management practices for fueling and maintenance of excavation and earthnoving equipment" or its exception portly of the property of



## NOTES:

- NOTES:

  1. STONE FOR STABILIZED CONSTRUCTION ENTRANCE SHALL BE 1 TO 2 INCH STONE, RECLAIMED STONE, OR RECYCLED CONCRETE EQUIVALENT.

  2. THE LENGTH OF THE STABILIZED ENTRANCE SHALL NOT BE LESS THAN 50 FEET, EXCEPT FOR A SINGLE RESIDENTIAL LOT WHERE A 30 FOOT MINIMUM ENGTH WOULD APPLY.

  3. THICKNESS OF THE STONE FOR THE STABILIZED STRANDES SHALL NOT BE LESS THAN 6 INCHES.

  4. THE WOIT OF GREESS COCKIES, OR 10 FEET, WHICKNEY HAVE SHALL NOT BE LESS THAN 6 INCHES.

  5. MINIMUM SHAPE STONE FOR THE STABILIZED STRANDES SHALL NOT BE LESS THAN 6 INCHES.

  6. ALL SURFACE WATER THAT IS FLOWING TO OR DIVERTED TOWARD THE ONSTRUCTION ENTRANCE SHALL BE PIPED BELFATH THE BRITANDES IN SHALL BE PIPED BELFATH THE BRITANDES SHALL BE PIPED BELFATH THE BRITANDES SHALL BE STONE.

  7. THE ENTRANCE SHALL BE MANTANDED FOR THE PIPE.

  7. THE ENTRANCE SHALL BE MANTANDED IN A CONDITION THAT WILL PREVENT TRACKING OR FLOWING OF SEDIMENT CNITO THE PUBLIC RIGHT—OF—WAY. THIS MAY REQUIRE PERIODIC TOP DRESSING WITH ADDITIONAL STONE AS COMMITTIONS DEARNON THE ADDITIONAL STONE AS COMMITTIONS DEARNON SHARES SHEED IN TRAPE.
- STONE AS CONDITIONS DEMAND AND REPAIR AND/OR CLEAN OUT OF ANY MEASURES USED TO TRAP-SEDIMENT. ALL SEDIMENT SPILLED, WASHED, OR TRACKED ONTO THE PUBLIC RIGHT-OF-WAY MUST BE REMOVED PROMPTLY.

### STABILIZED CONSTRUCTION ENTRANCE

Date: 04/29/21

NOT TO SCALE

Design: JAC | Draft: LAZ

#### TEMPORARY EROSION CONTROL NOTES

- THE SMALLEST PRACTICAL ASEA OF LAND SHALL BE EXPOSED AT ANY ONE TIME. AT NO TIME SHALL AN AREA IN EXCESS OF 5 ACRES BE EXPOSED AT ANY ONE TIME BEFORE DISTURBED AREAS ARE STABILIZED.
- EROSION, SEDIMENT AND DETENTION MEASURES SHALL BE INSTALLED AS SHOWN ON THE PLANS AND AT LOCATIONS AS REQUIRED, DIRECTED BY THE ENGINEER.
- ALL DISTURBED AREAS (INCLUDING POND AREAS BELOW THE PROPOSED WATERLINE) SHALL BE RETURNED TO PROPOSED GRADES AND ELEVATIONS. DISTURBED AREAS SHALL BE LOAMED WITH A MINIMUM OF 6" OF SCREENED ORGANIC LOAM AND SEEDED WITH SEED MIXTURE "C" AT A RATE NOT LESS THAN 1.10 POUNDS OF SEED PER 1,000 S.F. OF AREA (48 LBS. / ACRE).
- SLT FENCES AND OTHER BARRIERS SHALL BE INSPECTED EVERY SEVEN CALENDAR DAYS AND WITHIN 24 HOURS OF A RAINFALL OF 0.5° OR GREATER, ALL DAMAGED AREAS SHALL BE REPAIRED, AND SEDIMENT DEPOSITS SHALL PERDOCALLY BE REMOVED AND DISPOSED OF.
- AFTER ALL DISTURBED AREAS HAVE BEEN STABILIZED, THE TEMPORARY EROSON CONTROL MEASURES SHALL BE REMOVED AND THE AREA DISTURBED BY THE REMOVAL SMOOTHED AND RE-VEGETATED.
- AREAS MUST BE SEEDED AND MULCHED OR OTHERWISE PERMANENTLY STABILIZED WITHIN 3 DAYS OF FINAL GRADING, OR TEMPORARILY STABILIZED WITHIN 40 DAYS OF THE INITIAL DISTURBANCE OF SOIL ALL AREAS SHALL BE STABILIZED WITHIN 45 DAYS OF INITIAL DISTURBANCE.
- IN APEAS WHERE FINAL CRADING HAS NOT OCCURRED, TEMPORARY STABILIZATION MEASURES SHOULD BE IN PLACE WITHIN 5 CALENDAR DAYS FOR EXPOSED SOIL AREAS THAT ARE WITHIN 100 FEET OF A SURFACE WATERBOOY OR A WETLAND AND NO MORE THAN 14 CALENDAR DAYS FOR ALL OTHER AREAS PERMANENT STABILIZATION SHOULD BE IN PLACE WITHIN 3 CALENDAR DAYS FOLLOWING COMPLETION OF FINAL GRADING OF EXPOSED SOIL AREAS.
- ALL PROPOSED VEGETATED AREAS THAT DO NOT EXHIBIT A MINIMUM OF 85 PERCENT VEGETATIVE GROWTH BY OCTOBER 15, OR WHICH ARE DISTURBED AFTER OCTOBER 15, SHALL BE STABILIZED BY SEZDING AND INSTALLING NORTH AMERICAN GREEN 975 EROSINO CONTROL BILANKETS (OR AN EQUIVALENT APPROVED IN WRITING BY THE ENGINEER) ON SLOPES GREATER THAN \$1, AND SEZDING AND PLACING 3 TO 4 TONS OF MULCH PER ACRE, SCOURCE WITH ANCHORED NETTING, ELSEWHERE. THE INSTALLATION OF EROSION CONTROL BLANKETS OR MULCH AND NETTING SHALL NOT OCCUR. OVER ACCUMULATED SNOW OR ON FROZEN GROUND AND SHALL BE COMPLETED IN ADVANCE OF THAW OR SPRING MELT
- ALL DITCHES OR SWALES WHICH DO NOT EXHIBIT A MINIMUM OF 85 PERCENT VEGETATIVE GROWTH BY OCTOBER 15, OR WHICH ARE DISTURBED AFTER OCTOBER 15, SHALL BE STABILIZED TEMPORARLY WITH STONE OR ERCSION CONTROL BLANKETS APPROPRIATE FOR THE DESIGN FLOW CONDITIONS.
- AFTER OCTOBER 15th, INCOMPLETE ROAD OR PARKING SURFACES, WHERE WORK HAS STOPPED FOR THE WINTER SEASON, SHALL BE PROTECTED WITH A MINIMUM OF 3" OF CRUSHED GRAVEL PER NHDOT ITEM 304.3.
- 11. AN AREA SHALL BE CONSIDERED STABLE IF ONE OF THE FOLLOWING HAS OCCURRED:
  - a. BASE COURSE GRAVELS HAVE BEEN INSTALLED IN AREAS TO BE PAVED;
  - IN A MINIMUM OF REST VEGETATED GROWTH HAS BEEN ESTABLISHED:
  - c. A MINIMUM OF 3" OF NON-EROSIVE MATERIAL SUCH STONE OR RIPRAF HAS BEEN INSTALLED; OR
- & EROSION CONTROL BLANKETS HAVE BEEN PROPERLY INSTALLED.
- Fugitive dust control is required to be controlled in accordance with env-a 1000, and the project is to meet the requirements and intent of RSA 430:53 and AGR 3800 relative to invasive species.
- PRIOR TO BEGINNING CONSTRUCTION, THE CONTRACTOR'S NAME, ADDRESS, AND PHONE NUMBER SHALL BE SUBMITTED TO DES VIA EMAIL (SEE BELOW).
- 13. PRIOR TO CONSTRUCTION, A PHASING PLAN THAT DELINEATES EACH PHASE OF THE PROJECT SHALL BE SUBMITTED. ALL TEMPORARY SEDIMENT BASINS THAT WILL BE NEEDED FOR DEWATERING WORK AREAS SHALL BE LOCATED AND IDENTIFIED ON THIS PLAN.
- IN ORDER TO ENSURE THE STABILITY OF THE SITE AND EFFECTIVE IMPLEMENTATION OF THE SEDIMENT AND EROSION CONTROL MEASURES SPECIFIED IN THE PLANS FOR THE DURATION OF CONSTRUCTION, THE CONTRACTOR SHALL BE IN STRECT COMPLIANCE WITH THE FOLLOWING INSPECTION AND MAINTENANCE REQUIREMENTS IN ADDITION TO THOSE CALLED FOR IN THE SWPPP:
  - 5. A CERTIFIED PROFESSIONAL IN EROSION AND SEDIMENT CONTROL OF A PROFESSIONAL ENGINEER LICENSED IN THE TATE OF NEW HAMPSHIRE ("MONITOR") SHALL BE EMPLOYED TO INSPECT THE SITE FROM THE START OF LTERATION OF TERRAIN ACTIVITIES UNTIL THE SITE IS IN FULL COMPUANCE WITH THE SITE SPECIFIC PERMIT
  - b. DURING THIS PERIOD, THE MONITOR SHALL INSPECT THE SUBJECT SITE AT LEAST ONCE A WEEK, AND IF POSSIBLE, DURING ANY 1/2 INCH OR GREATER RAIN EVENT (LE. 1/2 INCH OF PRECIPITATION OR MORE WITHIN A 24 HOUR PERIOD). IF UNABLE TO BE PRESENT DURING SUCH A STORM, THE MONITOR SHALL INSPECT THE SITE WITHIN 24 HOURS OF THIS EVENT.
  - c. THE MONITOR SHALL PROVIDE TECHNICAL ASSISTANCE AND RECOMMENDATIONS TO THE CONTRACTOR ON THE APPROPRIATE BEST MANAGEMENT PRACTICES FOR EROSION AND SEDIMENT CONTROLS REQUIRED TO MEET THE REQUIREMENTS OF RSA 458 A:17 AND ALL APPLICABLE DES PERMIT CONTRIONS.
  - d. WITHIN 24 HOURS OF EACH INSPECTION, THE MONITOR SHALL SUBMIT A REPORT TO DES VIA EMAIL (RIDGELY MALICK AT: RIDGELY MALICK BDES.NH.GOV). e. THE MONITOR SHALL MEET WITH DES TO DECIDE UPON A REPORT FORMAT. THE REPORT FORMAT SHALL BE BENEFUED AND APPROVED BY DES PRIOR TO THE START OF CONSTRUCTION.

# Stabilize Outermost Bank With Sad or Other Sultable Material Earth PLAN VIEW CROSS SECTION

#### TEMPORARY SEDIMENT BASIN

NOT TO SCALE

#### SEEDING SPECIFICATIONS

- 1. GRADING AND SHAPING
  A. SLOPES SHALL NOT BE STEEPER THAN 2:1 WITHOUT APPROPRIATE EROSION CONTROL MEASURES AS SPECIFIED ON THE PLANS (3:1 SLOPES OR FLATTER ARE PREFERRED).
  B. WHERE MOWING MILL BE DOWN, 3:1 SLOPES OR FLATTER ARE RECOMMENDED.

- SEDBED PREPARATION
   A. SURFACE AND SEEPAGE WATER SHOULD BE DRAINED OR DIVERTED FROM THE SITE TO PREVENT DROWNING OR WINTER KILLING OF THE PLANTS.
   B. STONES LARGER THAN 4 INCHES AND TRASH SHOULD BE REMOVED BECAUSE THEY INTERFERE WITH SEEDING AND FUTURE MAINTENANCE OF THE AREA. WHERE FEASIBLE, THE SOIL SHOULD BE TILLED TO A DEPTH OF ABOUT 4 INCHES TO PREPARE A SEEDBED AND FERTILIZER AND LIME MIXED INTO THE SOIL THE SEEDBED SHOULD BE LEFT IN A REASONABLY FIRM AND SMOOTH CONDITION. THE LAST TILLAGE OPERATION SHOULD BE PERFORMED ACROSS THE SLOPE WHEREVER PRACTICAL.

- 3. <u>Establishing a Stand.</u>

  A. Lime and fertilizer should be applied pror to or at the time of seeding and incorporated into the soil. Types and amounts of lime and fertilizer should be based on an evaluation of soil tests, when a soil test is not available, the following minimum amounts should be applied:
  - APPLIED: AGRICULTURAL LIMESTONE. 2 TONS PER ACRE OR 100 LBS. PER 1,000 SQ.FT.
- AGRICULTURAL LIMESTONE, 2 TONS PER ACRE OR 100 LBS. PER 1,000 SQ.FT.
  NITROGEN(N), 50 LBS. PER ACRE OR 1.1 LBS. PER 1,000 SQ.FT.
  PHOSPHATE(P.205), 100 LBS. PER ACRE OR 2.2 LBS. PER 1,000 SQ.FT.
  POTASH(XCQ), 100 LBS. PER ACRE OR 2.2 LBS. PER 1,000 SQ.FT.
  (NOTE: THIS IS THE EQUIVALENT OF 500 LBS. PER ACRE OF 10-20-20 FERTILIZER OR 1,000 LBS. PER
  ACRE OF 5-10-10.)
  EXEMPTION OF THE STIPLE OF THE REFER TO THE 'SEEDING GUIDE' AND 'SEEDING RATES' TABLES ON THIS SHEET FOR APPROPRIATE SEED
- REPER TO THE SEEDING GUIDE AND SEEDING RATES TABLES ON THIS SMELL FOR APPROPRIATE SEED MIXTURES AND RATES OF SEEDING. ALL LEGIURES (ROOMWITCH, BIRDSFOOT, TREFIC), AND FLATFEA) MUST BE INOCULATED WITH THEIR SPECIFIC INOCULANT PRIOR TO THEIR INTRODUCTION TO THE SITE. WHEN SEEDED AREAS ARE MULCHED, PLANTINGS MAY BE MADE FROM EARLY SPRING TO EARLY OCTOBER. WHEN SEEDED AREAS ARE NOT MULCHED, PLANTINGS SHOULD BE MADE FROM EARLY SPRING TO MAY 20th OR FROM AUGUST 10th TO SEPTEMBER 1st.

4. MULCH
A. HAY, STRAW, OR OTHER MULCH, WHEN NEEDED, SHOULD BE APPLIED INMEDIATELY AFTER SEEDING.
B. MULCH WILL BE HELD IN PLACE USING APPROPRIATE TECHNIQUES FROM THE BEST MANAGEMENT PRACTICE
FOR MULCHING, HAY OR STRAW MULCH SHALL BE PLACED AT A RATE OF 90 LBS PER 1000 S.F.

- MAINTENANCE TO ESTABLISH A STAND.
   A PLANTED AREAS SHOULD BE PROTECTED FROM DAMAGE BY FIRE, GRAZING, TRAFFIC, AND DENSE WEED
- GROWIT.

  FORTILIZATION NEEDS SHOULD BE DETERMINED BY ONSITE INSPECTIONS. SUPPLEMENTAL FERTILIZER IS USUALLY THE KEY TO FULLY COMPLETE THE ESTABLISHMENT OF THE STAND BECAUSE MOST PERENNALS TAKE 2 TO 3 YEARS TO BECOME FULLY ESTABLISHED.

  C. IN WATERWAYS, CHAMINELS, OR SWALES WHERE UNFORM FLOW CONDITIONS ARE ANTICIPATED, ANNUAL MOWING MAY BE NECESSARY TO CONTROL GROWTH OF WOODY VEGETATION.

| USE  | SEEDING<br>MIXTURE 1/ | DROUGHTY             | WELL<br>DRAINED   | MODERATELY<br>WELL<br>DRAINED | POORLY<br>DRAINED    |
|--|-----------------------|----------------------|-------------------|-------------------------------|----------------------|
| STEEP CUTS AND<br>FILLS, BORROW<br>AND DISPOSAL  | A<br>B<br>C           | FAIR<br>POOR<br>POOR | G000<br>G000      | GOOD<br>FAIR<br>EXCELLENT     | FAIR<br>FAIR<br>GOOD |
| AREAS  | D                     | FAIR                 | EXCELLENT         | EXCELLENT                     | POOR                 |
| WATERWAYS, EMERGENC'<br>SPILLWAYS, AND OTHER<br>CHANNELS WITH<br>FLOWING WATER.                          |                       | G000<br>G000         | G000<br>EXCELLENT | GOOD<br>EXCELLENT             | FAIR<br>FAIR         |
| LIGHTLY USED PARKING<br>LOTS, ODD AREAS,<br>LINUSED LANDS, AND<br>LOW INTENSITY USE<br>RECREATION SITES. | A<br>B<br>C           | GOOD<br>GOOD         | GOOD<br>EXCELLENT | GOOD<br>FAIR<br>EXCELLENT     | FAIR<br>POOR<br>FAIR |
| PLAY AREAS AND<br>ATHLETIC FIELDS.<br>(TOPSOIL IS ESSENTIAL<br>FOR GOOD TURF.)                           | E<br>F                | FAIR<br>FAIR         | EXCELLENT         | EXCELLENT                     | 2/<br>3/             |

GRAVEL PIT, SEE NH-PM-24 IN APPENDIX FOR RECOMMENDATION REGARDING RECLAMATION OF SAND AND GRAVEL PITS.

1/ REFER TO SEEDING MIXTURES AND RATES IN TABLE BELOW.
27 POORLY DRAINED SOILS ARE NOT DESIRABLE FOR USE AS PLAYING AREA AND ATHLETIC FIELDS.

NOTE: TEMPORARY SEED MIX FOR STABILIZATION OF TURF SHALL BE WINTER RYE OR GATS AT A RATE OF 2.5 USS. PER 1000 S.F. AND SHALL BE PLACED PRIOR TO OCTOBER 19th, IF PERMANENT SEEDING NOT YET COMPLETED.

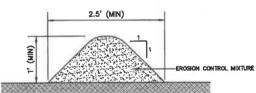
#### SEEDING GUIDE

| POUNDS<br>PER ACRE | 1.000 Sq. Ft   |
|--------------------|--|
| 20                 | 0.45   |
| 20                 | 0.45   |
| 2                  | 0.05   |
| 42                 | 0.95   |
| 15                 | 0.35   |
| 10                 | 0.25   |
| 15                 | 0.35   |
| 30                 | 0.75   |
| 40 OR 55           | 0.95 OR 1.35   |
| 20                 | 0.45   |
| 20                 | 0.45   |
| 8                  | <u>0.20</u>  |
| 48                 | 1.10   |
| 20                 | 0.45   |
| 30                 | 0.75   |
| 50                 | 1.20   |
| 50                 | 1.15   |
| 50                 | 1.15   |
| 100                | 2.30   |
| 150                | 3.60   |
|                    | 20<br>20<br>22<br>42<br>15<br>10<br>15<br>15<br>5<br>40 OR 55<br>20<br>8<br>48<br>20<br>50<br>50 |

SEEDING RATES

#### CONSTRUCTION SEQUENCE

- PRIOR TO THE START OF ANY ACTIVITY, IT IS THE RESPONSIBILITY OF THE STE'S SITE DEVELOPER (OR OWNER) TO FILE A NOTICE OF INTENT (NO!) FORM WITH THE ENVIRONMENTAL PROTECTION ACENCY (EPA IN ORDIER TO GAIN COMPERAGE UNDER THE PROPES GENERAL PERMIT FOR STORM WATER DISCHARGES CONSTRUCTION ACTIVITIES. A PRE CONSTRUCTION MEETING IS TO BE HELD WITH ALL DEPARTMENT HEAD PRIOR TO THE START OF CONSTRUCTION.
- WETLAND BOUNDARIES ARE TO BE CLEARLY MARKED PRIOR TO THE START OF CONSTRUCTION.
- 3. CLIT AND REMOVE TREES IN CONSTRUCTION AREA AS REQUIRED OR DIRECTED.
- CLEAR, CUT, GRUB AND DISPOSE OF DEBRIS IN APPROVED FACILITIES. THIS INCLUDES ANY REQUIRED DENOLITION OF EXISTING STRUCTURES, UTILITIES, ETC.
- 8. CONSTRUCT AND/OR INSTALL TEMPORARY OR PERMANENT SEDIMENT AND/OR DETENTION BASIN(S) AS REQUIRED. THESE FACILITIES SHALL BE INSTALLED AND STABILIZED PRIOR TO DIRECTING RUN-OFF TO
- STRIP LOAM AND PAVEMENT, OR RECLAIN EXISTING PAVEMENT WITHIN LIMITS OF WORK PER THE RECOMMENDATIONS OF THE PROJECT ENGINEER AND STOCKPILE EXCESS MATERIAL STABILIZE STOCKPILE AS NECESSARY.
- 8. PERFORM PRELIMINARY SITE GRADING IN ACCORDANCE WITH THE PLANS, INCLUDING THE CONSTRUCTION OF ANY RETAINING WALLS.
- 9. PREPARE BUILDING PAD(S) TO ENABLE BUILDING CONSTRUCTION TO BEGIN.
- INSTALL THE SEWER AND DRAINAGE SYSTEMS FIRST, THEN ANY OTHER UTILITIES IN ACCORDANCE WITH THE PLAN AND DETAILS. ANY CONFLICTS BETWEEN UTILITIES ARE TO BE RESOLVED WITH THE INVOLVEMENT AND APPROVAL OF THE ENGINEER.
- 11. INSTALL INLET PROTECTION AT ALL CATCH BASINS AS THEY ARE CONSTRUCTED IN ACCORDANCE WITH DETAILS
- ALL SWALES AND DRAINAGE STRUCTURES ARE TO BE CONSTRUCTED AND STABILIZED PRIOR TO HAVING RUN-OFF DIRECTED TO THEM.
- PERFORM FINAL FINE GRADING, INCLUDING PLACEMENT OF "SELECT" SUBGRADE NATERIALS.
- 15. PAVE ALL PARKING LOTS AND ROADWAYS WITH INITIAL BASE COURSE'.
- PERFORM ALL REMAINING SITE CONSTRUCTION (i.e. BUILDING, CURBING, UTILITY CONNECTIONS, ETC.).
- LOAM AND SEED ALL DISTURBED AREAS AND INSTALL ANY REQUIRED SEDIMENT AND EROSION CONTROL FACULTIES (i.e. RIP RAP, EROSION CONTROL BLANKETS, ETC.).
- 18 FINISH PAYING ALL ROADWAYS AND PARKING AREAS WITH "FINISH" COURSE.
- ALL ROADWAYS AND PARKING LOTS SHALL BE STABILIZED WITHIN 72 HOURS OF ACHIEVING FINISHED GRADE.
- 20. ALL CUT AND FILL SLOPES SHALL BE SEEDED/LOAMED WITHIN 72 HOURS OF ACHIEVING FINISHED GRADE.
- 21. COMPLETE PERMANENT SEEDING AND LANDSCAPING.
- 22. REMOVE TEMPORARY EROSION CONTROL MEASURES AFTER SEEDING AREAS HAVE BEEN 75%-85% ESTABLISHED AND SITE IMPROVEMENTS ARE COMPLETE. SMOOTH AND RE-VEGETATE ALL DISTURBED AREAS.
- 23. CLEAN SITE AND ALL DRAINAGE STRUCTURES, PIPES AND SUMPS OF ALL SILT AND DEBRIS.
- 24. INSTALL ALL PAINTED PAVEMENT MARKINGS AND SIGNAGE PER THE PLANS AND DETAILS. 25. ALL EROSION CONTROLS SHALL BE INSPECTED WEEKLY AND AFTER EVERY HALF-INCH OF RAINFALL.
- 26. UPON COMPLETION OF CONSTRUCTION, IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO NOTIFY ANY RELEVANT PERMITTING AGENCIES THAT THE CONSTRUCTION HAS BEEN FINISHED IN A SATISFACTORY MAINTRY.



#### NOTES:

- 1 ORGANIC FILTER BERMS MAY BE LITILIZED IN LIEU OF SILT FENCE, UNLESS OTHERWISE SPECIFIED.
- THE EROSION CONTROL MIX USED IN THE FILTER BERMS SHALL BE A WELL-GRADED MIXTURE OF PARTICLE SIZES, MAY CONTAIN ROCKS LESS THAN 4" IN DIAMETER, STUMP GRADINOS, SHEDDED OR COMPOSTED BARK, OR ACCEPTABLE MANUFACTURED PRODUCTS, AND SHALL BE FREE OF REFUSE, PHYSICAL CONTAMINANTS, AND MATERIAL TOXIC TO PLANT GROWTH, AND SHALL MEET THE FOLLOWING STANDARDS.
- d) THE ORGANIC CONTENT SHALL BE 80-100% OF DRY WEIGHT.
  b) PARTICLE SIZE BY WEIGHT SHALL BE 100% PASSING A 6" SCREEN, AND 70-85% PASSING A 0.75" SCREEN.
  c) THE ORGANIC PORTION SHALL BE FIBROUS AND ELONGATED.
  d) LARGE PORTIONS OF SILTS, CLAYS, OR FINE SANDS SHALL NOT BE INCLUDED IN THE INVENTIGE.

- ORGANIC FILTER BERMS SHALL BE INSTALLED ALONG A RELATIVELY LEVEL CONTOUR. IT MAY BE NECESSARY TO CUT TALL GRASSES OR WOODY VEGETATION TO AVOID CREATING VOIDS AND BRIDGES THAT WOULD ENABLE FINES TO WASH UNDER THE BERN.
- ON SLOPES LESS THAN 5%, OR AT THE BOTTOM OF SLOPES STEEPER THAN 3:1, UP TO 20' LONG, THE BERM SHALL BE A MINIMUM OF 12" HIGH (AS MEASURED ON THE UPHILL SIDE), AND A MINIMUM OF 36" MIDE. ON LONGER OR STEEPER SLOPES, THE BERM SHALL BE WIDER TO ACCOMMODATE THE POTENTIAL ADDITIONAL RUNOFF.
- 5. FROZEN GROUND, OUTCROPS OF BEDROCK, AND VERY ROOTED FORESTED AREAS PRESENT THE MOST PRACTICAL AND EFFECTIVE LOCATIONS FOR ORGANIC FILTER BETMS. OTHER BBYS SHOULD BE USED AT LOW POINTS OF CONCENTRATED RUNDET, BELOW CULVERT OUTLET APRONS, AROUND CATCH BUSING, AND AT THE BOTTOM OF STEEP PERMETER SLOPES THAT HAVE A LARGE CONTRIBUTING AREA. SEDIMENT SHALL BE REMOVED FROM BEHIND THE STRUCTURES WHEN IT HAS ACCUMULATED TO ONE HALF THE ORIGINAL HEIGHT OF THE STRUCTURE.
- 7. STRUCTURES MAY BE LEFT IN PLACE ONCE THE SITE IS STABILIZED.
- ORGANIC FILTER BERM

NOT TO SCALE

Designed and Produced in NH LAZ REMOVED ROAD LAZ REVISED PER CITY COMMENTS Jones & Beach Engineers, Inc. LAZ LAZ

PO Box 219

LAZ

BY

**EROSION AND SEDIMENT CONTROL DETAILS** Plan Name: **BAYBERRY COMMONS** 

19 OLD GONIC ROAD, ROCHESTER, NH

LEO P. LACOUTURE REV. TRUST & WILLIAN B. LACOUTURE 19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148

SHEET 44 OF 45

DRAWING No.

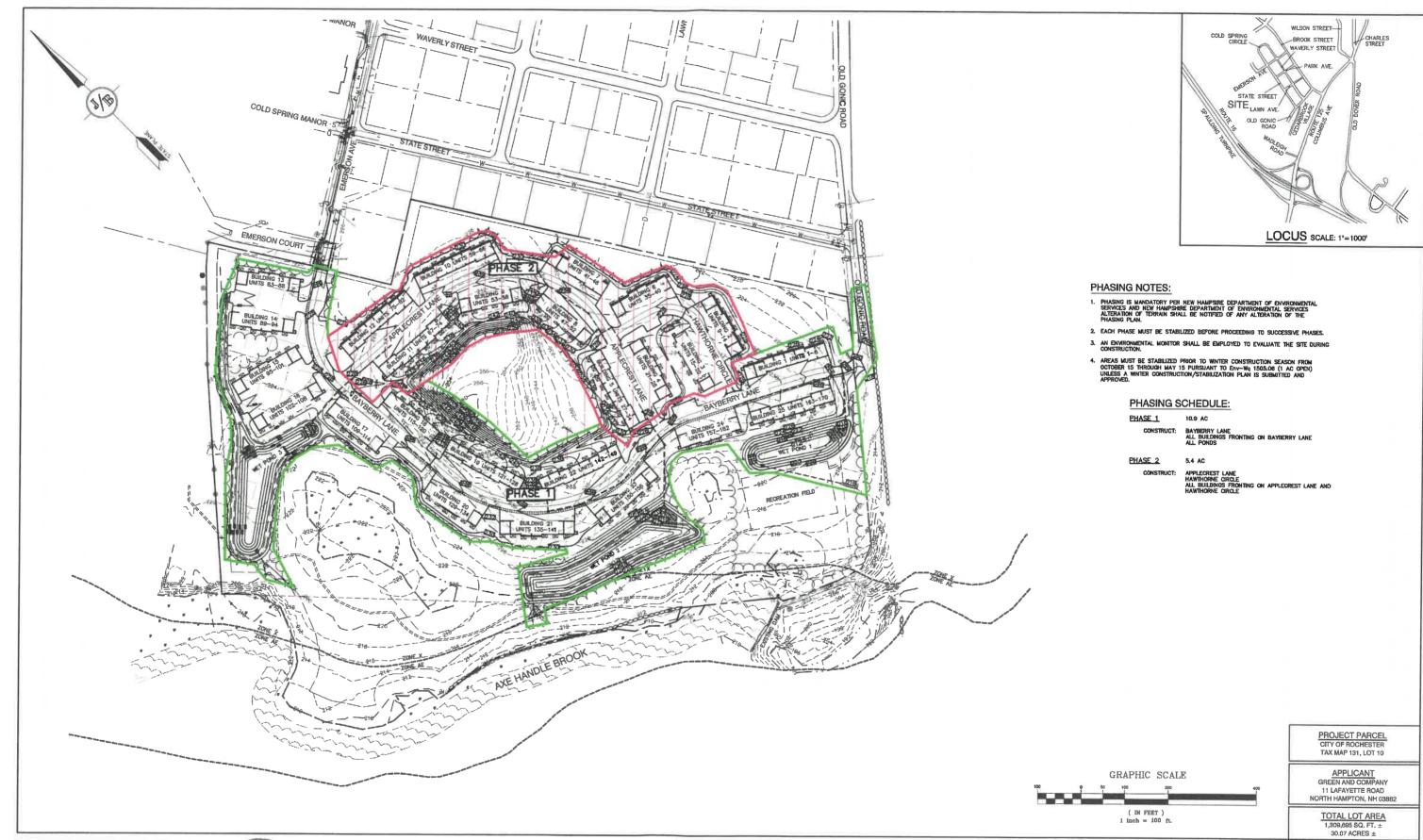
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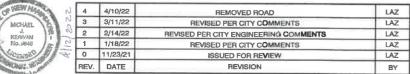


4 4/10/22 3 3/11/22 2 2/14/22 REVISED PER CITY ENGINEERING COMMENTS 1/18/22 REVISED PER CITY COMMENTS 0 11/23/2 ISSUED FOR REVIEW REV. DATE

85 Portsmouth Ave. Civil Engineering Services FAX: 603-772-0227



| Design: JAC     | Dran;    | LAZ          | Date: 04/29/21       |
|-----------------|----------|--------------|----------------------|
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| Plan Name:       | PHASING PLAN   |
|------------------|--|
| Project:         | BAYBERRY COMMONS<br>19 OLD GONIC ROAD, ROCHESTER, NH   |
| Owner of Record: | LEO P. LACOUTURE REV. TRUST & WILLIAN B, LACOUTURE<br>19 OLD GONIC RD., ROCHESTER, NH 03867 BK 4093 PG 148 |

